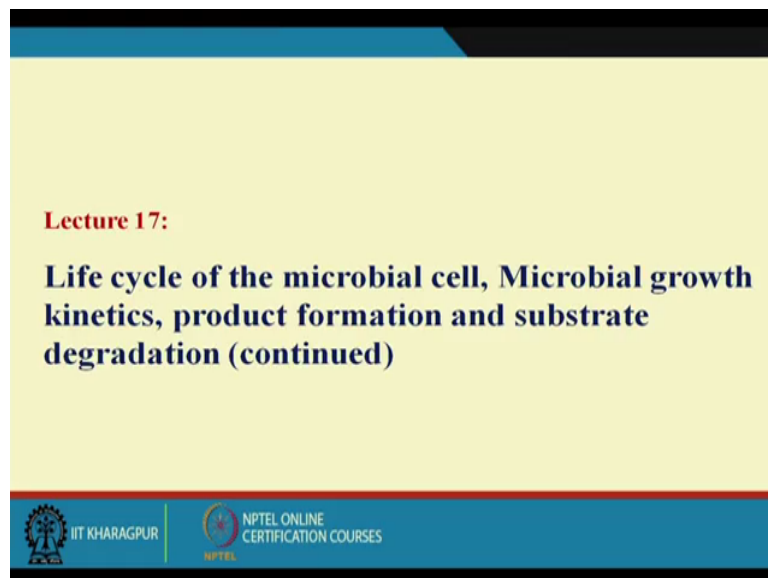


Course on Industrial Biotechnology
By Prof. Debabrata Das
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Indian Institute of Technology Kharagpur
Lecture 17

Life Cycle Of The Microbial Cell, Microbial Growth Kinetic, Product Formation And Substrate Degradation (Contd.)

Let me welcome back here again in my course industrial biotechnology. Now I was discussing about the microbial growth kinetics product formation and substrate degradation.

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In the last class I try to find out that that what is the role of for life cycle for the growth of the cells. I told you when whenever we do the inauguration of the because different and the growth cycle we have different phases and different phase has the difference significance. Lack Phase is considered as a actualization phase growth which is considered.

The Lock Phase is considered as a growth phase where the organisms are active and in stationary phase is considered the starvation phase where most of the secondary metabolite formation take place. Now when you do do the inauguration of the cell (1:19) to do the inauguration of the cell.

In the either mid lock phase to get lock phase. Just to ensure the organisms are active. Now um we used the Michaels menten equation. I showed you the menten equation so for the study the growth of the organism. So similar to Michaels menten equation only we come

across the is which is considered as a growth limiting substrate and the growth limiting substrate might be anything because media composition is a number of chemicals.

It may be carbon source, it may be nitrogen source, it may be vitamins, it may be minerals so anything might be the growth limiting substrate provided the growth is if viewed from if it changes with respect to change of concentration of the particular component present in the reaction mixture then and only then we got growth limiting substrate. Then we come across the batch process and the.

And the chemostat process. Batch process is the process through which we can have this we can find out the life cycle of the cells but major disadvantage of the batch processes that we cannot hold particular phase of growth for infinite period of time. As the time passes on one phase which which what to the other phases. But in the chemostat process we find that under $(2:47)$ condition.

And and at the steady state steady state condition μ equals to D , so by controlling dilution rate it is possible to maintain a particular phase of growth in the in the fermentation block. So we can we supposed particularly Baker's yeast fermentation process we need more cell mass production so literally that rate of cell mass production report in the in the growth phase but in case a batch process.

We cannot hold the phase for longer period of time but in the in case of chemostat process we can continue this growth Phase for infinite period of time. I think and how to find out how to calculate this this growth of the organism? How to calculate the substrate degradation? I show in the next class.

Now now this particular lecture I try to concentrate that we will come across the D_{max} and D_{wash} out which is very important as well chemostat operation is concern. Then with this can be overcome by using either by mobilization of the cell or by the the recycling the cell mass to the reactor and how we can do that? So this this year I am going to highlight in my lecture.



(Refer Slide Time: 4:14)

Monod chemostat model

□ Cell mass productivity (Q_X) = $\frac{\text{cell mass produced}}{\text{time}} = DX$ ($\frac{g}{L.h}$)
 $= Y_{X/S} \left(DS_0 - \frac{D^2 K_S}{\mu_{max} - D} \right)$ (15)

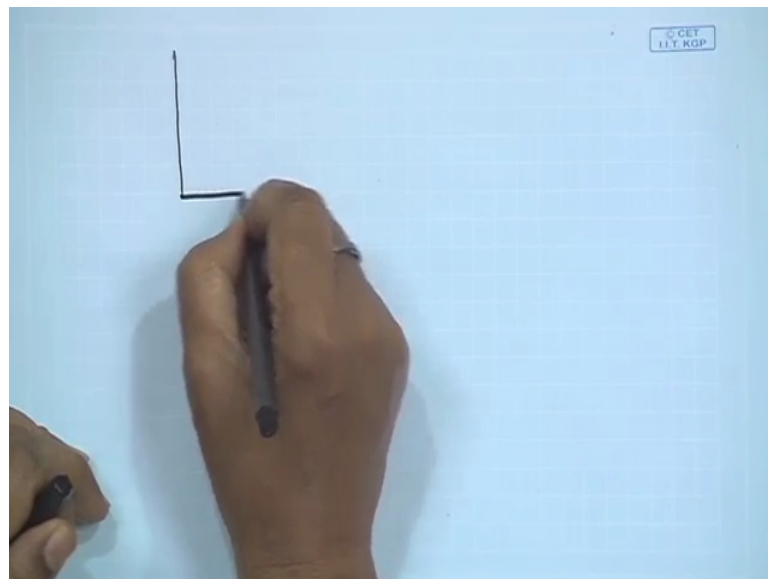
□ To obtain maximum dilution rate (optimum dilution rate) D_{max} , where the productivity will be maximum $\{(DX)_{max}\}$, $\frac{d(DX)}{dD} = 0$

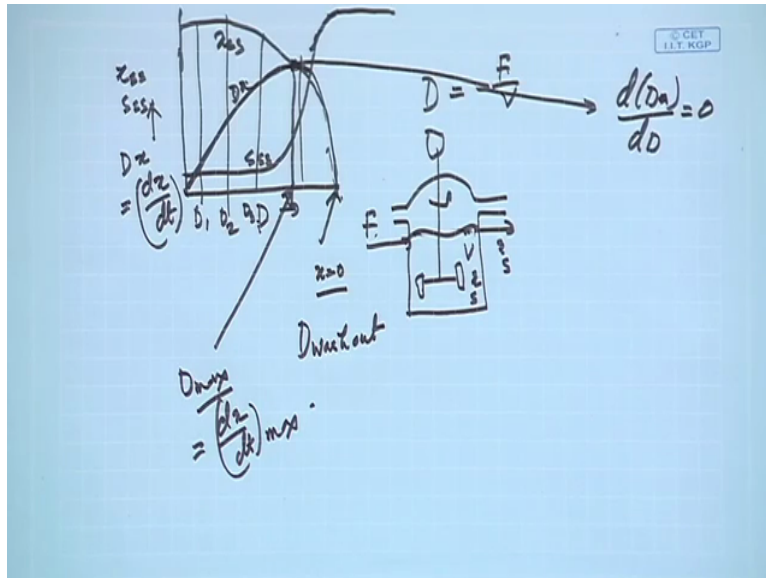
$$\frac{d(DX)}{dD} = Y_{X/S} \left[S_0 - \frac{(\mu_{max} - D)2DK_S - D^2 K_S(2)(\mu_{max} - D)}{(\mu_{max} - D)^2} \right] = 0$$
$$S_0 = \frac{2DK_S}{(\mu_{max} - D)} + \frac{D^2 K_S}{(\mu_{max} - D)^2}$$
$$\frac{S_0}{K_S} = \frac{2D}{(\mu_{max} - D)} + \frac{D^2}{(\mu_{max} - D)^2}$$

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Let me start with that, first let me show you how you can calculate the D Max?

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D Max is considered as a that maximum the dilution rate at which we will get the maximum rate of cell mass production. This is equal to I showed you before that D into X is nothing but DX by DT what is DX by DT? Is the rate of growth of the cells. Now this will be like this is go like this and this will come down like this. Now at the same time we can have the plot for X. X is is the steady state cell mass concentration.

The state State substrate concentration and steady state concentration will be like this it will go like this then it'll be constant and then your your cell mass concentration will will come back here. This is Xss and this is Sss. So this is very important because because as as your dilution rate increases because this is the different dilution rate. This is D1, this is D2, this is D3. Now I told you dilution it is equal to what F by V.

So in case of any kind of Chemostat suppose this is this is any chemostat, if you pass this, this is F and this is V. So we can change the value of D if we simple increase the value V is constant. The volume of the reactor the volume of the working volume of the reactor is constant. So if you want to change the value of D we can change the value of F when you change the value is changed.

