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NATIONAL PROGRAMME ON
TECHNOLOGY ENHANCED LEARNING

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ADVANCE
PROCESS CONTROL

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Lecture No. 04

Topic:
Development of Control Relevant
Linear Perturbation Models - 1

Sub-Topic:

Introduction to Z-Transforms and
Development of Grey-box Models

In our last lecture we were looking at Z-transforms, I just briefly introduced Z-transforms, so Z-transforms are defined for the sequence of vectors or a sequence of scalars, infinite sequence world from time 0 to time ∞ it is a discrete sequence.

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z Transforms

Consider discrete time uniformly sampled discrete signal
 $\{f(k) : k = 0, 1, \dots\}$
 z-Transform of $\{f(k)\}$ is defined as

$$Z\{f(k)\} = f(z) = \sum_{k=0}^{\infty} f(k)z^{-k}$$
 where z is a complex variable.
 Inverse transform is given as

$$f(k) = \frac{1}{2\pi j} \oint f(z)z^{k-1} dz$$
 where contour integral encloses all singularities of $f(z)$.

Note: $z = e^{Ts}$ and $T =$ sampling interval, $s =$ Laplace operator

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The set of values which are connected at uniform sampling interval, whatever it is could be, as I said it could be one second it could be 0.1 second, it could be 1, depending upon the application. And Z-transform of this infinite sequence is defined by what is given here, and corresponding the defined, so Z-transform converts the signal from time domain to Z domain. And it can define inverse Z-transform which converts the signal from Z domain to time domain okay.

The relationship between S and Z-transform, and I am going to derive it in this class, I am going to leave it to you to read about it, I have given two reference at the end of these notes, I represent giving notes slightly revised notes, we make our corrections in the last lecture. So I opposed those notes, so you can have a look at it.

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Reference Textbooks

- Astrom, K. J., and B. Wittenmark, *Computer Controlled Systems*, Prentice Hall India (1994).
- Franklin, G. F., Powell, J. D., and M. L. Workman, *Digital Control Systems*, Addison Wesley, 1990.
- Ljung, L., Glad, T., *Modeling of Dynamic Systems*, Prentice Hall, N. J., 1994.

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At the end if I put three references which, so at the end I give three references, the first text book here is Astrom and Wittenmark. You can say this is like Bible of digital control, if you want to know, if you want to perceive career control systems, this is the book which you must have. This was, what I have given here is one which I have published by Prentice Hall India no longer Indian nation is available.

International nation of this book is of course available, you should buy edition 3 if you are interested. The second book is also equally important reference, a very good book Franklin and Powell on digital control systems. Throughout this course I will not going to refer to one book, I will do with multiple books, I will keep giving you references. It is not possible to come up with one single reference for this course.

Because this is your advanced control course which is my version okay. So advanced control is a notion Mendel, I am picking up a few things from it and put it and giving it to you, because what I think is relevant is, what is represented. So it is going to be collection of the new material form variety of sources. So at this part I would refer to this particular text book okay.

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z Transforms : Properties

Linearity

$$Z[af(k) + bg(k)] = aZ[f(k)] + bZ[g(k)]$$

Time Shift

$$Z\{q^{-n}f(k)\} = z^{-n}f(z)$$

$$Z\{q^n f(k)\} = z^n \left[f(z) - \sum_{j=0}^{n-1} f(j)z^{-j} \right]$$

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So let us go back and have a look at Z-transforms okay. So we looked at the properties just a quick review that linearity modes if you add to signals, but if you take two signals and take a linear population of two signals and take Z-transform is nothing but Z-transform of a linear combination of Z-transform will be reduces. Then time shift is one of the important property for us, this time shift property is used to convert difference equation into an algebraic equation.

Just like analogy is used, Laplace operator to convert a differential equation into an algebraic equation. Likewise, here Z-transforms are used to convert a difference equation into an algebraic equation, linear difference equation. So this is the fundamental result which is used for converting, and you can see similarities between the result in Laplace domain. In Laplace domain if you are nth derivative, you will get S^n if you remember, you will get S^n .

Here you have a difference operator which is n steps higher in future you will get Z^1 , Z^1 you see that, that is quiet close resemblance between the – and you have initial value theft in mind, final value theorem which are analogous to what you have in continuous time or in Laplace domain.

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z Transforms : Examples

Example 1

$y(kT) = \alpha$ with $k \geq 0$ (step function)

$$Z\{y(kT)\} = \alpha + \alpha z^{-1} + \alpha z^{-2} + \dots$$

$$= \frac{\alpha}{1 - z^{-1}}$$

Example 2

$y(kT) = kT$ with $k \geq 0$ (ramp)

$$Z\{y(kT)\} = 0 + Tz^{-1} + 2Tz^{-2} + \dots$$

$$= T(z^{-1} + z^{-2} + \dots)$$

$$= \frac{Tz}{(z-1)^2}$$

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In the last class I gave some examples of Z-transforms the simple signal which is units that at 0 before time 0 and becomes value α at time 0 to ∞ , such a signal if you take Z-transform we will get Z^{-1} . And likewise if you obtain this book computer control systems or Franklin and Powell give us the examples or you will see tables of Z-transforms of variety of signals.

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Pulse Transfer Function Matrix

$$\mathbf{x}(k+1) = \Phi \mathbf{x}(k) + \Gamma \mathbf{u}(k)$$

Taking z - transform on both sides of difference equation

$$\sum_{k=0}^{\infty} \mathbf{x}(k+1)z^{-k} = z \left[\sum_{k=0}^{\infty} \mathbf{x}(k)z^{-k} - \mathbf{x}(0) \right]$$

$$= \Phi \left[\sum_{k=0}^{\infty} \mathbf{x}(k)z^{-k} \right] + \Gamma \left[\sum_{k=0}^{\infty} \mathbf{u}(k)z^{-k} \right]$$

$\mathbf{x}(z)$ $\mathbf{u}(z)$

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What we are interested in these pulse transfer function. And this is where we were in the last lecture, this is what I wanted to. So I said the reason why we wanted to introduce the Z-transforms is because we want to convert difference equations into algebraic operators or transfer function matrix, that is what it would be okay. here instead of Laplace transfer function matrix it will be a Z-transfer function matrix.

What I have done here is I am starting with this difference equation and I am taking Z-transform on both the sides. If you see here, I am taking Z-transform on both the sides okay.

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z Transforms : Properties

Linearity

$$Z[\alpha f(k) + \beta g(k)] = \alpha Z[f(k)] + \beta Z[g(k)]$$

Time Shift

$$Z\{g^{-n} f(k)\} = z^{-n} f(z)$$

$$Z\{g^n f(k)\} = z^n \left[f(z) - \sum_{j=0}^{n-1} f(j) z^{-j} \right]$$

Initial Value Theorem

$$f(0) = \lim_{z \rightarrow \infty} f(z)$$

Final Value Theorem
 If $(1-z^{-1})f(z)$ does not have any poles on or outside the unit circle, then

$$\lim_{k \rightarrow \infty} f(k) = \lim_{z \rightarrow 1} (1-z^{-1})f(z)$$

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I am just going to use this time shift formula, the one which is the second one, I am going to use this formula here. In this particular case I am taking Laplace, I am taking Z-transform of X_{k+1} , X_{k+1} would involve here X_0 okay.

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Pulse Transfer Function Matrix

$$\mathbf{x}(k+1) = \Phi \mathbf{x}(k) + \Gamma \mathbf{u}(k)$$

Taking z - transform on both sides of difference equation

$$\sum_{k=0}^{\infty} \mathbf{x}(k+1)z^{-k} = z \left[\sum_{k=0}^{\infty} \mathbf{x}(k)z^{-k} - \mathbf{x}(0) \right]$$

$$= \Phi \underbrace{\left[\sum_{k=0}^{\infty} \mathbf{x}(k)z^{-k} \right]}_{\mathbf{x}(z)} + \Gamma \underbrace{\left[\sum_{k=0}^{\infty} \mathbf{u}(k)z^{-k} \right]}_{\mathbf{u}(z)}$$

When $\mathbf{x}(0) = \bar{\mathbf{0}}$ we have

$$z\mathbf{x}(z) = \Phi \mathbf{x}(z) + \Gamma \mathbf{u}(z)$$

Rearranging $[z\mathbf{I} - \Phi]\mathbf{x}(z) = \Gamma \mathbf{u}(z)$

$$\Rightarrow \mathbf{x}(z) = [z\mathbf{I} - \Phi]^{-1} \Gamma \mathbf{u}(z)$$

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If I just use that formula and come up with the Z-transform I get summation K going from Z to ∞ , I take the $\sum_{k=0}^{\infty} \mathbf{x}(k)Z^{-k}$, so this is nothing but $\mathbf{x}(z)$ and you have this term $\mathbf{x}(0)$ which is appearing, and I am taking Z-transform with the right hand side. So if I actually combine this now, if I combine this and make one more assumption that initial state, initial perturbation at time 0 is 0 which is usually the case when you find out a transfer function matrix.

Whether it is in continuous domain or in Laplace domain, or in Z domain. A usual assumption is that initial state is 0 with that you will get this transfer function matrix. Here all the competency here this term is nothing but $\mathbf{x}(0)$, I am taking $\mathbf{x}(0)=0$. So this term here collapses to $z \mathbf{x}(z)$, right hand side is Φ times $\mathbf{x}(z)$, and Γ times $\mathbf{u}(z)$ okay. So this is just the next step just using the definition of Z-transforms okay.

Then I will just rearrange, remember this Φ is a matrix, so $z\mathbf{I} - \Phi$ times $\mathbf{x}(z)$ $= \Gamma \mathbf{u}(z)$ and this gives me a relationship between the state and $\mathbf{u}(z)$. When you derive a transfer function matrix your purpose is to come up with relationship between input and output, I want to eliminate the state okay.

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Pulse Transfer Function Matrix

$$y(k) = Cx(k)$$

Taking z transform on both the sides

$$\underbrace{\left[\sum_{k=0}^{\infty} y(k)z^{-k} \right]}_{y(z)} = C \underbrace{\left[\sum_{k=0}^{\infty} x(k)z^{-k} \right]}_{x(z)}$$

$$\Rightarrow y(z) = Cx(z)$$

Combining $x(z) = [zI - \Phi]^{-1} \Gamma u(z)$ with $y(z) = Cx(z)$
we have


$$y(z) = \left(C[zI - \Phi]^{-1} \Gamma \right) u(z) = G(z)u(z)$$

Pulse Transfer Function

$$G(z) = C[zI - \Phi]^{-1} \Gamma$$

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So I am going to look at this relationship Y are the measured outputs and X are the states, C is the matrix that relates measured outputs with the states, or perturbations in the measure of could be the perturbations in the states. And then if I just get Z-transform of both the sides I get $y(z) = cx(z)$ it is a straightforward, anyone hear about this, I am just applying a definition of Z-transform.

Now I am going to combine these two results, I am going to eliminate X, I want to have a relationship between measured outputs and manipulated inputs okay. So what you get here is this matrix $C(zI - \Phi)^{-1} \Gamma$ okay, again you will notice that this is very, very similar to what we have for U transforms okay. So shift and get a transform, this is very, very similar and you get $g(z) u(z)$, this is called as a pulse transfer function again same thing.

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Example: Quadruple Tank System

Pulse transfer function model
Sampling Time (T) = 5 sec

$$\begin{bmatrix} h_1(z) \\ h_2(z) \\ y(z) \end{bmatrix} = \begin{bmatrix} \frac{0.2}{z-0.9233} & \frac{0.01138z+0.01034}{z^2-1.734z+0.749} \\ \frac{0.006045z+0.005614}{z^2-1.793z+0.8009} & \frac{0.1528}{z-0.9462} \end{bmatrix} \begin{bmatrix} v_1(z) \\ v_2(z) \\ u(z) \end{bmatrix}$$

G(z)

Student question: How does one select sampling interval for model discretization?

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While if I do it for quadruple tank system, I will get this transfer function matrix between two level perturbations H1 and H2 and 0.2 voltage input perturbations okay. So these are my two, now just remember right now what we are doing is going through developing a control relevant model starting from a mechanistic model, starting from a first principle model or a group of model.