At different dilution rate I told you that when you change the value of a after infinite time will get the steady state condition. What is steady state condition? When the cell mass condition will remain unaltered. When the substrate concentration cell mass concentration they will unchanged with respect to time that is called steady state condition. T at the different dilution rate you get the different steady state condition.

So this is exactly what is happening, as the dilution rate increases, your steady state cell mass concentration will finally this is a crucial point where X equal to 0 X equal to 0. No cell is present in the reactor. If there is no cell present in the reactor there will be no reactions. Because cell mass is usually responsible for carrying out the reaction and this is considered as D washout.

D washout means that at the dilution rate there is no cell present in the reactor. This is the D washout and here you give DX by DT this is DX by DT with respect to time increase and then decrease. Now here we have a point and this point we considered as the D-max what is Dmax? Dmax is the dilution rate when DX by DT equal to maximum. that means what we can we can write.

When when at this particular point I can write at this particular point D DX by DT this should be equal to zero. Because this is D this is the DX this is DX and D DX by DT this this is Evan Plato so I can get there at the Dmax this is the condition that we have. Now now let me come here.

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Monod chemostat model

Cell mass productivity (Q_X) = $\frac{\text{cell mass produced}}{\text{time}} = DX$ ($\frac{g}{L \cdot h}$)
 $= Y_{X/S} \left(DS_0 - \frac{D^2 K_S}{\mu_{max} - D} \right)$ (15)

To obtain maximum dilution rate (optimum dilution rate) D_{max} , where the productivity will be maximum $\{(DX)_{max}\}$, $\frac{d(DX)}{dD} = 0$

$$\frac{d(DX)}{dD} = Y_{X/S} \left[S_0 - \frac{(\mu_{max} - D)2DK_S - D^2 K_S(2)(\mu_{max} - D)}{(\mu_{max} - D)^2} \right] = 0$$

$$S_0 = \frac{2DK_S}{(\mu_{max} - D)} + \frac{D^2 K_S}{(\mu_{max} - D)^2}$$

$$\frac{S_0}{K_S} = \frac{2D}{(\mu_{max} - D)} + \frac{D^2}{(\mu_{max} - D)^2}$$


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That here we can write that DX by DT we can write like this.

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Lecture 17:



Life cycle of the microbial cell, Microbial growth kinetics, product formation and substrate degradation (continued).

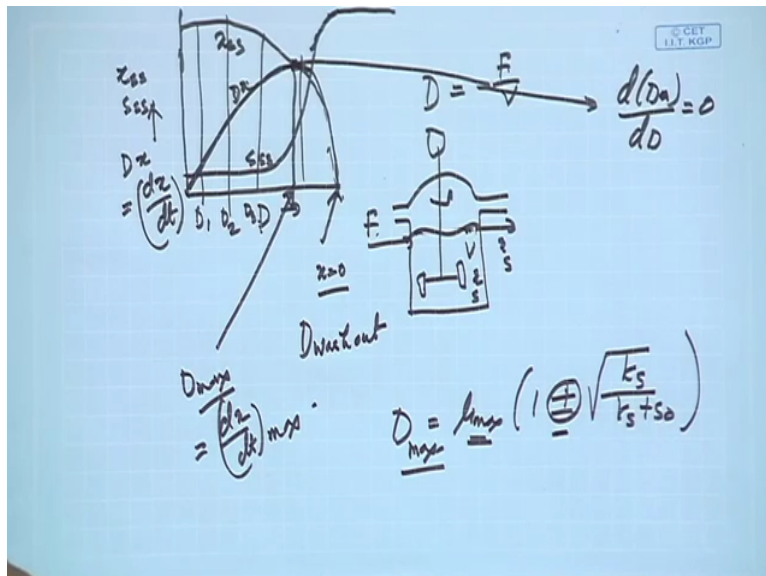
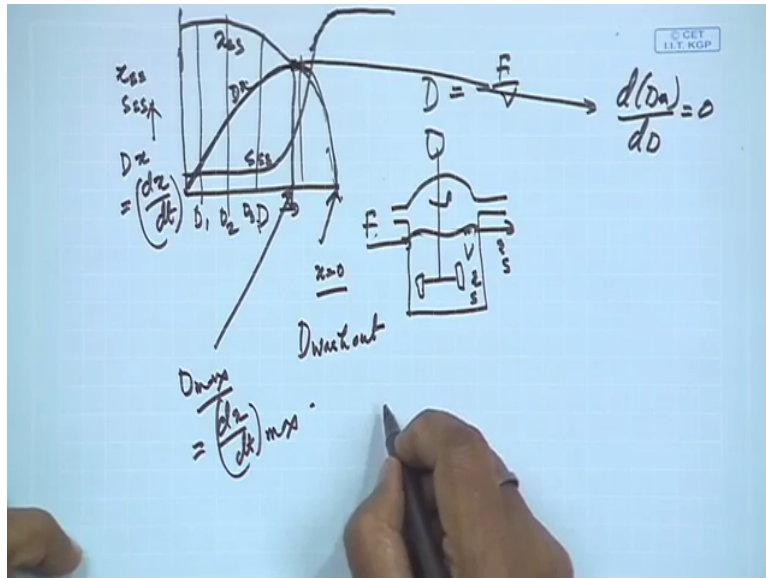


Because we have we have we have seen that with this is the expression that we have then S_0 we can write like this is the way we can write the like this.

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Monod chemostat model

$$1 + \frac{S_0}{K_S} = 1 + \frac{2D}{(\mu_{max} - D)} + \frac{D^2}{(\mu_{max} - D)^2}$$
$$1 + \frac{S_0}{K_S} = \left\{1 + \frac{D}{(\mu_{max} - D)}\right\}^2$$
$$\frac{(K_S + S_0)}{K_S} = \left(\frac{\mu_{max}}{\mu_{max} - D}\right)^2$$
$$\left\{\frac{\mu_{max} - D}{\mu_{max}}\right\}^2 = \frac{K_S}{K_S + S_0}$$
$$\left(1 - \frac{D}{\mu_{max}}\right) = \mp \sqrt{\frac{K_S}{K_S + S_0}}$$
$$D = \mu_{max} \left(1 \mp \sqrt{\frac{K_S}{K_S + S_0}}\right)$$




Ultimately we will come now come this equation and this equation is what this is D equal to mew Max one plus minus Root $K_s + K_s + S_0$. Now one thing I want to find out that you are that this is this is the D_{max} value this is the D_{max} value we can calculate like this. Now the D_{max} value always should be less than mew Max value. So it cannot be plus it will be always negative.

So usually the D_{max} value will be $1 - \sqrt{K_s / (K_s + S_0)}$ then we derive this plus minus but actually they cannot be possible is always should be less than mu Max minus K_s by S_0 .

(Refer Slide Time: 9:25)

Monod chemostat model

- So, $D_{max} = \mu_{max} \left(1 - \sqrt{\frac{K_S}{K_S + S_0}}\right)$
- As, $D_{max} < \mu_{max}$

$$D_{max} = \mu_{max} \left(1 - \sqrt{\frac{K_S}{K_S + S_0}}\right) \dots\dots\dots (16)$$

- **Operation of chemostat at D_{max} gives maximum rate of cell mass production from the reactor**
- Cell mass concentration at D_{max} ,

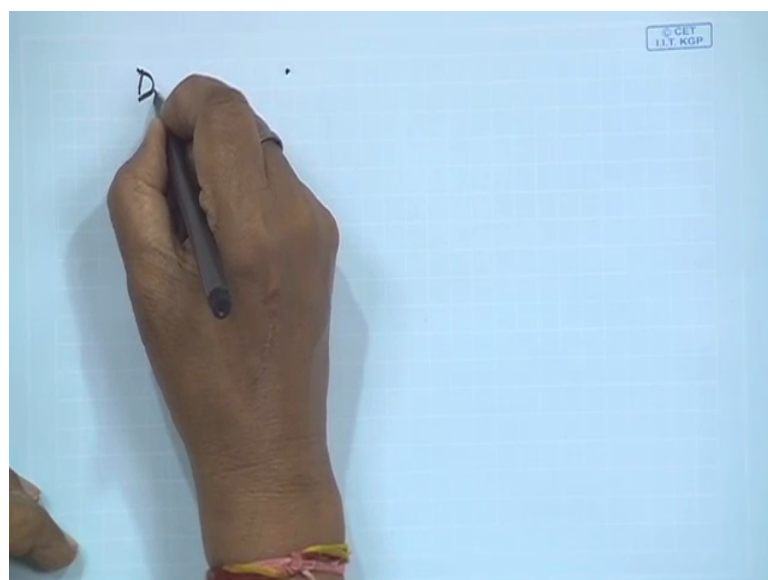
$$X_{max} = Y_{X/S} \left(S_0 - \frac{D_{max} K_S}{\mu_{max} - D_{max}} \right)$$