You have a good model which is coming from physics or mixture of physics and correlations. And then we are deriving that model to come up with this control relevant model, this model is control relevant model, I can use this for controller synthesis okay. yeah, sampling time typically you choose based on what is called as, you know turbulent frequency or the fastest frequency in a signal okay that you have.

Now what is the fastest frequency in a signal time, you have to have some oplyary idea about how fast your particular system behaves okay. So one, there are multiple ways of choosing a sampling time one way is that you find out the smallest time constant, you have to send what a time constant is yeah. So find the smallest time constant, take one tenth of that or you find out the settling time, you know what is a settling time, you do a step change and find the settling time and take 100th of the settling time.

So here I have chosen five seconds as one tenth of your shortest sampling, the shortest smallest time constant okay. Actually the tendency in the industry is very, very small sampling time. Well it is not required okay, it will tend to sample temperature for this at every one second. Where the

thing is going to happen for a minute okay. So actually you should chosen sampling time based on the response time of the system itself okay.

So here five seconds is because the smallest time constant in this particular system is about 50, so I have taken one tenth of that probably okay. You can find out good discussion about the choice of sampling time in Franklin and Powell or in Astram and Wettenmark okay.

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Example: Quadruple Tank System

Pulse transfer function model

Sampling Time (T) = 5 sec

$$\begin{bmatrix} h_1(z) \\ h_2(z) \end{bmatrix} = \begin{bmatrix} \frac{0.2}{z-0.9233} & \frac{0.01138z+0.01034}{z^2-1.734z+0.749} \\ \frac{0.006045z+0.005614}{z^2-1.793z+0.8009} & \frac{0.1528}{z-0.9462} \end{bmatrix} \begin{bmatrix} v_1(z) \\ v_2(z) \end{bmatrix}$$

$y(z)$ $G(z)$ $u(z)$

Developed using discretization of linearized mechanistic model

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So what we are dropped here that we come back what we have got here we have to eliminated the state variables there are four step and there are four levels, now this transfer function matrix relates only measure that is with manipulated inputs okay it does not say anything about unmeasured levels okay.

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Time domain difference Equation

$$y(z) = \frac{b_1 z + b_2}{z^2 + a_1 z + a_2} z^{-d} u(z) = \frac{b_1 z^{-d+1} + b_2 z^{-d}}{1 + a_1 z^{-1} + b_2 z^{-2}} u(z)$$

↕

d = dead time

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Now I would go back and relate to time domain okay, so you should be very, very comfortable going back from time domain to Laplace domain or Laplace domain to time domain or zee domain to time domain to z domain and so on, okay you should go back and these are only representations it is only one model which has been represented through move on which being used through different filters or different you know different inspects it specific thing ultimately so I want to show that this model.

This is a model between some wide and some I am picking up copy this right now we will say that say H , H_1 B_2 or H_2 V_1 and so on I am just saying this that one general transfer function between some how to write okay if you get some how to write and some into let us assume that there is a transfer function is given by $B_1 z + B_2$ upon $z^2 + a_1 z + a_2$ or else 1 more time of here and here okay $z - b$ okay now this $z - b$ actually represents time delayed or dead time or other what is a dead time.

How many of you know about what is a dead time everyone knows dead time is the time required for you know it has different interpretations in different context it could be time with requires of actual terms to start doing up will give a signal it could also mean that I replied for the measurement to reach the computer that d when the measurement then have relevant temptations, so a time delay of d samples the model for that this tells out to be z^{-d} okay if I have a dead time of g samples.

The d samples then the model is z^{-d} so I have combined this model which has a time delay of d samples and then I get this model is z^{-1} I just want to convert it that into time domain so I am cross multiplying and then you take z inverse to z inverse to write the z inverse we were going to compute to integrate there you just go back using the formula that time shift if you see this formula you will see that it is very easy to go back to time domain difference equation okay, so here z^{-1} simply differs $y_k - u_{k+1}$ then z^{-2} you operating on z or z^{-d-1} operating of u .

Simply becomes $k - d - 1$ okay k is the current I know that k is not parent time $k -$ while in $k - 2$ and so on, okay so I get this linear difference equation in model starting from the original transfer function model is it clear when you do this difference equation model, I have written it as current equal to.

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Time domain difference Equation

$$y(z) = \frac{b_1 z + b_2}{z^2 + a_1 z + a_2} z^{-d} u(z) = \frac{b_1 z^{d+1} + b_2 z^{d+2}}{1 + a_1 z^{-1} + a_2 z^{-2}} u(z)$$

d = dead time

$$[1 + a_1 z^{-1} + a_2 z^{-2}] y(z) = [b_1 z^{-d+1} + b_2 z^{-d+2}] u(z)$$

Taking Inverse z transform on both sides, we get

$$y(k) + a_1 y(k-1) + a_2 y(k-2) = b_1 u(k-d-1) + b_2 u(k-d-2)$$

Linear Difference Equation Model

$$y(k) = -a_1 y(k-1) - a_2 y(k-2) + b_1 u(k-d-1) + b_2 u(k-d-2)$$

where $k = 2, 3, 4, \dots$

Initial Conditions : $y(0) = y(1) = 0$

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Something in a past and the reference side is write a as parent so what does it tell you it tells you that the new measurement is refer that to the past measurement and new inputs which are coming, so what about new inputs $u_k - d$ whether time delay okay it is a time delay which means if I make a change in the input right now is going to reflected after sometime what is happening now is the effect of something that is happened in the past, okay there is something going to happen in the past so this tell you that, that correct input u_k is not going to influence by k or $y_k + 1$.

If the input in the past is influencing that current measurement okay that is because of the d okay and then this is my difference equation model okay to solve this difference equation model is not call difficult if I go u is the input sequence in put is something which is given to you either by a controller or by operator.

If you have rotating the plant you are changing the input you know what is u okay and given u I can solve this linear difference equation matching in time if I know value at instant you know 0 and 1 I can find out value at instant 2 if I know at 1 and 2 I can find out 3 I can go often in time this is a difference equation as k increases we will get.

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Practical Difficulty and Remedy

Practical Difficulty
A reliable mechanistic model may not be available for the system under consideration.

Instead of starting from well developed nonlinear mechanistic model, can we estimate parameters of linear perturbation directly from operating data?

Remedy

1. Inject known input perturbations in the system
2. Record measured outputs generated in response to the perturbations
3. Estimate dynamic model parameters using optimization

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Okay so far so we got this model we started that the mechanistic model b linearized it use tell us the expansion then we got a states specks model a discretized that if you go to and industry and so that well where is the mechanistic model you know people might laugh at you unless we are going to some variety lab there away what is happening okay, what is a mechanistic model and why it is required, so you go to a slow and or you go to some lab of you know where at walls development is going on.

They would of course know what we are talking about in that either or a general industry if you go and say what I want a mechanistic model for the system we would get everything you will not have mechanistic model, now what to do so the question is well if I go to a industry I have the system to be controlled I do not have a mechanistic model can I simply developed model from

data I can do well I have to some experiment with this system okay, well I have to tweet the system you allow to make the system.

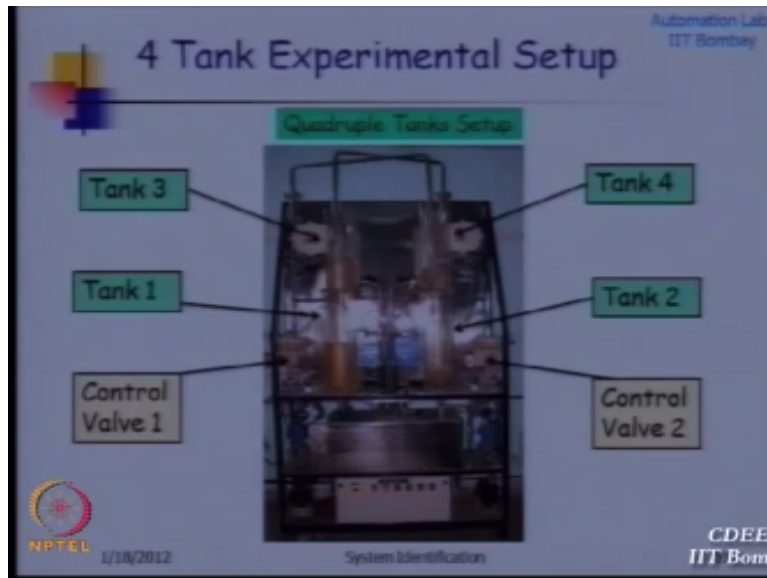
It is like the example that I keep giving this the model we developed for a car when we get we start to driving a new car or a new vehicles, so notice so you know we the manipulate variables are accelerator and the break, so we played with it know initially we slightly increase that when I see how it goes redundant, we apply the break and see after distance it stops and then we develop a model which is interrupted the output is the speed or you know breaking distance and there is input is my you know.

The pressure at to come the accelerator or the pressure at, so given my inputs and my outputs are you know + speed or in the breaking distance, so primarily these kind of models I think about to play with this system you can developed to drive my car but I do not have a model coming from physics for the car, so can I still to work with it yeah, so my approach from now one it is going to be like this well I am going to inject perturbations into the system okay I do not know with this principle model.

And I still going to get going to the controller design okay, I cannot say that well call engineer who will model this for me and then I start, I do not know daily from model using some simple to its and you know what I am going to do is I am going to record the inputs that even and I am going to return out measurement that I have okay, and then between this input and output I want to fit the model okay I want to fit a model just like if it is a correlation I can fit a differential equation I come to this difference equation.

Okay it is now necessary that you will have a algebraic correlations between variables okay you can have you know some system is there you have some input some output you can develop you know differential equation or a curious strict model which is a differential equation have a difference equation.

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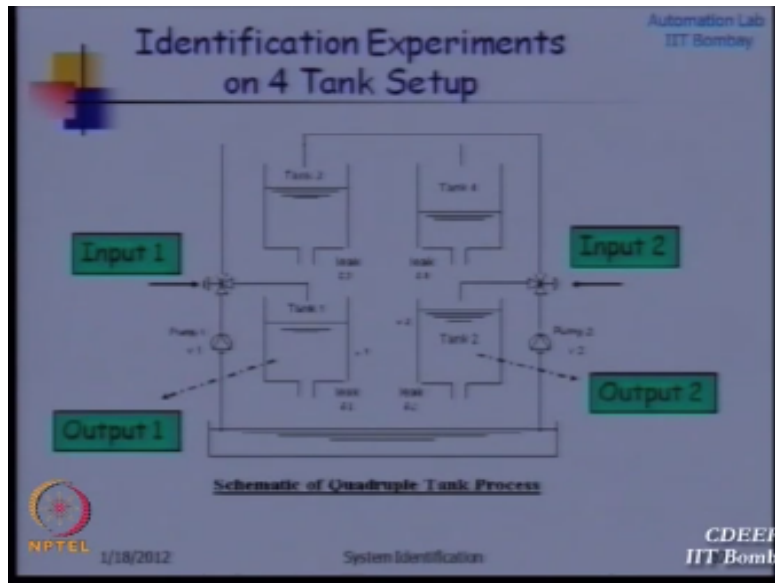


Okay so let us look at this what would the time set up and I have this straight up in my land okay, there are four times you can see them and where we saw this in the first few lectures in that two times start from each other and you can see here this is the control valve part of the flow goes to this fine remaining part of the flow goes to this, this stand, so goes to this stand so tank 1 and tank 4 get you know input that is coming from this controls there and time few more time 3 we get flow which is coming from this control work okay.

So let us assume that I do not have a model probably from physics for the system, but it is connected to my computer I can change the board okay experiment that I am going to do is I am going to change the wall I am going to protect the wall okay.