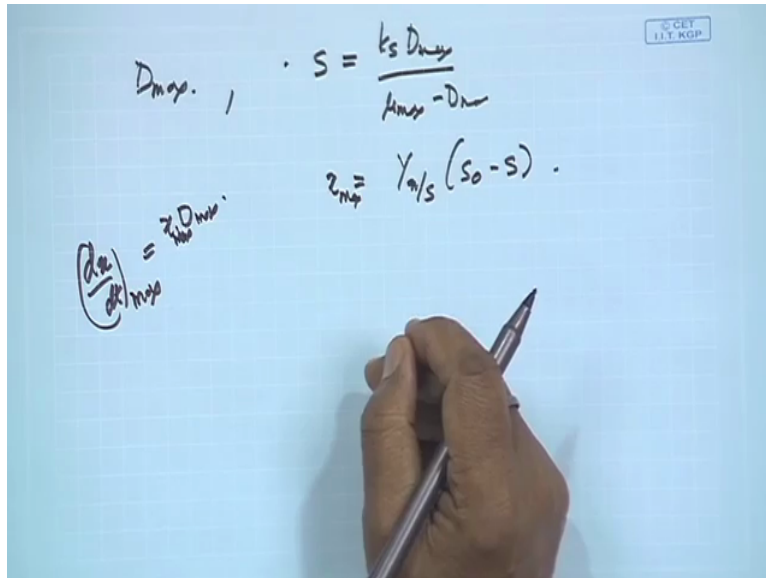
$$X_{max} = Y_{X/S} \left(S_0 - \frac{K_S}{\frac{\mu_{max}}{D_{max}} - 1} \right)$$

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Now here D_{max} equal to like this. But since D_{max} is much less than μ_{max} so we can write it D_{max} equal to $\mu_{max} \left(1 - \sqrt{\frac{K_S}{K_S + S_0}}\right)$. Now that operation of the chemostat at D_{max} is the maximum rate of cell mass production from the reactor. The cell mass now how we can find out what is the maximum rate of growth of the cells? Suppose what what you can we can do in a chemostat?

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If you find out the D_{max} value then you can find out what is the S value? S value is what S value is what we can write $K_S D_{max} / \mu_{max} - D_{max}$. I can easily find out this value. We can and similarly I can find out the value of X . This is X equal to this is the maximum value of X_{max} is equal to what $Y_{X/S}$ into S_0 minus S . So this is now X_{max} .

What is the when rate of growth of the cell rate of production of cell is maximum when X into D_{max} into D_{max} . If you multiply that you can we have we have come across like this. Now now if we can we can we can do the calculation in other way also.

(Refer Slide Time: 11:08)

Monod chemostat model



- So, $D_{max} = \mu_{max} \left(1 - \sqrt{\frac{K_S}{K_S + S_0}}\right)$
- As, $D_{max} < \mu_{max}$

$$D_{max} = \mu_{max} \left(1 - \sqrt{\frac{K_S}{K_S + S_0}}\right) \dots\dots\dots (16)$$

- **Operation of chemostat at D_{max} gives maximum rate of cell mass production from the reactor**
- Cell mass concentration at D_{max} ,

$$X_{max} = Y_{X/S} \left(S_0 - \frac{D_{max} K_S}{\mu_{max} - D_{max}}\right)$$

$$X_{max} = Y_{X/S} \left(S_0 - \frac{K_S}{\frac{\mu_{max}}{D_{max}} - 1}\right)$$



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Suppose this we we we calculated the cell mass production this is this is this is X X X X
 X_{max} equal to $Y_{X/S}$ by S this is the S_0 minus this one. That is the substrate concentration the
 that is the rate of substance that you consume that you can find out the value that form that
 we can calculate this this one and finally we come across the X_{max} value is this one.

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Model chemostat model

$$X_{max} = Y_{X/S} \left(S_0 - \frac{K_S}{\mu_{max} \left(1 - \frac{K_S}{\sqrt{K_S + S_0}} \right)} \right)$$

$$X_{max} = Y_{X/S} \left(S_0 - \frac{K_S}{\frac{\sqrt{K_S + S_0}}{(\sqrt{K_S + S_0} - \sqrt{K_S})} - 1} \right)$$

$$X_{max} = Y_{X/S} \left(S_0 - \frac{(\sqrt{K_S + S_0} - \sqrt{K_S}) K_S}{\sqrt{K_S + S_0} - \sqrt{K_S + S_0} + \sqrt{K_S}} \right)$$

$$X_{max} = Y_{X/S} \left(S_0 - (\sqrt{K_S + S_0} - \sqrt{K_S}) \sqrt{K_S} \right)$$



$$X_{max} = Y_{X/S} \left(S_0 - \sqrt{K_S(K_S + S_0)} + K_S \right)$$



Monod chemostat model

□ At $D = D_{max}$,

$$X_{max} = Y_{X/S} \left(S_0 - \sqrt{K_S(K_S + S_0)} + K_S \right) \quad \dots\dots (17)$$

□ Maximum cell mass productivity can be determined from the equation (15) with $D = D_{max}$

$$Q_{X,max} = Y_{X/S} \left(D_{max} S_0 - \frac{D_{max}^2 K_S}{\mu_{max} - D_{max}} \right) \quad \dots\dots (18)$$



And D_{max} we find out this equation. We derive this equation equal to X_{max} equal to $Y_{X/S}$ by S_0 root over K_S K_S K_S into K_S plus S_0 plus K_S . The maximum cell productivity can be determined by the equation D equal to D_{max} . Now we multiply D with the D_{max} we will get this equation. This is then equal to this is the maximum rate of production will be $Y_{X/S}$ by S into D_{max} into this that we have in the previous equation that can we can write in the 15 equation.

(Refer Slide Time: 12:22)



Monod chemostat model

Cell mass productivity (Q_X) = $\frac{\text{cell mass produced}}{\text{time}} = DX$ ($\frac{g}{L.h}$)
 $= Y_{X/S} \left(DS_0 - \frac{D^2 K_S}{\mu_{max} - D} \right)$ (15)

To obtain maximum dilution rate (optimum dilution rate) D_{max} , where the productivity will be maximum $\{(DX)_{max}\}$, $\frac{d(DX)}{dD} = 0$

$$\frac{d(DX)}{dD} = Y_{X/S} \left[S_0 - \frac{(\mu_{max} - D)2DK_S - D^2 K_S(2)}{(\mu_{max} - D)^2} \right] = 0$$

$$S_0 = \frac{2DK_S}{(\mu_{max} - D)} + \frac{D^2 K_S}{(\mu_{max} - D)^2}$$

$$\frac{S_0}{K_S} = \frac{2D}{(\mu_{max} - D)} + \frac{D^2}{(\mu_{max} - D)^2}$$





So in the 15 equation this equation we can put this value we can put this value in D Max V equal to D max. We can have this equation this is we can write this.

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Monod chemostat model

At $D = D_{max}$,
 $X_{max} = Y_{X/S} (S_0 - \sqrt{K_S(K_S + S_0)} + K_S)$ (17)

Maximum cell mass productivity can be determined from the equation (15) with $D = D_{max}$

$$Q_{X,max} = Y_{X/S} \left(D_{max} S_0 - \frac{D_{max}^2 K_S}{\mu_{max} - D_{max}} \right)$$
 (18)
 


We can find out the maximum cell mass production.

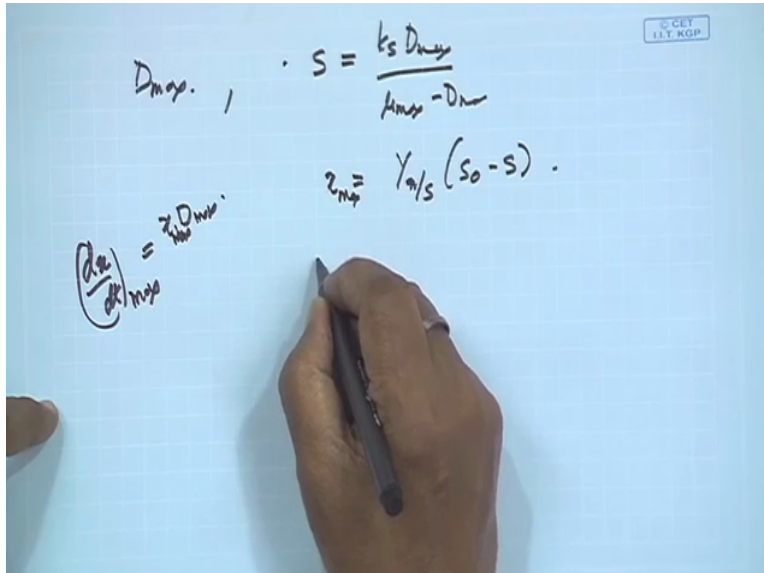



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Monod chemostat model

□ $D_{washout}$

- As D increase, S increase slowly at first and then more rapidly as D approaches μ_{max} ; correspondingly, X decrease so that $X \rightarrow 0$ as $D \rightarrow \mu_{max}$. The condition at high dilution rate whereby X reduces to zero is known as 'washout'. The corresponding dilution rate is called $D_{washout}$
- The growth rate can no longer keep up with the dilution rate
- $D_{washout} = \frac{\mu_{max} S_0}{K_S + S_0}$