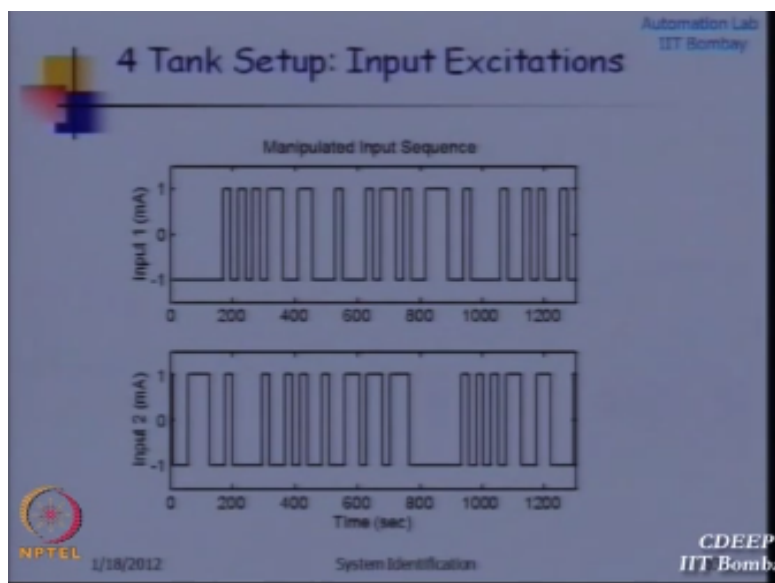
There are many questions do I part of that more a time we have both that valve simultaneously while if you want to say I would get a both the valves simultaneously we find it is difficult because if too many things are changing simultaneously how do you model then not that difficult as we will see, so okay so this is.

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A schematic diagram of the same set up okay and full times where two inputs and I have two outputs, two outputs are still there it is right, and now going to measure all 4 levels and we want to measure only level 1 and level 2 in times fall in time to okay.

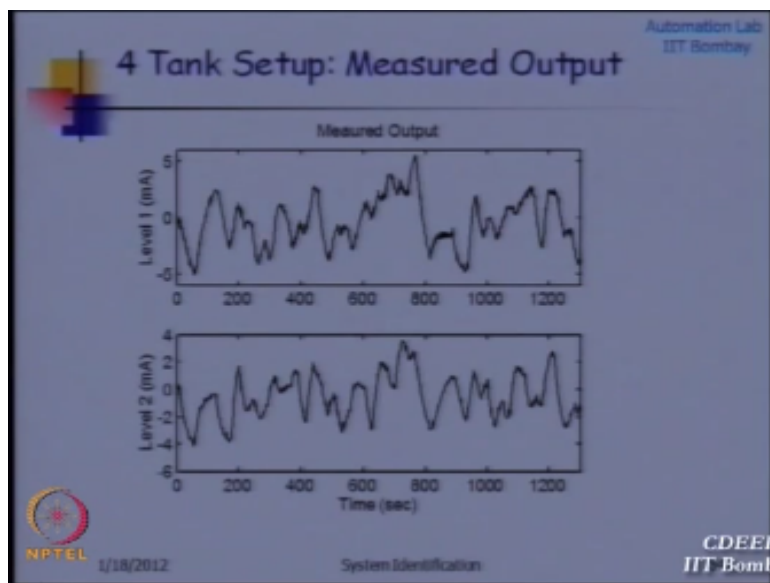
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Now I actually converted the experimental my okay so what I read this I took initially the system to a study state and in the rejected part of excitations 0 here is not really 0, 0s 12 millions as this

plotted the parts of the inputs, so I have given I have both the system to a steady state okay by giving 12 million which to both the control valves the level has complete study stat okay and then I inject perturbations I would just plotted here the perturbations you see the perturbations in by 1 and valve 2 how did the system respond okay.

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These are the measured outputs we have to measure the outputs again perturbations from the study state level okay, all of these data which means for this particular system I have plate this system I have you know manipulated the valves according to certain.

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Experimental Data for Modeling

Experimental data collected

Measured Outputs
 $Y_N = \{Y(0), Y(1), \dots, Y(N)\}$

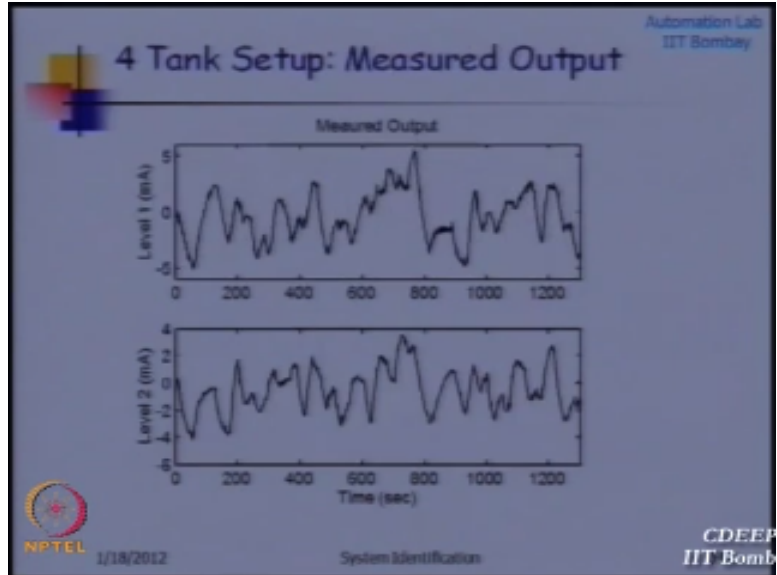
Known and/or manipulated Inputs
 $U_N = \{U(0), U(1), \dots, U(N)\}$

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According to certain scheme this particular signal which I have given here is called as pseudo random binary signal and randomly changing between two values +1 a milli amp to -1 milli amp, okay my system the control will input between 4 to 20 milli amps okay, if you give 20 milli amps the valve is full open if you give 4 milli amps the valve is full closed okay, I am first taking the opening the valves to 12 milli amps, so 12 milli amps is my base level okay.

At 12 milli amps I wait till the system levels come to steady state the system is perfectly at the steady state at 12 milli amps okay. Now we start my perturbation studies okay, and then around third milli amps so this when you say here plus or minus 1 it actually means I am perturbing the input to the valve from 12 to 13 and 11 for each of the valves, okay this is the perturbation are injected to the system and how does the levels react.

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Levels have reacted like this, this is the perturbation in the level around the steady state okay.

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Experimental Data for Modeling

Experimental data collected

Measured Outputs

$$Y_N = \{Y(0), Y(1), \dots, Y(N)\}$$

Known and/or manipulated Inputs

$$U_N = \{U(0), U(1), \dots, U(N)\}$$

Operating
Steady State
 $= (\bar{Y}, \bar{U})$

Generate Perturbation Variables

Measured Outputs

$$Y_N = \{y(0), y(1), \dots, y(N)\}$$

Known and/or manipulated Inputs

$$U_N = \{u(0), u(1), \dots, u(N)\}$$

$$y(k) = Y(k) - \bar{Y}$$

$$u(k) = U(k) - \bar{U}$$

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So what I have done actually that we put it mathematically what I have done is our collected data for y_0, y_1, \dots, y_N , Y capital is the absolute value U is the absolute value of the input, absolute value of the input is between + or - 11 volts, + or - 11 amperes milli amps and the level is measured again in terms of milli amps okay, the level is measured between milli amps. Now I am going to develop the input output model okay, now what is input here, the input here is the current input that goes to the control valve very, very important input right now is not really the flow okay.

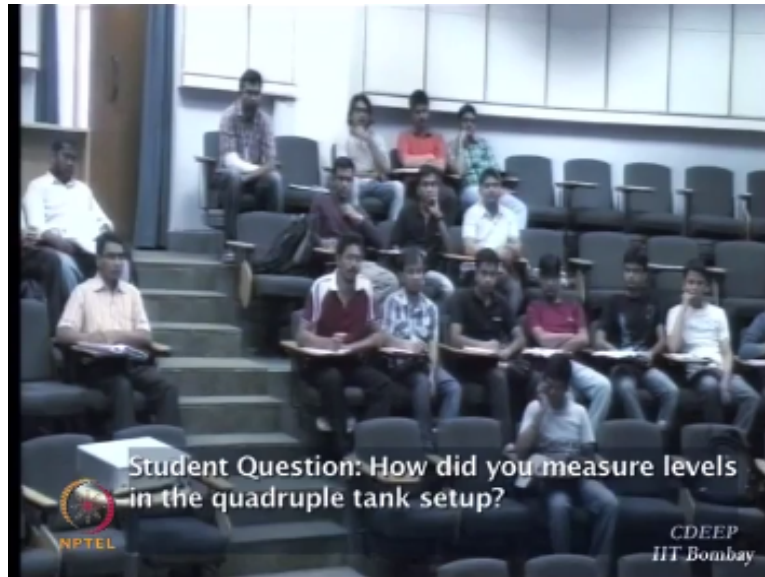
So whatever is going out of my computer is the input whatever is coming to the computer is the measurement so measurement includes level dynamics sensor dynamics everything okay, the measured inputs that control you know the manipulate input here is the value which is send out of the computer which means process includes valve dynamics posses dynamics, sensor dynamics everything, okay.

It is not just okay, then well I should know what is my operating steady state I can take a measurement initially what is the steady state level and what is the steady state input I told you in this cases 12 milli amps input is the steady state input so \bar{U} is 12 milli amp/ milli amp and \bar{Y} how to find out experimentally whatever I get, I subtract that so I define this negation variables and finally I generate perturbation inputs what I plotted here is this perturbation inputs okay.

I have collected data which is the data collected is not in terms of perturbation data collected that is what variables. For the purpose of modeling I am going to converted into perturbation variables why, because they are going to develop up a model using Taylor's roxy perturbation,

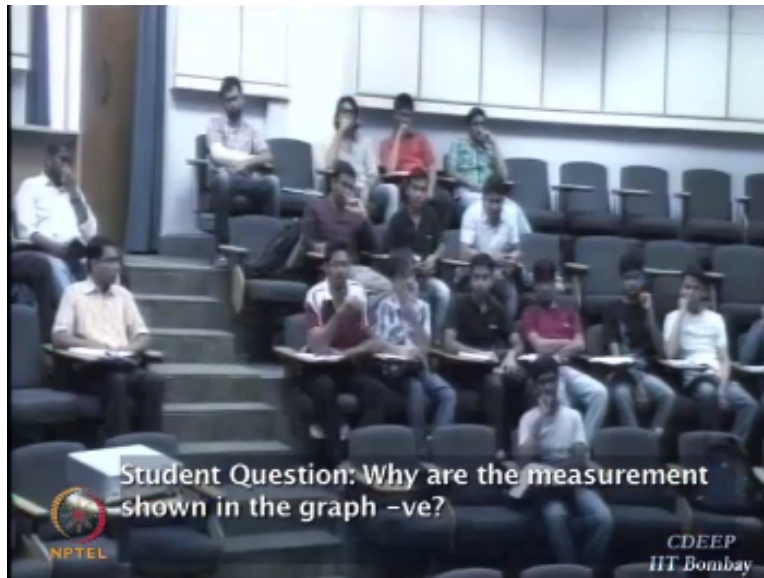
Taylor's roxy perturbation talks about perturbations in the input to perturbation in the output okay, yeah.

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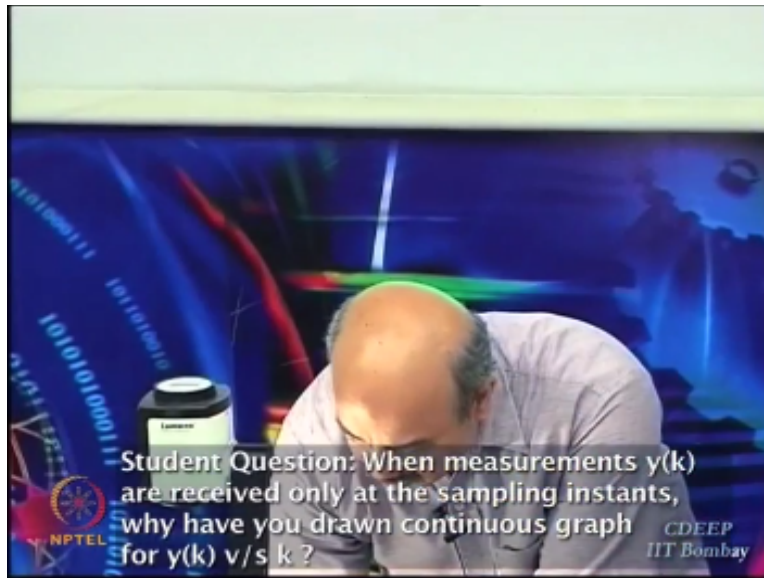
In this case we have for the level measurement we have differential equation transmitters okay, which convert the 0 to 100 cm water column into 4 to 20 milli amps so 100 cm water column is or 60 cm water column I think 60 cm water column is 20 milli amps 0 cm water columns 4 milli amps, so that is our and then that transmitter is connected to my analog to digital convertor okay, which is giving me measurements at every five second interval okay. So every five seconds I get one measurement from.