$D_{max} < D_{washout} \leq \mu_{max}$

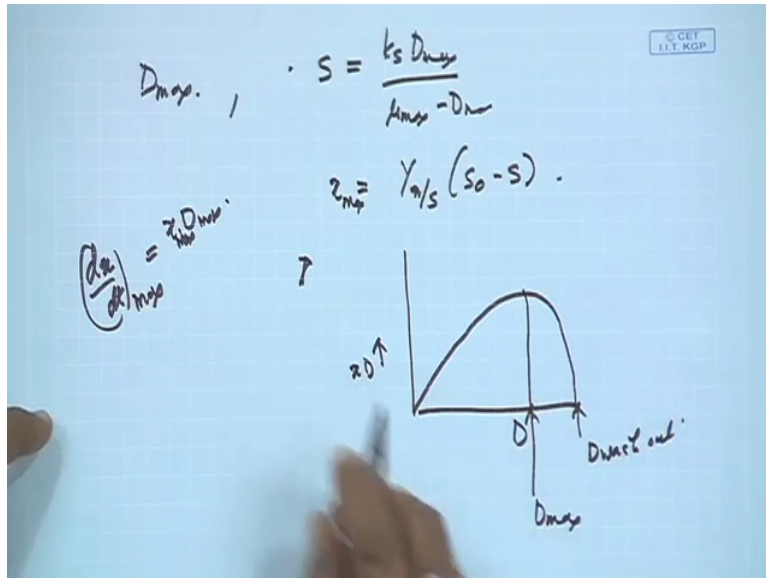


D_{max} , $S = \frac{k_s D_{max}}{\mu_{max} - D_{max}}$

$z_{np} = Y_{x/s} (s_0 - S)$

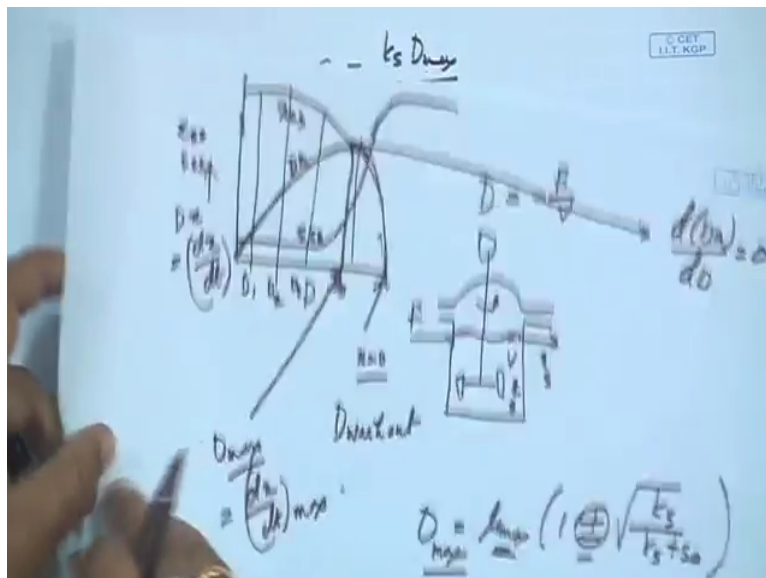
$\left(\frac{d_x}{dt}\right)_{np} = -x D_{max}$

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Now in case of Chemostat process major drawback that we have the Dwashout because that the wash out if you if you look at it I can show it like this that if you have X into D related with correlated with this one.

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$z_{ss} = \frac{Dz}{ds}$
 $Dz = \left(\frac{dz}{dt} \right)_{ss}$

$D = \frac{d(Dz)}{dt} \rightarrow \frac{d(Dz)}{dt} = 0$

$D_{max} = \frac{Dz}{dt}$

$D_{max} = \frac{K_s D_{max}}{K_s + s_0}$

$D_{max} \cdot s = \frac{K_s D_{max}}{K_s + s_0}$

$z_{mp} = \frac{Y_0}{s} (s_0 - s)$

$\left(\frac{dz}{dt} \right)_{mp} = z_{in} D_{max}$

$D_{max} \text{ out}$

$D_{max} \cdot s = \frac{K_s D_{max}}{K_s + s_0}$

$z_{mp} = \frac{Y_0}{s} (s_0 - s)$

$\left(\frac{dz}{dt} \right)_{mp} = z_{in} D_{max}$

$D_{max} \text{ out} = \frac{K_s s_0}{K_s + s_0}$

This is like this. So you have two two points we have here you have D_{max} value, here you have $D_{washout}$ value $D_{washout}$. Now as $D_{washout}$ value I showed you it before that here here I have showed you that at $D_{washout}$ value this this X will be zero and if X will be zero this corresponding value will be X_0 . That is that is corresponding point will be S_0 so if it is S_0 then what what will be the $D_{washout}$ value?

$D_{washout}$ value D equal to $\mu_{max} S_0 / (K_S + S_0)$ steady state condition I can write $\mu_{max} S$ will be $S_0 + K_S + S_0$. So since there is no cell when reaction takes place so S is considered as S_0 and if you put the value of S_0 , you can easily calculate that. So we have we have the expression with us D_{max} value and they are very close to each other and in the industry.

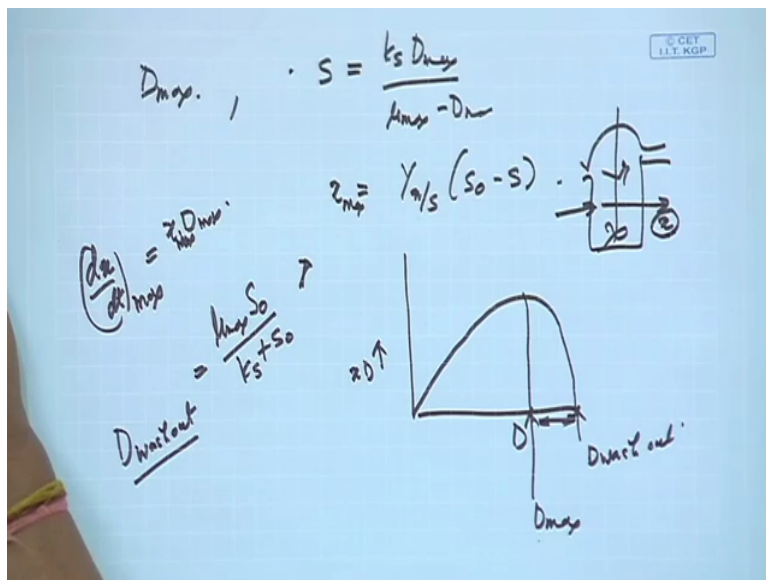
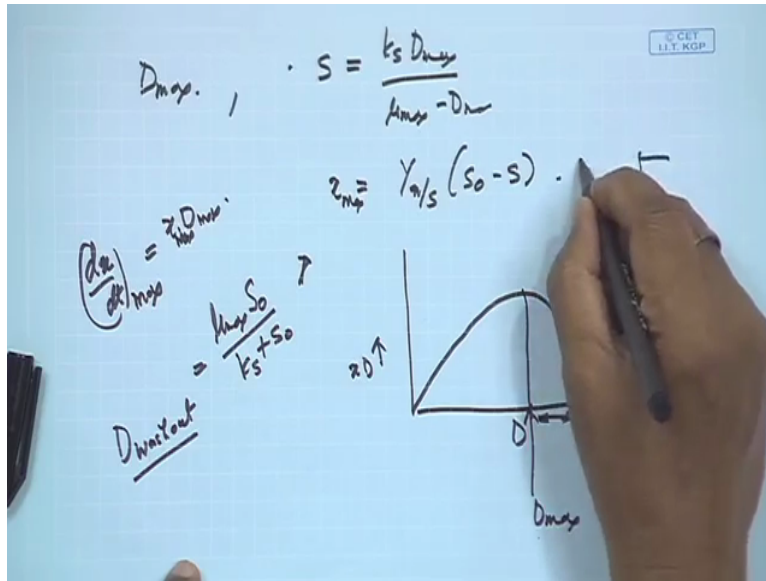
Here I want to mention that in the industry when you operate a chemostat process that we don't have different forms for the operation of different product μ_{max} . We use for maintaining the different product and how we maintain the different product? Just just opening the valve because we have seen in the wash basin when you open your valve then you'll be more water flow tech plus.