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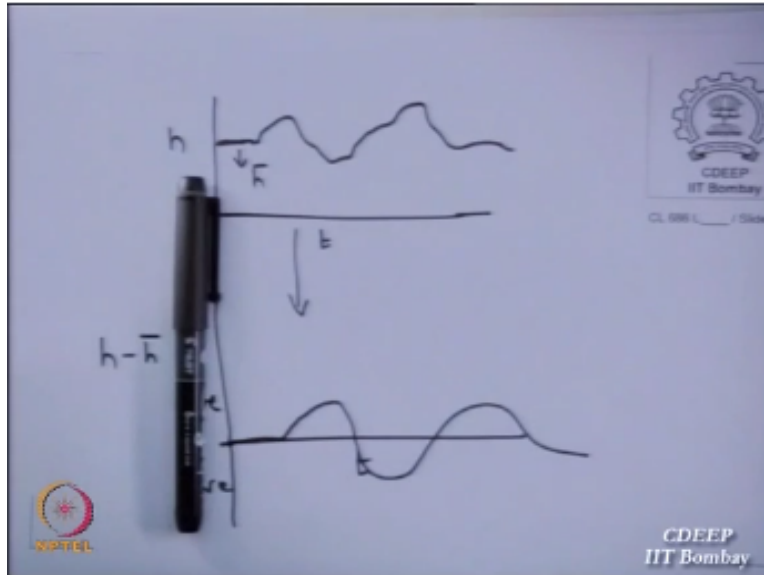


Because it is portability, it is deviation so see here my original output is not negative values but if I take a steady state okay.

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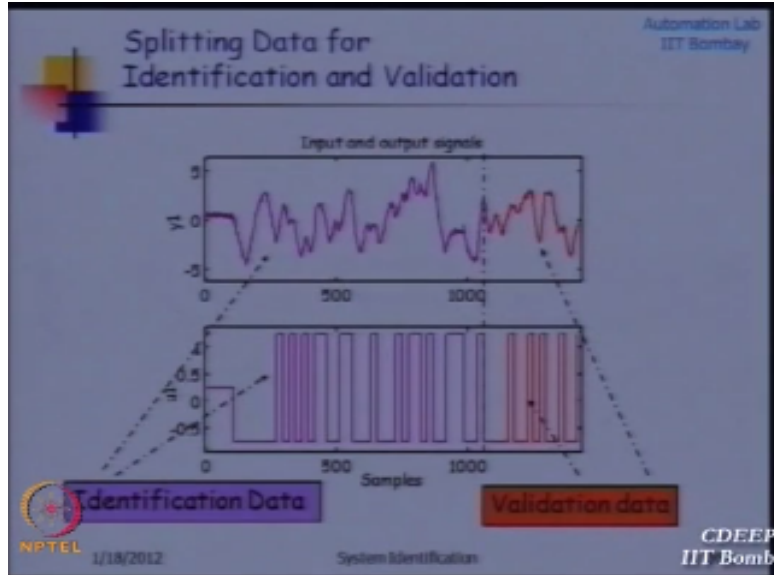


See where original output is h versus time is something like this so let us say my initial unit is at steady state then it starts changing, okay so this is the steady state. Now if I plot this in terms of you know h so let us call this point as \bar{h} , so if I plot $h - \bar{h}$ versus time then it will look like this whatever this is negative this is positive okay, but original signal is not like that original signal is you know let us say it is varying between some 10 milli amps to 14 milli amps or something like that, okay is varying between 10 to 14 milli amps.

I removed the mean value or the steady state value then that gives me signal which is positive and negative okay, is everyone clear on this. you get perturbation signals which can be positive, negative original signal may or may not be positive or negative it depends up on the system okay. If you have induction motor you may have currents which are negative or positive but if you have temperature, temperature is not good to be in, I mean temperature can be negative if you take depended on the scale but something is like concentration is never going to be negative, okay.

But perturbation concentration can be negative because there is perturbation around some mean value okay, so that time be negative so okay, yeah. No, I should now be drawing output as a continuous signal I should be drawing it to the discrete points okay, it is only that I will connect the discrete points okay, so idea of their drawing this would be just points. There are 250 measurements there should be 250 points okay, it is just for the sake of you know, so look at here this is my initial steady state, okay, yeah.

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So this is my initial steady state because is at 0 I have subtracted this steady state value and then this is the perturbation around the steady state these are the perturbation inputs okay.

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Quadruple Tank: Grey Box Linear Model

Let us treat elements of matrices in the discrete
Linear state space model as unknowns

$$\Phi = \begin{bmatrix} \alpha_1 & 0 & \alpha_2 & 0 \\ 0 & \alpha_3 & 0 & \alpha_4 \\ 0 & 0 & \alpha_5 & 0 \\ 0 & 0 & 0 & \alpha_6 \end{bmatrix} \quad \Gamma = \begin{bmatrix} \beta_1 & \beta_2 \\ \beta_3 & \beta_4 \\ 0 & \beta_5 \\ \beta_6 & 0 \end{bmatrix} \quad \mathbf{C} = \begin{bmatrix} \gamma_1 & 0 & 0 & 0 \\ 0 & \gamma_2 & 0 & 0 \end{bmatrix}$$

Note: We are assuming that structure of matrices is
known i.e. we know where zero and non-zero elements are

Define parameter vector

$$\Theta = [\alpha_1 \quad -\alpha_6 \quad \beta_1 \quad -\beta_6 \quad \gamma_1 \quad \gamma_2]^T$$

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Well, now what I can say is let us go back to this, let us go to the model that we have developed earlier and in connect, we develop this model from eagerization and finally yeah.

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Computation of Model Matrices

When matrix A is invertible $\int_0^T \exp(A\tau) d\tau = [\Phi - I]A^{-1}B$

Quadruple Tank System
Discrete Time State Space Model Matrices
Sampling Time $T = 5$ sec

$$\Phi = \begin{bmatrix} 0.9233 & 0 & 0.1813 & 0 \\ 0 & 0.9462 & 0 & 0.1493 \\ 0 & 0 & 0.8112 & 0 \\ 0 & 0 & 0 & 0.8465 \end{bmatrix}$$

$$\Gamma = \begin{bmatrix} 0.4001 & 0.02276 \\ 0.01209 & 0.3055 \\ 0 & 0.2159 \\ 0.1438 & 0 \end{bmatrix} \quad C = \begin{bmatrix} 0.5 & 0 & 0 & 0 \\ 0 & 0.5 & 0 & 0 \end{bmatrix}$$

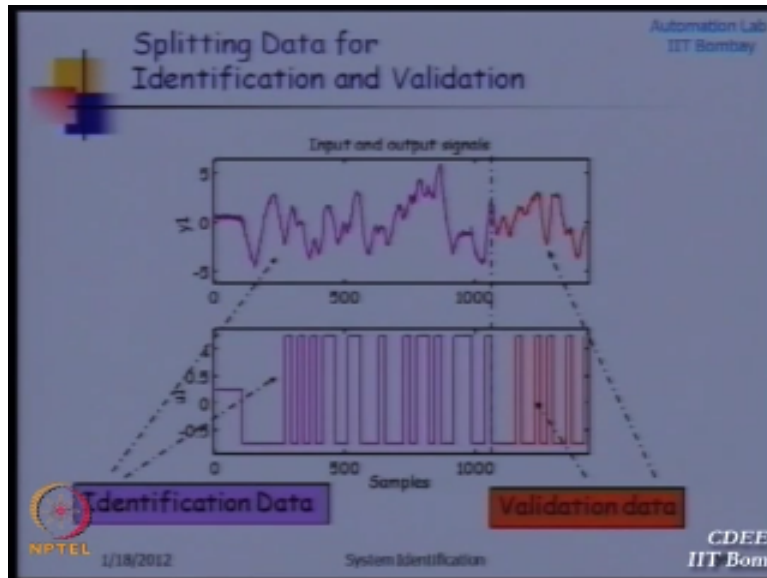
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Finally I got this matrix okay, I want to do look at this matrix closely okay, there are certain elements which are 0 here why they are 0, because they decoupled there is no relationship that is why those are 0, okay. There are only few elements in fact if you look at Φ matrix there are only six elements which are non-zero right, the six elements how many it is a matrix which is 4x4 only six elements no not six, yeah only six elements are no zero okay.

Out of 16 six elements are no zero okay, look at γ matrix γ matrix has two elements which are o whatever sampling interval we choose for this particular system structurally these matrices I am going to look same then I am going to look different, is it clear. Structurally these matrices are going to look exactly like this whatever we will do same is that case for C matrix I am measuring only two levels okay, in that only two elements I am going to be non zero remaining are going to be 0, okay.

So what if I treat these sic elements here as unknowns to be estimated from data okay, can I do that so what I am going to do now.

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I have this data with me okay, I would just plotted here Y_1 , U_1 there will be data for Y_2 , U_2 okay, I have this data for two inputs two outputs and I am just showing here one portion of it okay, so I have data for Y_2U_2 .

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Quadruple Tank: Grey Box Linear Model

Let us treat elements of matrices in the discrete Linear state space model as unknowns

$$\Phi = \begin{bmatrix} \alpha_1 & 0 & \alpha_2 & 0 \\ 0 & \alpha_3 & 0 & \alpha_4 \\ 0 & 0 & \alpha_5 & 0 \\ 0 & 0 & 0 & \alpha_6 \end{bmatrix} \quad \Gamma = \begin{bmatrix} \beta_1 & \beta_2 \\ \beta_3 & \beta_4 \\ 0 & \beta_5 \\ \beta_6 & 0 \end{bmatrix} \quad C = \begin{bmatrix} \gamma_1 & 0 & 0 & 0 \\ 0 & \gamma_2 & 0 & 0 \end{bmatrix}$$

Note: We are assuming that structure of matrices is known i.e. we know where zero and non-zero elements are

Define parameter vector

$$\Theta = [\alpha_1 \quad \dots \quad \alpha_6 \quad \beta_1 \quad \dots \quad \beta_6 \quad \gamma_1 \quad \gamma_2]^T$$

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Okay, now I am going to say that if I discretized a model coming from physics okay, it has a certain structure and that structure is given by this you know matrix these three matrices. Now what do I mean by structure is given by three matrices I have put 0 there I know there going to be 0 okay, and an events which call me or go of determine through linear addition of a model I am going treat them as a unknowns okay.

So I am treating $\alpha_1, \alpha_2, \alpha_3, \alpha_4, \alpha_5$ and α_6 the six unknowns in five matrix the six unknowns in γ matrix the two unknowns in C matrix okay, so now question is can I estimate these 6+6, 12+2 14 parameters only from data without worrying about starting from physics coming with a non linear differential equation model nothing. But starting from that model if I had a clue of what that model is I can come up with this structure, okay.

If I want what is the model from physics is okay, I can come up with this structure I am going to call this model as a grey box linear model, why grey box because some information from first principle has been used, but I do not have parameters of the first principle model okay, but I have used the first principle information to arrive at a structure of this linear perturbation model, okay. The structure has been formed from physics but the parameters values are unknown and I am going to estimate the model parameter values from data so how do I do that, okay.

Let me define a vector called θ this θ has 14 elements α_1 to α_6, β_1 to β_6 and γ_1 and γ_2 all 14 elements put into this θ vector I am going to use least square estimate. Do you use you know least square estimation if it cure fitting okay, instead of curve fitting I am going to do a

differential equation fitting or a difference equation fitting, okay there is only the difference between what you know and what are going to do now, okay.

I am going to fit a difference equation linear difference equation into this data of Y_1 Y_2 and U_1 U_2 , okay treating these 14 parameters as unknowns. How do you do this if you are given some data and if you have look fit a line okay, what do you do. Do not tell me I use excel and I just click and I get a print that is not the answer what we do? Linear re square estimation remembers what is the linear re square estimation, what you minimize? That are between measurement, predicted estimated output and actual measured output okay so I minimize difference between I minimize the difference between estimated output and the measured output, estimated by what? Estimated by the model okay.