If you close the wall you will find less water fall. So we can control the flow of water with the help of valve. In the in the industry that that flow rate is controlling by the with the help of valve. Now by mistake with operated this is usually done by the operator increase the valve then there is a possibility that D_{max} will switch what to the $D_{washout}$ that is the major drawback that we have with the chemostat process.

And then question comes that what is the physical significance of the $D_{washout}$? Why the $D_{washout}$ take place? The reason is that one reason I can tell you that I am I talked about the generation time. What is the generation time? The time required for the cell division. Now $1/D$ is what? $1/D$ is the hydraulic retention time. Hydraulic retention time is how long you allow the liquid inside the reactor.

Now suppose the cell has some generation time. Suppose this whatever bacterial cell usually they have the generation time 15 to 20 minutes. Now if you if you allow the liquid less than 15 minutes or so maybe 10 minutes then what will happen you will not allow the bacteria to grow. Before it grow you are taking out the bacteria. So you are not getting any any cell in the reactor $D_{washout}$. So the another way I can explain the situation this is suppose this is chemostat process.

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Now now now now if you operate the chemostat process like this now now here I told you that there is in the major drawback of the chemostat process is that always there is a cell mass loss on the reactor. If the rate of cell mass that is going out of the reactor is more as compare to rate of growth of the cell. Then what will happen? The time will come when there is no cell present in the reactor. That is also that is why we come across the D washout in this reactor. So we are we should be very careful.


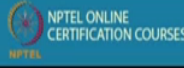
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Monod chemostat model

□ $D_{washout}$

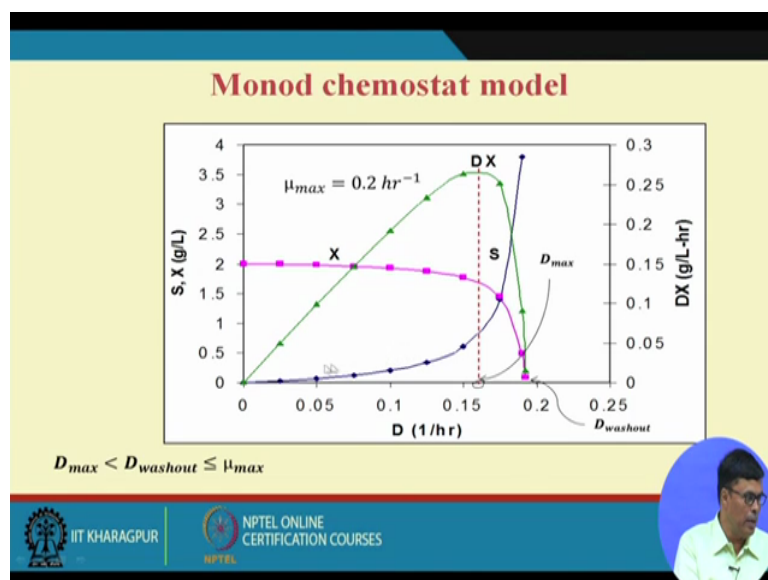
- As D increase, S increase slowly at first and then more rapidly as D approaches μ_{max} ; correspondingly, X decrease so that $X \rightarrow 0$ as $D \rightarrow \mu_{max}$. The condition at high dilution rate whereby X reduces to zero is known as 'washout'. The corresponding dilution rate is called $D_{washout}$
- The growth rate can no longer keep up with the dilution rate
- $D_{washout} = \frac{\mu_{max} S_0}{K_S + S_0}$

$D_{max} < D_{washout} \leq \mu_{max}$

We mention here as the D increases S also increases slowly at first and then more more rapidly as D approaches μ_{max} corresponding S decreases as X tends to 0. So this D wash out is equal to and the correlation between the D_{Max} , D wash out and μ_{max} is like this. D_{max} is less than D wash out and D washout is less or equal to μ_{max} .

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Now ((17:17)) that you know we can we can we can graphically I can explain like this this is DX that is like this and this is the typical one particular fermentation process there we have tried to find out this where μ_{Max} value is point 2. So here you see that D_{Max} is around this point 15 and where D wash out is then less than point 2.

You can see that is not exactly point 2. So it is usually the D Max is higher than D washout value. So you can you easily find out and they are very close point 15 and this is about to less than point 2. So this is very close. So even little increased in flow rate there is it possible we can meet the situation.



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Parameters estimation for Monod chemostat model

□ From the Monod chemostat model

$$D = \frac{\mu_{max}S}{K_S + S}$$

$$\frac{1}{D} = \frac{K_S + S}{\mu_{max}S}$$

$$\frac{1}{D} = \frac{K_S}{\mu_{max}} \frac{1}{S} + \frac{1}{\mu_{max}}$$



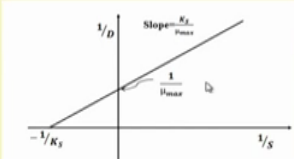


And now they do this how we can find out that.

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Parameters estimation for Monod chemostat model

$$\frac{1}{D} = \frac{K_S}{\mu_{max}} \frac{1}{S} + \frac{1}{\mu_{max}}$$

Plotting $\frac{1}{D}$ vs $\frac{1}{S}$ yields the value of K_S and μ_{max}

Now this kinetic constant of this of this mu max and KS we can determine the continuous process also. If we plot 1 by the D buses 1 by S we can have this line of ((18:31)) and from

the slope we can get the value of K_S by μ_{max} and intercept we can find out. So this constant value we can find out both by operating the chemostat as well as the batch process.

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Drawbacks of the chemostat operation

- ❑ Usually D_{max} is very close to $D_{washout}$, it may not be practical to operate at D_{max} . Small variation of dilution rate in this region can cause large fluctuations in X and S , unless the dilution rate is controlled very precisely, washout may occur.
- ❑ A major drawback of chemostat is that they work best at lower dilution rates where the changes in X and S are small.
- ❑ To keep the cell concentration higher than the normal steady state level, cells in the effluent can be recycled back to the reactor

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So the drawbacks of the batch process as I mentioned that mainly the D washout problem that we have and how it can be avoided ((18:56)) it can be avoided ((18:59)) by two ways either you recycle the cell mass to the reactant whatever the excessive that is going out of the reactor you recycle back. The same cell to the reactor and other otherwise cell on the solid Matrix no cell out cell washout the reaction take place.

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Chemostat with recycle

- ❑ To keep the cell concentration higher than the normal steady-state level in a chemostat, cells in the effluent can be recycled back to the reactor
- ❑ Cell recycle increases the rate of conversion (or productivity)
- ❑ Increase stability by dampening perturbations of input stream properties
- ❑ Cell mass balance around the chemostat

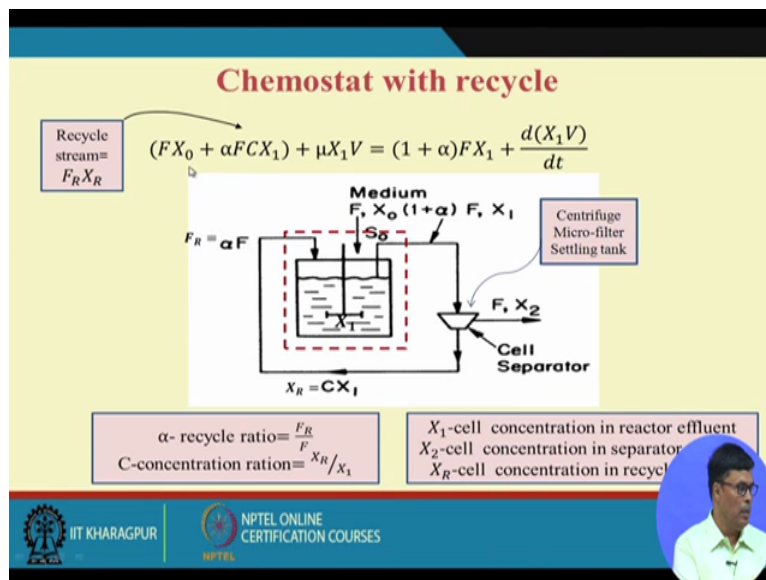
$$\text{Input} + \text{cell generation} = \text{output} + \text{cell death} + \text{accumulation} \quad =0$$

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Now and let me discuss that how you can analyse the chemostat cell mass recycling because the major drawback that we have with the chemostat that can be overcome by recycling and this is adopted by the different industry. I can give the example of activated sludge process. Activated sludge process is largely used by the industry for wastewater treatment process because this is easily operated.

And here this is activated sludge process is nothing but cell mass recycling. The cell mass recycling increase the rate of conversion and increase the stability by dampening perturbation like this. So we can write the balanced equation is the inputs alienation output so it will be assumed to be zero and Accommodation.