What is the raw way if doing this? You can guess the parameters okay you can guess parameters then for every guess you can generate model estimated model outputs you have measured model outputs you compare the two okay if you think that the fit is not god you revise your estimate and go on doing this till you know the estimated output goes close to the measured output okay so this is what I am going to do next okay I am going to do it through optimization, optimization how to solve the optimization problem I am not going to get in to that in this I am just going to formulate you can solve it using met lap tool box.

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Model Parameter Estimation

Given set $U_N = \{u(0), u(1), \dots, u(N-1)\}$,
 guess for Θ and initial state $\hat{x}(0)$
 we can generate state sequence
 by recursively using linear difference equation

$$\hat{y}(0) = C(\Theta)\hat{x}(0)$$

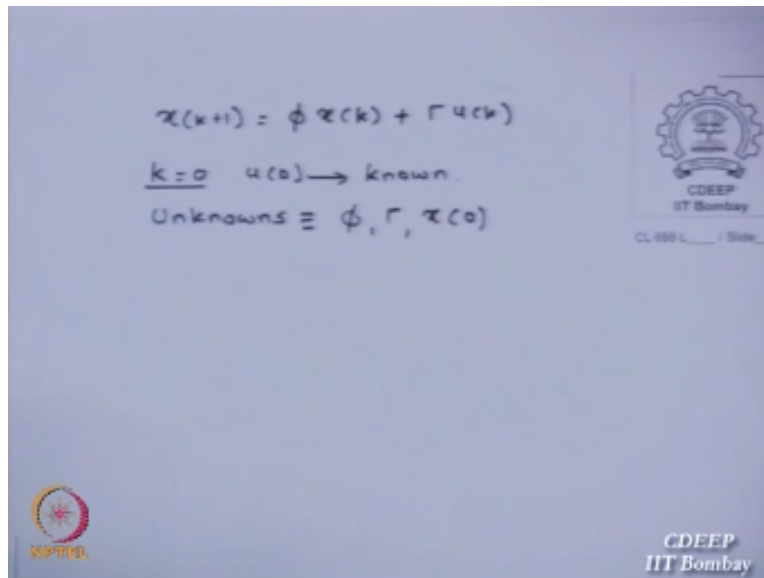
$$\hat{x}(1) = \Phi(\Theta)\hat{x}(0) + \Gamma(\Theta)u(0)$$

$$\hat{y}(1) = C(\Theta)\hat{x}(1)$$

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So let us see how this can be done, now what is known to you the inputs are known to you input sequence is known is you know you are introduce the inputs right you have change the wall position so wall position as a function of time is known to you also know that it is p2 constant okay. So you the wall positions okay, what is not known to me, what is not model?

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So now model is okay this is my model, let us say I am write time 0 okay so at $k = 0$ what is known to me I know u_0 okay, I do not know okay so this is known what are the unknowns? One thing which I do not know is right now is ϕ matrix I do not know what is ϕ matrix so I do guess what I have to guess α_1 to α_6 I have to give x for α_1 to α_6 I have to guess elements of γ , I do not know what is what are the elements of γ right.

I also do not know what is x_0 I do not know x_0 what if I guess all three of them okay what if I guess all three of them let us see what we can do.

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Model Parameter Estimation

Given set $U_N = \{u(0), u(1), \dots, u(N-1)\}$,
guess for Θ and initial state $\hat{x}(0)$
we can generate state sequence
by recursively using linear difference equation

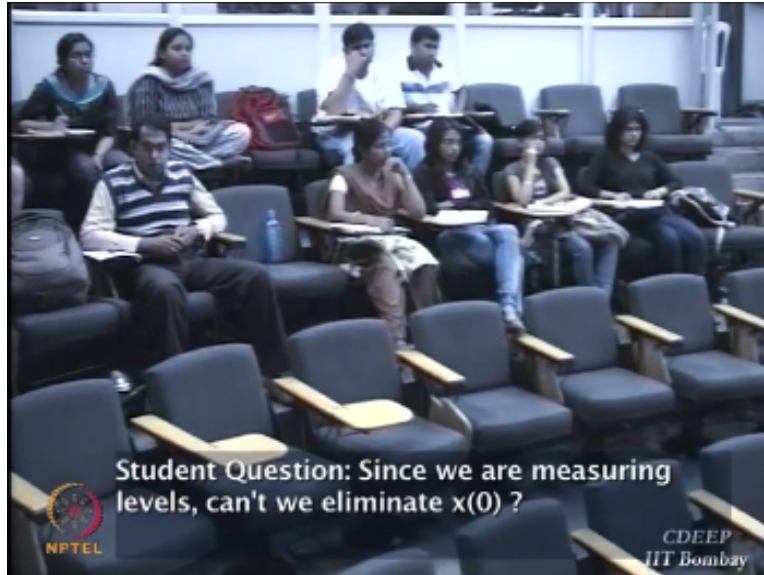
$$\hat{y}(0) = C(\Theta)\hat{x}(0)$$
$$\hat{x}(1) = \Phi(\Theta)\hat{x}(0) + \Gamma(\Theta)u(0)$$
$$\hat{y}(1) = C(\Theta)\hat{x}(1)$$

Student Question: Is there some way by which we can eliminate need to guess the initial state $x(0)$?

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So initial state one way of eliminating is making in a simplistic assumptions that x_0 is 0 you are starting from steady state and x_0 is 0 that is typically done.

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No you cannot eliminate, you can make simplifying assumptions as x_0 is 0 we cannot really eliminate x_0 , but you are not measuring x you are only measuring y so I am only measuring two levels below I am not measuring all the four levels see because y is there because see level transmitter cost okay, a level transmitter a d to b transmitter could cost something of the order of a good quality to be transmitter but cost something like 70 to 80000 okay.

So I do not have money to put all four level transmitters okay so I cannot measure x_0 I can measure only two of them I can know initial level foraminant two not for all four so x_0 has to be some of guessed okay some part of it might be measured you can actually put those values other parts we have to guess or make a simplifying assumption initially you are starting from 0 steady state okay and x_0 is 0 they have a two ways okay.

So coming back to this equation if you look here I have given a guess for this θ vector and what is now y_0 y_0 is see I am now make the notation little bit complex because I want to just emphasize on this slide that c is guessed I guess θ then I get c I guess θ then I get ϕ I guess θ then I get γ , okay that is why I have made the notation little complex here, so starting from this guess I know u_0 I have guess this I have guess this I have guess this I can compute x_1 right this is a difference equation.

And then y_1 becomes y_1 becomes $c\theta$, $c\theta$ will have based x_1 bar on a computer here okay so I get y_1 okay. So I got x_1 now using x_1 and u_1 I can estimate x_2 okay and then arching in time now okay I know input sequence I know u_0 u_1 u_2 u_3 u_4 okay just see I have put this little

march above here \hat{y} this is \hat{x} \hat{y} \hat{x}^2 \hat{y} because it is an estimate, you do not know whether it is correct or not these are all estimate, estimate based on your guess θ because your guess θ you have estimated x okay yeah.

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Model Parameter Estimation

Given set $U_N = \{\mathbf{u}(0), \mathbf{u}(1), \dots, \mathbf{u}(N-1)\}$,
guess for Θ and initial state $\hat{\mathbf{x}}(0)$
we can generate state sequence
by recursively using linear difference equation

$$\hat{\mathbf{y}}(0) = C(\Theta)\hat{\mathbf{x}}(0)$$

$$\hat{\mathbf{x}}(1) = \Phi(\Theta)\hat{\mathbf{x}}(0) + \Gamma(\Theta)\mathbf{u}(0)$$

$$\hat{\mathbf{y}}(1) = C(\Theta)\hat{\mathbf{x}}(1)$$

↓

$$\hat{\mathbf{x}}(2) = \Phi(\Theta)\hat{\mathbf{x}}(1) + \Gamma(\Theta)\mathbf{u}(1)$$

$$\hat{\mathbf{y}}(2) = C(\Theta)\hat{\mathbf{x}}(2)$$

Student Question: What is vector theta appearing in these equations?

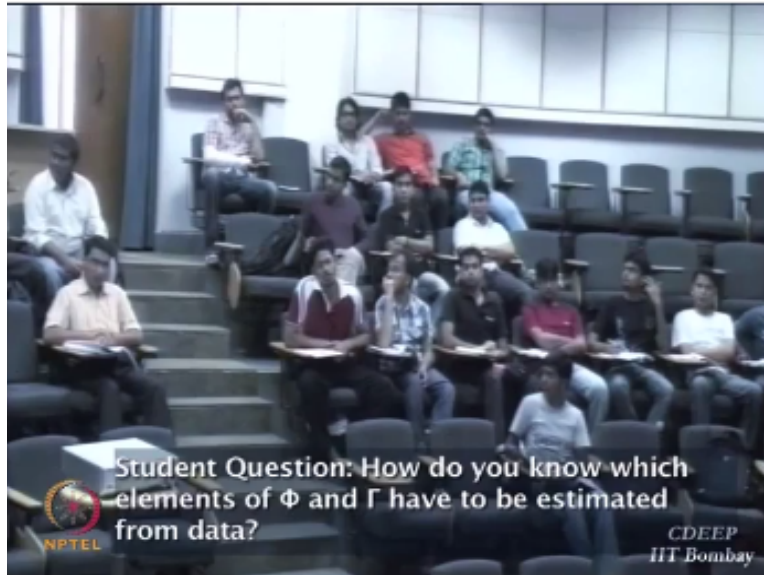
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So θ is this parameters let us go back θ is this parameter side okay θ is this α_1 to α_6 β_1 to β_6 γ_1 to γ_2 so once I guess this look at this slide once I get this ϕ γ and c get defined okay.

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That is because it is coming from physics so I am assuming that I have a model from physics but I do not know it is parameters that I know enough to come up with this structure okay that is why I am calling it gray box okay, afterwards I am going to relax this also I am going to say when I have this data and I do not know anything about the model structure then what that is the next question.

So I am going in a gradual manner you know I am starting from physics I have full model how do I get control the level model okay second is well I have a model but I do not know it is a parameters but I do not know something about the structure then how do I explode it okay, next is well I do not know anything okay then what I do? So three stages okay.

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Model Parameter Estimation

Given set $U_N = \{u(0), u(1), \dots, u(N-1)\}$,
 guess for Θ and initial state $\hat{x}(0)$
 we can generate state sequence
 by recursively using linear difference equation

$$\hat{y}(0) = C(\Theta)\hat{x}(0)$$

$$\hat{x}(1) = \Phi(\Theta)\hat{x}(0) + \Gamma(\Theta)u(0)$$

$$\hat{y}(1) = C(\Theta)\hat{x}(1)$$

↓

$$\hat{x}(2) = \Phi(\Theta)\hat{x}(1) + \Gamma(\Theta)u(1)$$

$$\hat{y}(2) = C(\Theta)\hat{x}(2)$$

↓

$$\hat{x}(3) = \Phi(\Theta)\hat{x}(2) + \Gamma(\Theta)u(2)$$

$$\hat{y}(3) = C(\Theta)\hat{x}(3)$$

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So any one with me on this I can go on now watching in time for every guess of parameters and every guess and every time I guess parameters I also get x_0 okay I can generate complete state sequence right, if I can generate state sequence I can also estimate y okay and then well the conventional v_2 estimation what I want to minimize I want to minimize difference between y measured and y estimated I defined in error ϵ which is difference between y measured and y estimated okay.

And now I have to minimize some of this square of errors, troubles ϵ is a vector what do I do? Take the norm take two norm again take a vetted norm that was I can defined a vatic matrix w I can take a vetted norm, vetted norm is many times you know you will have this y consisting of variable of different magnitudes one could be pressure the other could be temperature third could be you know some concentration the physical values will be completely different.

If you just take some of the square of errors you know pressure values will be Newton per meter square 10^5 and you know concentration might been fraction and you will have problem numerical problems okay so we can use the waiting matrix to balance elements of this and then what I am going to do is to solve this parameter estimation problem as an optimization problem it is an optimization problem okay,

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Model Parameter Estimation

Define prediction error Let W = Diagonal weighting matrix with +ve elements

$$e(k) = y(k) - \hat{y}(k)$$

Estimate Θ and initial state $\hat{x}(0)$ by solving following optimization problem

$$(\hat{\Theta}, \hat{x}(0)) = \underset{\Theta, \hat{x}(0)}{\text{Min}} \sum_{k=0}^N [e(k)]^T W e(k)$$

Subject to

$$\hat{x}(k+1) = \Phi(\Theta)\hat{x}(k) + \Gamma(\Theta)u(k)$$

$$\hat{y}(k) = C(\Theta)\hat{x}(k)$$

where $k = 0, 1, 2, \dots, N-1$

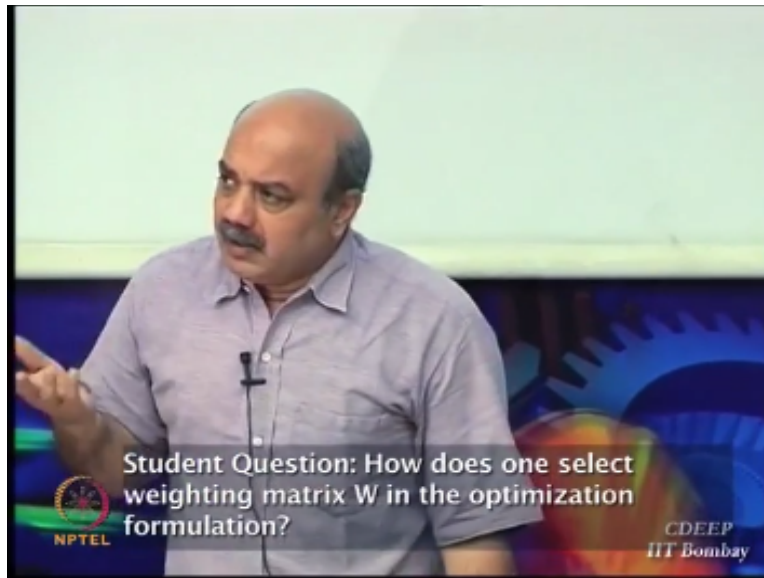
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In which I am going to minimize this objective function this is a objective function we get some of the square of errors because this is you know because this is a vector of taking vetted transpose $w \times$ vector so this will give me a scalar value okay some of this from time 0 to time n I have data 250 points okay I want to minimize this some of the square of errors with respect to θ with respect to x_0 , one simplification I can do is assume x_0 is 0 then it with respect to only θ okay.

This is the optimization problem that I need to solve you can solve this using mat lap tool box you can solve this using any one of the known methods it is enough to understand the formulation you know there are tools to solve this problem, so yeah.

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W matrix is typically decided to balance between different magnitudes and bring them on a same scale okay, so you know you would put it one simple way of doing it is find out the range or variability and then take elements of w matrix inverse of the range see for example if my pressure is changing between you know plus or minus 10^4 you know $+ or - 1 \times 10^4$ then you divide and bring it to $+ or - 1$ variation okay.

So you try to scale it is a scaling matrix okay see because you may have a temperature in your model in you y estimated you may have a temperature value which between you know $+ or - 100$ and pressure is varying between 10^4 to 10^5 you know 10^4 deviation pressure okay if you take just temperature square + pressure square you know the temperature square will get buried it will not be seen, so you scan it in such a way that temperature variation become $+ or - 1$ pressure variation become $+ or - 1$ so you chose w matrix such that you sort of balance numerically the values okay.

Is this optimization formulation clear? I am going to find out these parameters by numerical optimization okay.

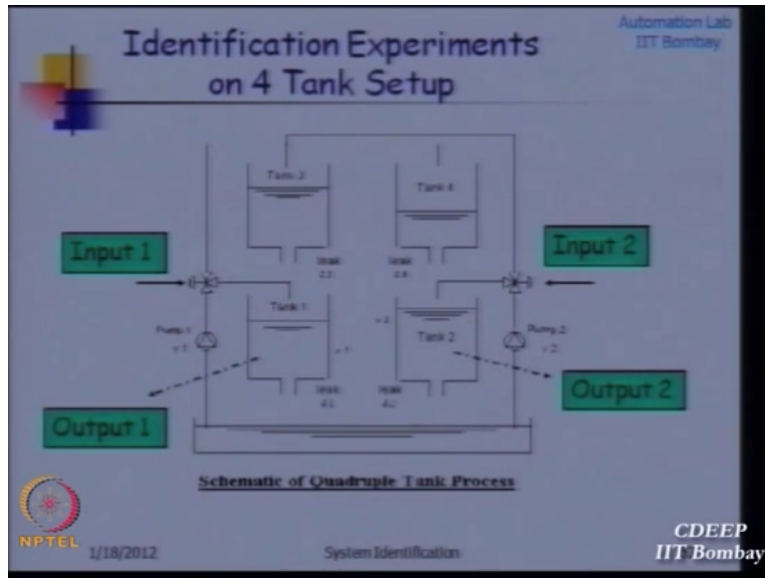
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The slide features a blue background with a white title 'Alternate Approach' at the top left. Below the title, the text reads 'Let us treat elements of q transfer function Matrix model as unknowns'. In the top right corner, it says 'Automation Lab IIT Bombay'. The bottom left corner contains the NPTEL logo and the date '1/18/2012'. The bottom center has the text 'System Identification', and the bottom right corner features the CDEEP IIT Bombay logo.

Well like a like he said how do you know the structure of the matrix okay I do not know such a matrix so I am relaxing even that constraint now I am going little okay now let us look at I do not know the structure of the matrix with let us assume that I know the structure of the transfer function matrix okay.

This can be known because you know first order you know what the first order is in second order transfer function I can know whether between y domain u_1 there is the transfer function is first order or second order see just go back to.

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Let us look at this program okay now between input 1 and type 1 what do you expect the transfer function order to be first order okay same thing between in an output input 2 and output 2 the first order okay what do you expect between output 2 and type 1 it will be second order because the input is going through this type and then going to this dynamics okay.

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Alternate Approach

Let us treat elements of q transfer function
Matrix model as unknowns

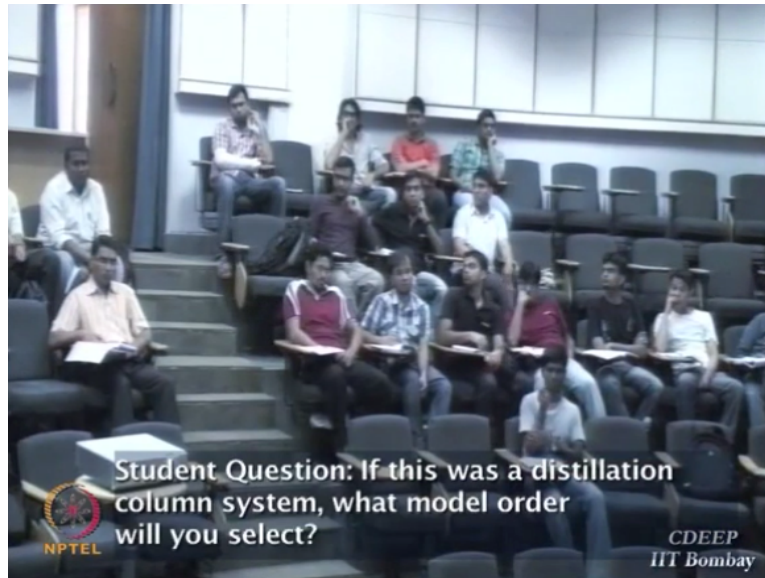
$$\begin{array}{c}
 \begin{bmatrix} y_1(k) \\ y_2(k) \end{bmatrix} \\
 \mathbf{y}(k)
 \end{array}
 =
 \begin{array}{c}
 \begin{bmatrix} \frac{b_1}{q+a_1} & \frac{b_2 q+b_3}{q^2+a_2 q+a_3} \\ \frac{b_4 q+b_5}{q^2+a_4 q+a_5} & \frac{b_6}{q+a_6} \end{bmatrix} \\
 \mathbf{G}(q)
 \end{array}
 \begin{array}{c}
 \begin{bmatrix} u_1(k) \\ u_2(k) \end{bmatrix} \\
 \mathbf{u}(k)
 \end{array}$$

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So now I have come up with these model abstract model with consume parameters is the quadrapation model okay I have come up with this abstract model with unknown parameters just that argue in like this you know this is this is between this and this only an type okay so model should be first order so the title elements of first order you see here y_1 u_1 expose order y_2 u_2 is first order okay.

But y_1 u_2 is second order because it is going to 2 times is simple is derived in this okay dynamics are sensor and neglecting dynamics are control valve so that simplification okay whether 1 should neglected or not difference upon because your judgment of the engineer whether you know this dynamics is negligible that depends upon this, this system okay.

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This is this was a distillation column system what the model order you will select yeah that is the good question with answer that will be later but in our distillation model well you can count the number of trace and say it is hundred out of model but it is impossible develop 100 order model okay then we do reduce certain model we approximate the second order of the model with the dead time and so on okay.

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Alternate Approach

Let us treat elements of q transfer function
Matrix model as unknowns

$$\begin{array}{c}
 \begin{bmatrix} y_1(k) \\ y_2(k) \end{bmatrix} = \begin{bmatrix} \frac{b_1}{q+a_1} & \frac{b_2 q+b_3}{q^2+a_2 q+a_3} \\ \frac{b_3 q+b_4}{q^2+a_4 q+a_5} & \frac{b_5}{q+a_6} \end{bmatrix} \begin{bmatrix} u_1(k) \\ u_2(k) \end{bmatrix} \\
 \mathbf{y}(k) = \mathbf{G}(q) \mathbf{u}(k)
 \end{array}$$

Define parameter vectors

$$\begin{array}{l}
 \Theta_1 = [a_1 \ a_2 \ a_3 \ b_1 \ b_2 \ b_3]^T \\
 \Theta_2 = [a_4 \ a_5 \ a_6 \ b_3 \ b_5 \ b_6]^T
 \end{array}$$

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So now what are we doing now is I am going to identify these parameters of this model this transfer function model okay I am going to look at one output type okay so problems of system identification I m going to develop Miso models, Miso multiple input single output MISO you probably have words so SISO what is SISO? Input and output right.

I am going to do Miso model between y_1 and u_1 u_2 and y_2 v_1 and v_2 I will reform two parameter vectors here θ_1 is $a_1, a_2, a_3, b_1, b_2, b_3$ so a_1, a_2, a_3 and then b_1, b_2, b_3 so further first row estimation I am going to do

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MISO Model Identification

Consider MISO model

$$\hat{y}_1(k) = \frac{b_1}{q + a_1} u_1(k) + \frac{b_2 q + b_3}{q^2 + a_2 q + a_3} u_2(k)$$

$$= \frac{b_1 q^{-1} (1 + a_2 q^{-1} + a_3 q^{-2}) u_1(k) + (1 + a_1 q^{-1}) (b_2 q^{-1} + b_3 q^{-2}) u_2(k)}{(1 + a_1 q^{-1}) (1 + a_2 q^{-1} + a_3 q^{-2})}$$

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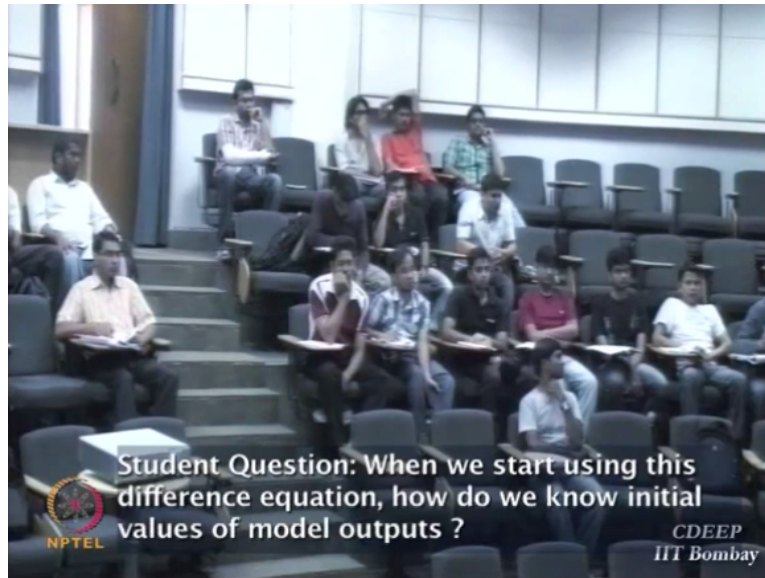
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Okay I'm considering this MISO model I am considering this MISO model okay now I have to convert this into time domain this is our I can use the algebra of transform functions if you see here then next step is to convert this into operator q^{-1} and then I have taken common denominator you see the common denominator okay and then after doing this I can multiply cross multiply and convert it into difference equation.