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This is this is the equation I can write and alpha is the recycle ratio. Recycle ratio means I told you that what you do that here whatever the cell mass is going out with a pass through cell separator a part of the cell will recycle back to the reactor and part of the cell you going out of the reactor what do you call cell mass wasting from the reactor. The and here we can take out the supernatant here another way we can take a separator.

So if that recycle will be the flow rate, if this is the recycle flow rate and if improve flow rate then f is considered as alpha. What is considered as the recycle ratio and XR is the second cell mass concentration. This is the cell separator. It separate the cell how easy easiest way of cell separation in the sedimentation another way is by centrifugation also you can separate the cell.

So you get the concentrated cell and peace with this is concentration with the XR and XR by the X X1. That is that is going out here. This is output cell mass concentration we can assumed to be see. Now obviously the XR XR and X X1 that should be always greater than one because under no circumstances it is less than 1 because XR is the second cell mass concentration and this is the suspended cell mass concentration.

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Chemostat with recycle

- At steady state (SS) condition, accumulation=0

$$(FX_0 + \alpha FCX_1) + \mu X_1 V = (1 + \alpha)FX_1$$
- For sterile feed ($X_0 = 0$)

$$\alpha FCX_1 + \mu X_1 V = (1 + \alpha)FX_1$$

$$\alpha \frac{F}{V} CX_1 + \mu X_1 = (1 + \alpha) \frac{F}{V} X_1$$

$$\alpha DCX_1 + \mu X_1 = (1 + \alpha)DX_1$$

$$\alpha DC + \mu = (1 + \alpha)D$$

$$\mu = \frac{(1 + \alpha - \alpha C)D}{1}$$

$$As$$

$$D = \frac{F}{V}$$

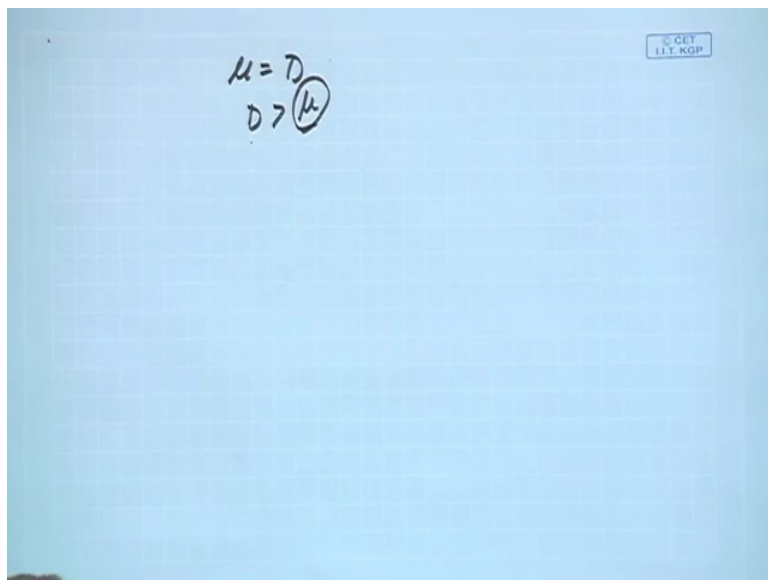
$$\mu = [1 + \alpha(1 - C)]D \quad \dots\dots (1)$$
- Since, $C > 1$ and $\alpha(1 - C) < 0$ then $\mu < D$. It implies that a **chemostat can be operated at dilution rates higher than the specific growth rate when cell recycle is used.**

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Now and we we write this balance equation the we try to analyse this equation and we come across the equation mu equal to 1 plus Alpha 1 minus C into D. This is very important because C as I told you C value always greater than one if it is greater than 1 then what will happen? This will be negative and if this this is the recycling ratio and this one minus negative will be less than 1 and so D will be mw Divided by fraction.

It can be operated at the higher higher growth rate that can be operated employees that chemostat can be operated at the dilution higher than the specific growth rate of the cells because I can show you that in case to steady state condition that mew equal to D.

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I have already shown you now here μ is a greater greater than D is greater than μ . So we can operate that your cell will not be wash out from the system. We can operate that that that that.

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Chemostat with recycle

- At steady state (SS) condition, accumulation=0

$$(FX_0 + \alpha FCX_1) + \mu X_1 V = (1 + \alpha)FX_1$$
- For sterile feed ($X_0 = 0$)

$$\alpha FCX_1 + \mu X_1 V = (1 + \alpha)FX_1$$

$$\alpha \frac{F}{V} CX_1 + \mu X_1 = (1 + \alpha) \frac{F}{V} X_1$$

$$\alpha DCX_1 + \mu X_1 = (1 + \alpha)DX_1$$

$$\alpha DC + \mu = (1 + \alpha)D$$



$$\mu = (1 + \alpha - \alpha C)D$$

$\mu = [1 + \alpha(1 - C)]D$

..... (1)

As
 $D = \frac{F}{V}$

- Since, $C > 1$ and $\alpha(1 - C) < 0$ then $\mu < D$. It implies that a chemostat can be operated at dilution rates higher than the specific growth rate when cell recycle is used.

That is why we have written here chemostat that can be operated at the dilution rate higher than the specific growth rate when the cell recycling is used.

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Chemostat with recycle

- Substrate balance around the chemostat
 Input = output + consumption + accumulation
- At steady state, accumulation=0

$$(FS_0 + \alpha FS) = (1 + \alpha)FS + (-r_s)V$$

Fresh feed

Recycled feed

Out stream from reactor

consumption


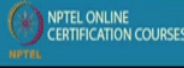
$$(FS_0 + \alpha FS) = (1 + \alpha)FS + \left(\frac{1}{Y_{X/S}}\mu X_1\right)V$$

$$F(S_0 - S) = \left(\frac{1}{Y_{X/S}}\mu X_1\right)V$$

$$\frac{F}{V}(S_0 - S) = \left(\frac{1}{Y_{X/S}}\mu X_1\right)$$

$(-r_s) = -\frac{dS}{dt} = \frac{1}{Y_{X/S}} \frac{dX}{dt}$
 $= \frac{1}{Y_{X/S}} \mu X$

$D = \frac{F}{V}$

So you can this can be calculated in other way this is fresh feed FS_0 , this is recycle feed, this is out going and this is the subject consumption. This is on the basis of substrate balance we can also write the equation like this.

(Refer Slide Time: 23:35)

Chemostat with recycle

$$D(S_0 - S) = \left(\frac{1}{Y_{X/S}}\right) \mu X_1$$


$$X_1 = \frac{D}{\mu} Y_{X/S} (S_0 - S) \quad \dots\dots\dots (2)$$

□ Substituting equation (1) into equation (2) yields

$$X_1 = \frac{Y_{X/S} (S_0 - S)}{[1 + \alpha(1 - C)]} \quad \dots\dots\dots (3)$$

□ Therefore, the steady-state cell concentration in a chemostat is increased by a factor of $\frac{1}{[1 + \alpha(1 - C)]}$

□ The substrate concentration in the effluent is determined from the equation (1) applying Monod equation

$$\frac{\mu_{max} S}{K_S + S} = [1 + \alpha(1 - C)] D$$


Now finally we come across this X1 equal to this value. The X1 equal to value can be taken therefore the steady state condition the chemostat increased by a factor. The cell mass factor is this one. The cell mass factor is by this. The substrate concentration of effluent is determined by the equation for monod equation can be expressed by this equation.

(Refer Slide Time: 24:05)



Chemostat with recycle

$$\frac{\mu_{max} S}{K_S + S} = [1 + \alpha(1 - C)] D$$

$$\frac{K_S + S}{S} = \frac{\mu_{max}}{[1 + \alpha(1 - C)] D}$$

$$\frac{K_S}{S} + 1 = \frac{\mu_{max}}{[1 + \alpha(1 - C)] D}$$

$$\frac{K_S}{S} = \frac{\mu_{max} - [1 + \alpha(1 - C)] D}{[1 + \alpha(1 - C)] D}$$

$$S = \frac{K_S [1 + \alpha(1 - C)] D}{\mu_{max} - [1 + \alpha(1 - C)] D} \quad (4)$$



Now chemostat with recycling at further analyze and we find out the value of S like this.



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Chemostat with recycle

□ Now, X_1 can be expressed as

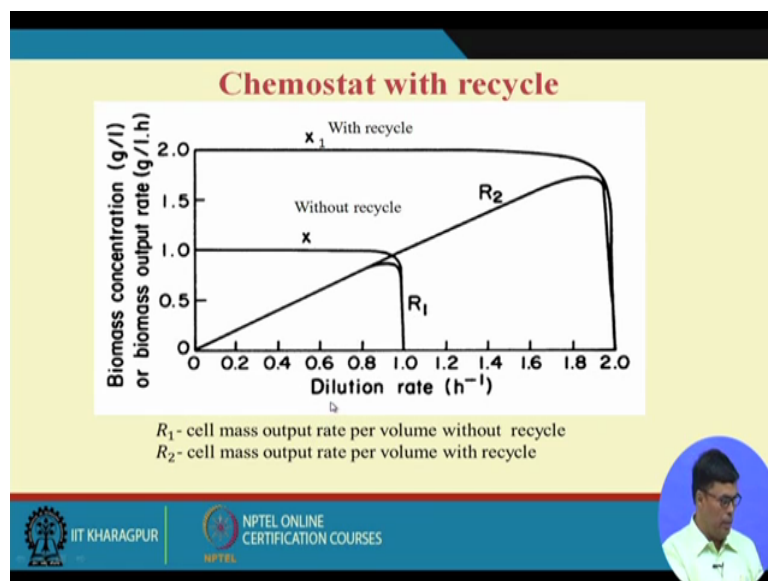
$$X_1 = \frac{Y_{X/S}}{[1 + \alpha(1 - C)]} \left[S_0 - \frac{K_S [1 + \alpha(1 - C)] D}{\mu_{max} - [1 + \alpha(1 - C)] D} \right]$$

□ Cell concentrations and productivities are higher with cell recycle, resulting in higher rates of substrate consumption



And then we can express the like this and the cell concentration and productivities are higher with the cell recycling result in the higher rate of substrate consumption.

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Now here that interesting thing is that



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Chemostat with recycle

□ Now, X_1 can be expressed as

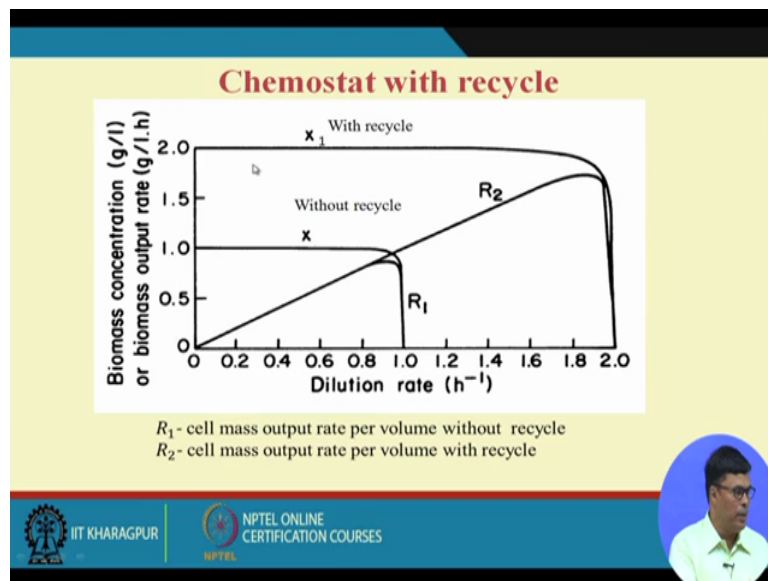
$$X_1 = \frac{Y_{X/S}}{[1 + \alpha(1 - C)]} \left[S_0 - \frac{K_S [1 + \alpha(1 - C)] D}{\mu_{max} - [1 + \alpha(1 - C)] D} \right]$$

□ Cell concentrations and productivities are higher with cell recycle, resulting in higher rates of substrate consumption

That here we find that X is increases.

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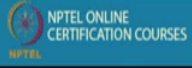



Now here that you see that in case of cell mass without recycling that X value that this is a dilution rate. Here we get a one might be the that C is approximately this is equal to cell wash out but when you do the recycling this is shifting to the two. That means you can operate it much higher dilution rate. Because that is the advantage of cell mass recycling that you know if you increase the dilution rate is increased if you if you do the recycling the dilution operating that can be increased a great extent.

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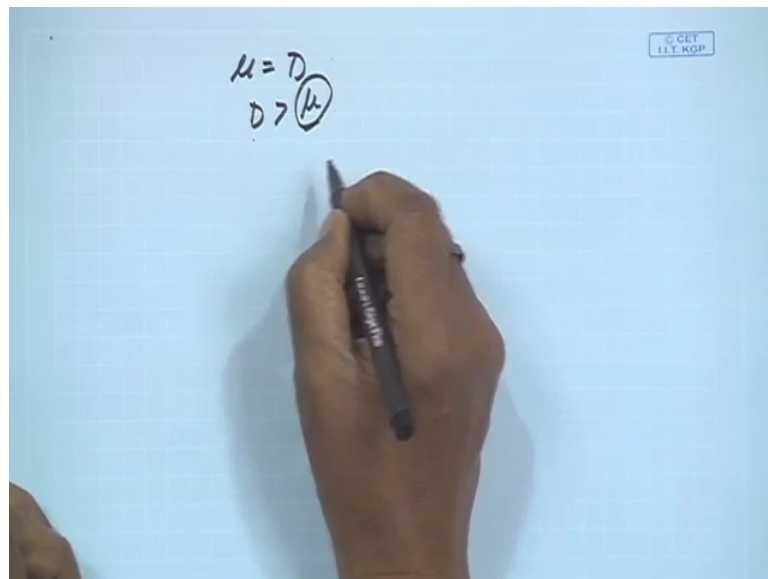
Multistage chemostat in series

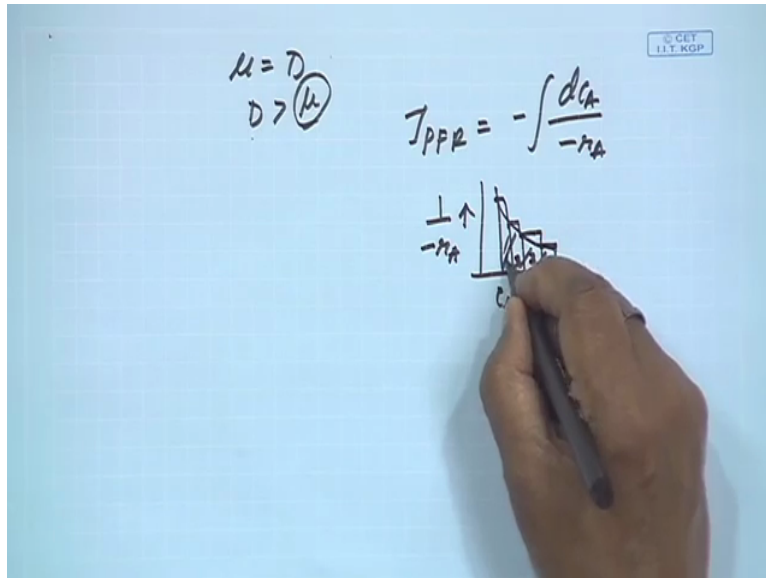
- ❑ For secondary metabolite production, the growth and product-formation steps need to be separated, since optimal conditions (temperature, pH and limiting nutrients) for each step are different. As a result multistage chemostat is employed
- ❑ **Assumption**
 - Steady state operation
 - No substrate addition in the consecutive stages
 - Balanced growth in all the stages



Now I want to point out that how to operate the multistage that chemostat in a series.

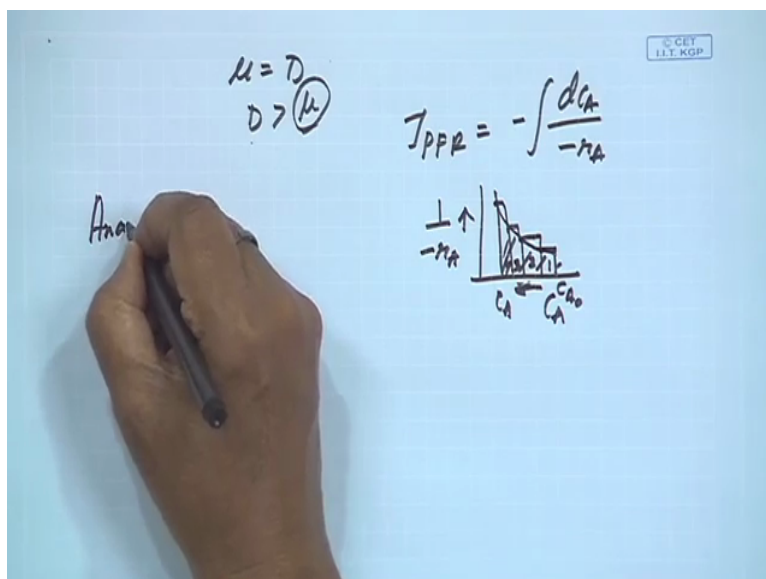
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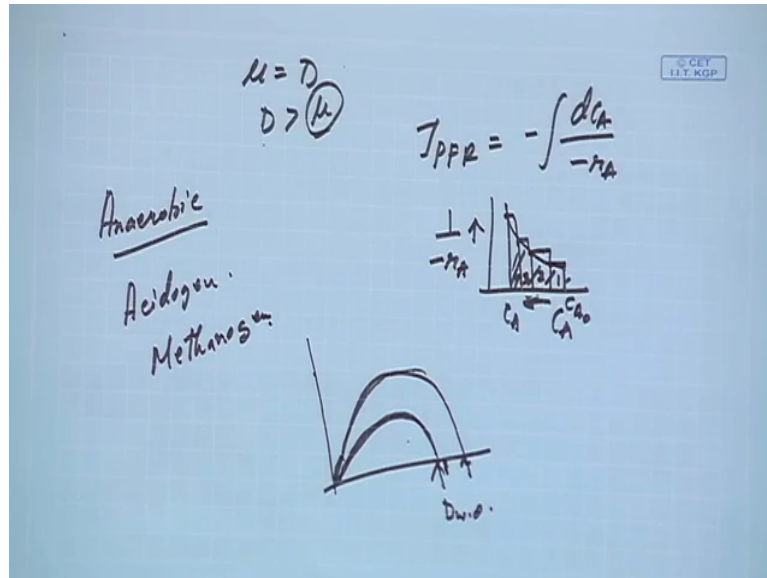