Because ultimately your computation is for optimization I need a difference equation so I need to go back to difference equation okay so what is my equivalent equation very, very easy to write if you look at, look at the numerator and the denominator you can just I mean the equation looks because there is a lot of algebra you multiply all the cross terms basically you know when you have q^{-1} .

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You know operating of u_k use that u_{k-1} and you will get u_{2k-1} and so on if you understand that simple thing this is just this is for algebra getting the difference equations starting from yeah you have to assured that.

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Model Parameter Estimation

Given set $U_N = \{u(0), u(1), \dots, u(N-1)\}$, guesses for Θ_1
and initial state $\hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)$
we can generate state sequence
 $\hat{y}_1(2), \hat{y}_1(3), \dots, \hat{y}_1(N)$
using difference equation (1) recursively

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See this model will tell you that will be doing it on next page okay see because $u(1)$ affix only u
 $y(3)$ okay and the separate more technical will be your problem is that you do not have to
assume equal to 0 you can liquidate in the list of unknown inputs or unknown variables and
optimize so do that okay.

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Model Parameter Estimation

Given set $U_N = \{u(0), u(1), \dots, u(N-1)\}$ guesses for Θ_1

and initial state $\hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)$

we can generate state sequence

$$\hat{y}_1(2), \hat{y}_1(3), \dots, \hat{y}_1(N)$$

using difference equation (1) recursively

Define prediction error

$$\varepsilon_1(k) = y_1(k) - \hat{y}_1(k)$$

Estimate $(\hat{\Theta}_1, \hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2))$ by solving following optimization problem

$$\underset{\Theta_1, \hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)}{\text{Min}} \sum_{k=2}^N [\varepsilon_1(k)]$$



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System Identification

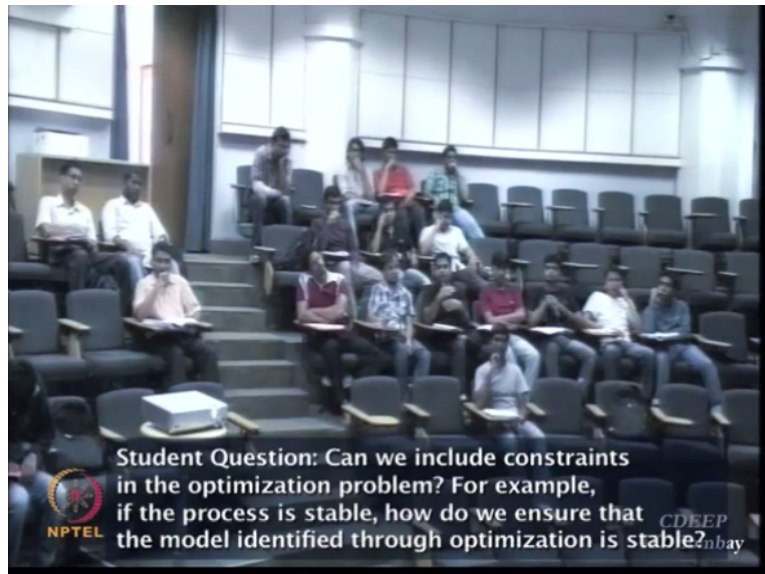
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You can read this y_0, y_1, y_2 to be unknown optimize guess an optimize okay so gain same thing if I have inputs sequence okay if I give you x path e path I can use a difference equation requires in times I can estimate y_1^{\wedge} what is y_1^{\wedge} level parameters as function of time okay estimated using the difference equation I find out the difference.

Now guessing the output x_k were I do not need any matrix okay so unless you have problem is I am including y_0, y_1, y_2 as you gets in that original case we have to base x_0 in this case I am guessing y_0, y_1, y_2 if you want to assure that it has go to 0 but you can do provided this system under consideration is open good stable.

I will talk about some little aspects later so I am not do it right now okay if it is open good statement it is fine to assure that this equal to 0 you will get some error initially but if you have large data that initial error will vanish okay on stable systems you cannot do this but identification of unstate system you have fairly complex is just an still you know into the domain of research not really okay.

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Is this clear is this optimization problem clear whether I want to do yeah, that is the good question so you have to introduce constraints into this problem that is not so easy okay that is a tough problem you probably have one way you can do it is to give constraints on θ okay but giving constraints of θ is also a difficulty okay.

So best till here is to start with a good guess okay now how do you start with good guess okay so well whether I can do this demonstrate some of these things has using a tool box you have the point you know extract just okay you have the point becomes at and you have to be profession till the hard you have to see the data.

You have to see how to do good guess is okay it will solve a problem it will keep it inside the meaningful range and so on but there are ways of initializing a module you know given a good guess of the module then particularly when the model is coming from physics see for example this kind of a model.


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Alternate Approach

Let us treat elements of q transfer function
Matrix model as unknowns

$$\begin{array}{c}
 \begin{bmatrix} y_1(k) \\ y_2(k) \end{bmatrix} \\
 \mathbf{y}(k)
 \end{array}
 =
 \underbrace{\begin{bmatrix} \frac{b_1}{q+a_1} & \frac{b_2 q+b_3}{q^2+a_2 q+a_3} \\ \frac{b_4 q+b_5}{q^2+a_1 q+a_2} & \frac{b_6}{q+a_6} \end{bmatrix}}_{\mathbf{G}(q)}
 \begin{array}{c}
 \begin{bmatrix} u_1(k) \\ u_2(k) \end{bmatrix} \\
 \mathbf{u}(k)
 \end{array}$$

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This kind of a model I can put constraint that the steady state gain should be negative or positive rather than no form physics if I increase the valve if it increase or decrease at the steady state okay so to find out the gain here for this you put $Q=1$ you will get the gain so I can put it explain that b_1 of power $1+a_2$ okay the steady state gain.

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$$x(k+1) = \phi x(k) + \Gamma u(k)$$

$k=0$ $u(0) \rightarrow$ known.

Unknowns $\equiv \phi, \Gamma, x(0)$

$$y_1(s) = \frac{b_2}{q + a_1} u_1(s)$$

$$q = 1 \quad \frac{b_2}{1 + a_1} > 0$$

So if I for this model the steady state gain for this model is obtained by setting $q=1$ so the steady state gain is b_2 upon $1+a_1$ okay now this argue from system if I change the valve 1 there is going to happen to level 1 so the increase or decrease it is going to be increase always going to increase so that gain steady state gain between the all 1 one position and level 1 is of course going to be positive okay.

So I just put the constraint that this is always greater than 0 okay so likewise we can argue about each element and put meaningful constraints you can give constraint optimization problem which that is a good question and to get meaningful for the solutions you may have to do such okay, okay so this is, this is the problem for level 1 and input 1 input 2 these four model likewise I can develop same thing for level 2 input 1 input 2 to measure the models.

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Pros and Cons

- In each case, we get highly nonlinear optimization problem
- Important to give good initial guess to obtain reliable model parameters: not an easy task
- It is assumed that 'structure' of the linearized state space model / q-TF matrix is known a-priori, which may not be the case

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I can combine and went into grand model and use of control okay well what about pros and cons of doing this in each case you have to solve an optimization problem and you have to give a good initial guess so highly non linear of optimization problem not at all easy to solve you were looks stake forward here how easy to solve so you did not get good guess is very, very important how did you good guess trouble it is not so easy to give good guess next thing is right.

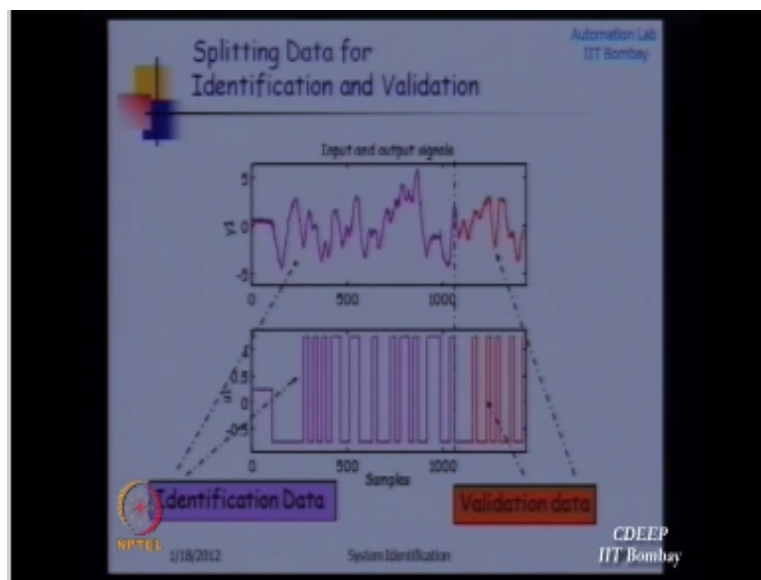
Now I have assure that structure of five model could be arrived at by some arguments okay you know these are zero and these are non zeros so I had a great model what if for a complex system you cannot do that it is quite slightly that for a complex system I cannot come up with this structure okay so, in that case I have no clue as to how this five matrix is going to look like okay could be anything, it could be full matrix could be in a fast matrix diagnose.

So there is one more thing I am just modeling here inputs that are no use okay any system will have inputs that are unknown okay for example inverse in this particular system okay you know there is a wall and either pump a pump gets voltage from the source and the source voltage is never perfectly contented to 20volts it is frustrating between 200 to 240 because of that the pump speed is vary because the pump speed is varying the flows frustrating.

So even if I keep the wall open in 50% actually flow is got constant flow keeps you know frustrating now this frustration have the impact on the level right it is not going to that the level is going to be constant because the flow is frustrating you know the wall position is constant the level is going to frustrate.

So my output measure as something else which is coming from some other input which is not measured I am not going to measure everything that happens right I am not going to measure the voltage in the it is not possible to measure everything so there are unknown disturbances and then I need to model them so what is the solution well so I am going to have relax even the assumption that I know the structure of the model nothing I want the flat form okay I only have data I only have this.

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Okay I have this which I can play I can give inputs I can collect data now can I derive with the model okay that is what we are going to see in the next series of lectures yeah.

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To different inputs sequence I have the identical output sequence mathematically yes no added two different equations not mathematically because it depends upon how many number of input how many number of outputs are there if you have in a differential equation because of the uniqueness of the solutions okay you will not get if you have input sequence different you will get output sequence different.

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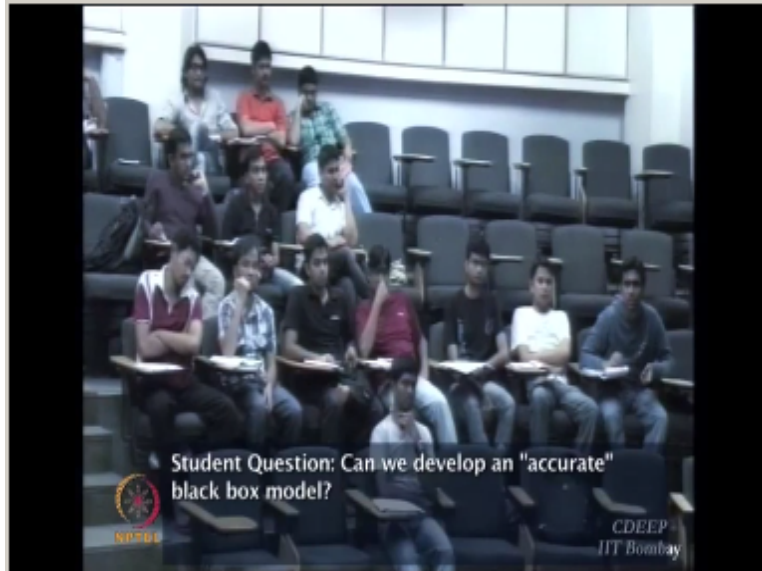


We assume that the differential equation have a unique solution yeah even then a having non unique solutions with the same it is possible in non linear system it is possible in linear system I cannot think of if you have number of inputs equal to the number of outputs if greatest amount but in a non linear system it is possible to have same input sequence for example a non linear system can have multiple studies state for the same input we can multiple steady states for the same input okay very much possible in non linear systems.

And technically it is what you are saying same input multiple solutions so how does a system will behave will depend upon locally where it is okay in the state place or where it goes now those kind of things are beyond the scope but it is only possible in real non linear systems in this ideal world of real systems we will get a but even for the systems if the disturbances are different every time then you will not get the same output.

Even if you give the same input okay so in this system time set up if I give this same sequence every time I beyond on get dextrally saying output because even the voltage fluctuation were every time different so the level fluctuations that is arising out of voltage fluctuations are been time different okay if there are voltage fluctuations what so ever perfect system if you same input should get the same output okay yeah.

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For about accurate black box model.

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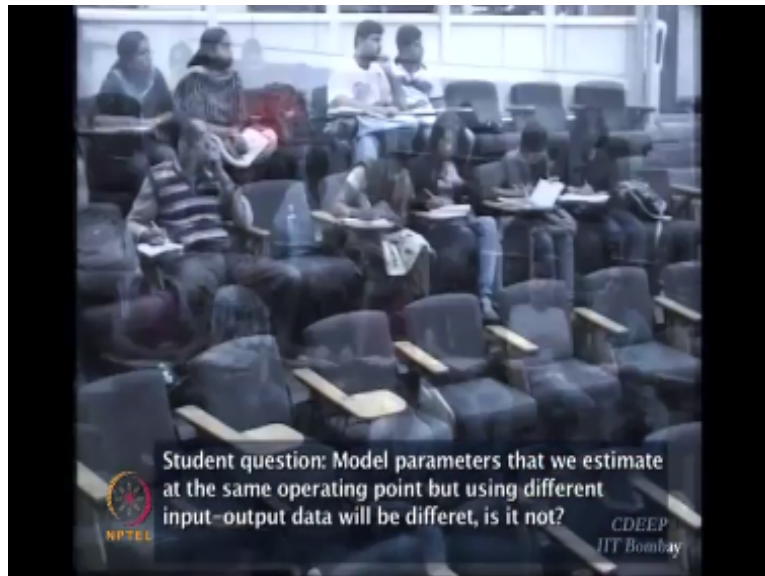


Well it is it is very difficult to review an offline answer what you mean by accurate black box model? It is an oxide model but if you can develop a black box model and if you have a black box structure you might in depend box again you have done the optima ion problem you are saying that after the optimization you do not get big black box model then what you do? Use black box model which is yes but then you know if there is a mismatch between the plant and the model.

And if you use the grey box model that is your fault okay the diagnose algorithm will say that something is quality all the time because there is a mismatch between the model and the black so is the grey box model is very helpful but, it has to be very good otherwise we had problem diagnose using a grey box model we had lot of problem because if there is a mismatch for control there is no problem for diagnoses there is a problem control you can handle model plant management.

And do a good control as long as you know order of magnitude changes of the model and in the plant are same okay but so control mismatch does not matter so much in diagnoses if you are saying diagnose is the application I would go for a grey box model and improving it for diagnoses it is very difficultly used by black box model so the application depends what is that for control I can use black box model.

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Yeah so thus the linear know if I change the linear action point I will get the difference model

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Yeah yes.

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Model Parameter Estimation

Given set $\mathbf{U}_N = \{\mathbf{u}(0), \mathbf{u}(1), \dots, \mathbf{u}(N-1)\}$ guesses for Θ_1

and initial state $\hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)$

we can generate state sequence


$$\hat{y}_1(2), \hat{y}_1(3), \dots, \hat{y}_1(N)$$

using difference equation (1) recursively

Define prediction error

$$\varepsilon_1(k) = y_1(k) - \hat{y}_1(k)$$

Estimate $(\hat{\Theta}_1, \hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2))$ by solving following optimization problem



$$(\hat{\Theta}_1, \hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)) = \underset{\Theta_1, \hat{y}_1(0), \hat{y}_1(1), \hat{y}_1(2)}{\text{Min}} \sum_{k=2}^N [\varepsilon_1(k)]$$

So every time you get a slightly different model.

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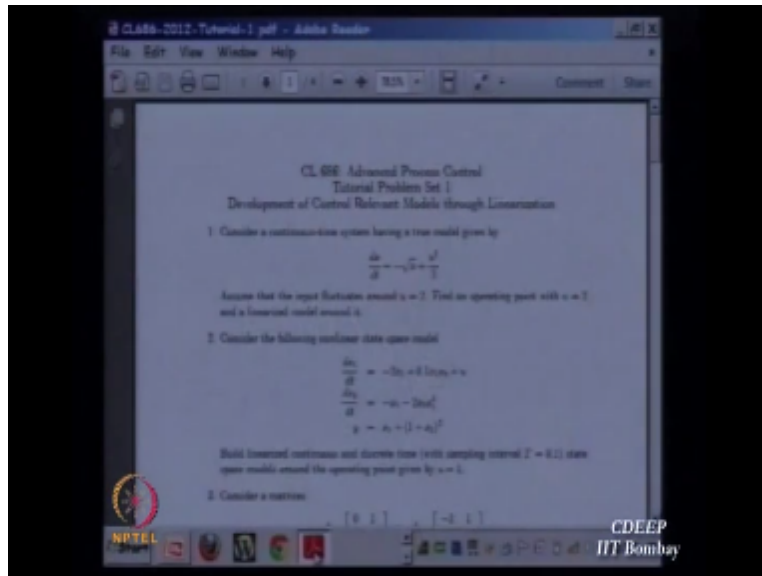
Pros and Cons

- In each case, we get highly nonlinear optimization problem
- Important to give good initial guess to obtain reliable model parameters: not an easy task
- It is assumed that 'structure' of the linearized state space model / q-TF matrix is known a-priori, which may not be the case
- Effect of unmeasured inputs (disturbances) on system dynamics is not captured by the model

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Hopefully when you are developing a black box model I am assuring that you know you are operating condition remain more or else same then only you can use it for design otherwise you cannot but then if you have a situation vary on nothing we just have this motor car drive and you did not have you know similar coming in metal lab then uses you can use simple models okay so I do not want to go into this today black box model and start with the in the next class I just want to show you this tutorial problems.

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Which I have uploaded so I upload this tutorial problems there are about 10 problems here either about linearizing the differential equations then converting them into difference equations finding out q transfer function matrix or z transfer function matrix first transfer function matrix while out of some problems which are given you here 9 problems are here mathematical problems just talking about x_1, x_2, y_1, y_2 like in that text book last two problems are.

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CLASS-2017-Tutorial-1.pdf - Aditya Rastogi

File Edit View Window Help

18. Consider a jacketed stirred-tank heater. A hot fluid is circulated through the jacket (assumed to be perfectly mixed) and heat flow between the jacket and vessel increases the energy content of the vessel fluid. Energy balances on the vessel and jacket fluids result in the following equations:

$$\frac{dT}{dt} = \frac{F}{V} (T_i - T) + \frac{UA}{V\rho c_p} (T_j - T)$$

$$\frac{dT_j}{dt} = \frac{F_j}{V_j} (T_{j,i} - T_j) - \frac{UA}{V_j \rho_j c_{p,j}} (T_j - T)$$

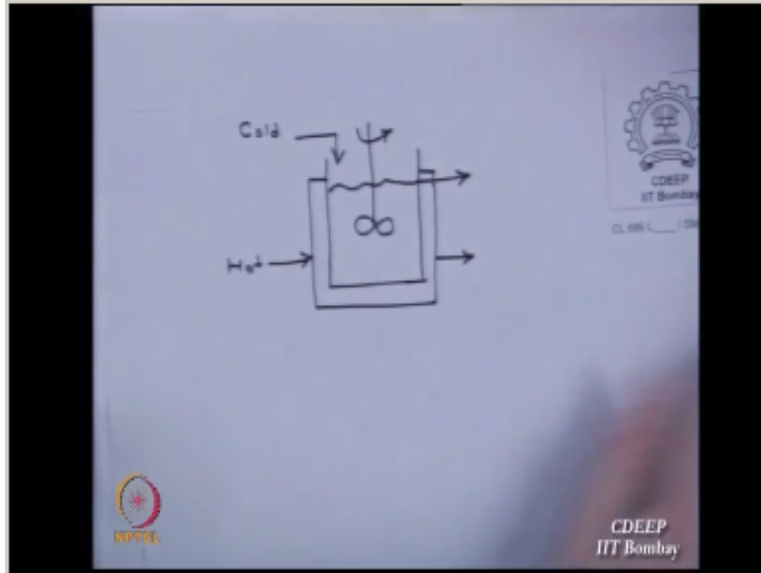
Here the outputs are the vessel and jacket fluid temperatures, which are also the states; the inputs are the jacket flow rate, feed flow rate, feed temperature, and jacket inlet temperature. The nominal (steady-state) values of the input and output variables and the parameters are given below:

Variable	Description	Nominal Value
F	Feed flowrate	$1 \text{ ft}^3/\text{min}$
F_j	Jacket fluid flowrate	$1.5 \text{ ft}^3/\text{min}$
T_i	Feed temp.	100°F
T_j	Vessel fluid temp.	120°F
$T_{j,i}$	Jacket inlet temp.	300°F
T_j	Jacket fluid temp.	100°F
ρ_c	---	$61.7 \text{ lb}_m/(\text{ft}^3 \text{ ft}^3)$

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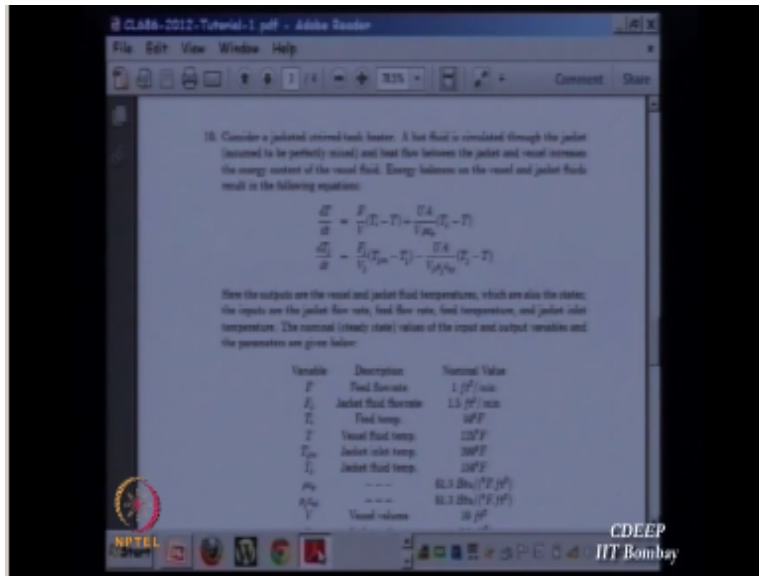
Real physical problems okay those are few words chemical engineers can appreciate both the problems the second problem actually it is not difficult to understand but you may face some difficult in appreciating what is the second model the first one here is just a system which is I will just draw this.

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We have this symbol means this is well system okay and it moves out and then there is a jacket here the hitting flow could be stream for example okay some hot fluid in industry they use some hot fluid to let say heat the condense inside this time so the cold stream here and this is hot fluid okay so the cold fluid becomes hot becomes cold there is a exchange of heat between the two and the model for that is.

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Is given by this two coupled equations so deviates this differential equations convert them into a model of this form $x=a+bu$ okay and I given them potential variables you then you convert it into different equation by discrete and I get the model okay for this last two problems which I coming from physics you may need to use metal lab okay first 1 to 9 problems you can do by hand because in those problems I have given 1 to 3 you will get some nice Eigen values and Eigen vectors you can see here.

So 1,1 and you will get some 5 problems are mainly for exam and for doing some practice and practice and then the last two problems are real problems and I accept that all those who are non chemical engineers should appreciate the problem 10 chemical engineers should appreciate both the problems 10 and 11 okay next time I will try to put some more problems from electrical mechanical some other problems which I have I had some models from electrical circuit but I do not have values.

Because you have linear at some point you need actually some values of and so on or spring mass systems which are modeling some car and all those models are available but I am trying to get values for physical parameters so what we have been learned here okay we actually implement it on the project in metal lab okay so it is the problem from different domains and then what will you do if you do really here design a container you design a container for your system and so on everything that you do on in the class you do it in the type of okay.

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