Multistage chemostat in series

- ❑ For secondary metabolite production, the growth and product-formation steps need to be separated, since optimal conditions (temperature, pH and limiting nutrients) for each step are different. As a result multistage chemostat is employed
- ❑ Assumption
 - Steady state operation
 - No substrate addition in the consecutive stages
 - Balanced growth in all the stages





Because what you call cascade type of fermenter. Cascade because I you can you can remember that in case of reaction kinematics we have come across this plug flow reactor. In case of plug flow reactor we have come across this equation. This minus DCA equal to minus RA. Now here I try to point out that minus RE if you plot by CA.

And if you have this this kind of thing and this is the this is the as the CA value decreases this is CA 0 to CA 1 by RA increases that means RA decreases. That is actually take place in case of product innovation because because as the substrate concentration decreases the innovation occur that means rate of reaction decreases and at this situation plug flow reactor is mandatory.

Now we observe this plug flow reactor is very difficult to operate because plug flow reactor there should not be any kind of back mixing. Now if you have been in place of that if you have multiple CSTR in series then that will be equivalent to plug flow reactor. 1 2 3 4 so this is exactly we we try to find out for secondary metabolite production that the growth and product formation steps to be separated optimal stage.



And multistage of the state process that we can not only that we can we can have because I can tell you this very interesting that in the anaerobic dilution process we have to type of culture one is called as acidogou and another is methanogens is going as compared to be the reasons so if you if you if this is available if you want to separate the acidegens from the methanogens you can do it very easily.

Because you have you have this picture is like this one is this and that is this so this is this is this for your methanogens and this is what acidegens. So if you here this is D wash out. For this is methanogens and this is D wash out for methanogens and acidegens. So if you use the dilution rate higher then this methanogens will be totally wash out from the mixed culture so.

(Refer Slide Time: 28:06)

Multistage chemostat in series

- ❑ For secondary metabolite production, the growth and product-formation steps need to be separated, since optimal conditions (temperature, pH and limiting nutrients) for each step are different. As a result multistage chemostat is employed
- ❑ **Assumption**
 - Steady state operation
 - No substrate addition in the consecutive stages
 - Balanced growth in all the stages

Multistage chemostat in series

- ❑ Assumed a two stage chemostat model
- ❑ Cell mass balance in 1st stage

$$FX_0 + r_x V_1 = FX + r_d V_1 + \frac{d(XV_1)}{dt}$$

At steady state, accumulation=0

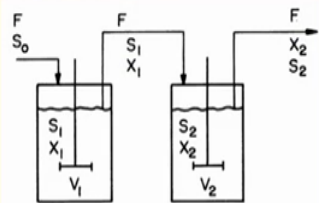


$$\mu_1 XV_1 = FX$$

$$\mu_1 = \frac{F}{V_1}$$

$$\mu_1 = D_1$$

Sterile feed, $X_0 = 0$
 Negligible endogenous metabolism, $r_d \rightarrow 0$

$\mu_1 = \frac{\mu_{max} S_1}{K_s + S_1}$

This is another advantage of this the different with the help of dilution at we can do this. Now in case of multistage and this is usually assume the steady state operation. No substrate addition for change of phase unbalanced growth occurs in this is like this this is substrate is coming again whatever substrate ((28:29)) we put it in the second reacted.

So then more substituted but for the first reacted we don't have analysis is not problem. Because we assume it in the serial field we have already done we have to easily find out the value of S1 and X1 in this reactor.

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Multistage chemostat in series

Substrate balance

$$FS_0 = FS_1 + (-r_s)V_1 + \frac{d(V_1S_1)}{dt}$$

At steady state, accumulation part is zero

At steady state
 $D_1 = \mu_1$

$$\frac{F}{V_1}S_0 = \frac{F}{V_1}S_1 + \left(\frac{1}{Y_{X/S}}\right)\frac{dX_1}{dt}$$

$$D_1(S_0 - S_1) = \frac{1}{Y_{X/S}}\mu_1 X_1$$

$$(S_0 - S_1) = \frac{1}{Y_{X/S}}X_1$$

$$X_1 = Y_{X/S}(S_0 - S_1)$$

$(-r_s) = -\frac{dS}{dt} = \frac{1}{Y_{X/S}}\frac{dX}{dt}$
 $= \frac{1}{Y_{X/S}}\mu X$
 $Y_{X/S} = -\frac{dX}{dS}$

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Multistage chemostat in series

Cell mass balance for the second stage yields

Input + generation = output + death + accumulation

$$FX_1 + \mu_2 X_2 V_2 = FX_2 + \frac{d(X_2 V_2)}{dt}$$

For negligible endogenous metabolism, death $\rightarrow 0$
 $D_2 = \frac{F}{V_2}$

At steady state, accumulation = 0

$$FX_1 + \mu_2 X_2 V_2 = FX_2$$

$X_1 = Y_{X/S}(S_0 - S_1)$

$$\mu_2 = \frac{F}{V_2} \left(1 - \frac{X_1}{X_2}\right) = D_2 \left(1 - \frac{X_1}{X_2}\right) \dots\dots\dots(5)$$

Where, $X_1 < X_2$, so $D_2 > \mu_2$

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Multistage chemostat in series

- Substrate balance for the second stage yields
 Input = output + consumption + accumulation
- At steady state, accumulation = 0


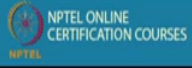

$$D_2 = \frac{F}{V_2}$$

$$FS_1 = FS_2 + \frac{\mu_2}{Y_{X/S}} X_2 V_2$$

$$S_2 = S_1 - \frac{\mu_2}{Y_{X/S}} X_2 \frac{1}{D_2} \quad \dots\dots\dots (6)$$

Equation (5) and (6) can be solved simultaneously for X_2 and S_2 by substituting

$$\mu_2 = \frac{\mu_{max} S_2}{K_S + S_2}$$

Now when you go to the second reactor, we shall have to do the material analysis. We shall have to do the substrate balance and we shall have to find out what is the X_1 and X_2 value that you have. We can calculate S_2 and X_2 value in the second reactor. We can calculate separately then you want to go to the third reactor.

And you have to do the similar type of analysis like this you can do the cascade type of analysis of the different reactors find out the different cell mass concentration and different type of reactor.

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Comparison between cascade chemostat and plug flow reactor

It can also be shown theoretically that as the number of stages in a chemostat (CSTR) cascade increase, the conversion characteristics of the entire system approach those of an ideal plug flow or mixed batch reactor

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So let me stop here today because we shall we shall continue this lectures and then the next class I will discuss some problem also so that whatever things I discuss this will be little bit clear to you. Now in this lecture I tried to point out that the major drawback of chemostat process is that cell mass that is wash out and this can be overcome by the recycling.

And by through recycling is it possible not only to operate at high dilution rate but at the higher dilution rate we increase the cell mass concentration to a great extent. The major concept of of the cell D wash out I try to explain that 1 by D is considered the higher retention time if we have hydraulic retention time less than that cell the cell division time required for the generation time.

Then say you are not $(30:31)$ the cell to grow that is why the cell wash out take place on how we can explain in other way if a Cell mass that is going out of the reactor is more as compared to cell mass that is growing in the system. If you allow the system to continue for longer period time we always meet the situation of D wash out. So this we can we can we easily separate by using the recycling of the cell.

And also also we discussed in the last previous classes immobilization of the whole cell. The immobilization of the whole cell we can hold a cell in the solid metric so that no wash out of the cell will take place. So we discuss I think in the coming lectures we try to try to discuss some compression of the chemostat and plug flow reactor then I shall discuss about this some

problem so that your how this can be applied for solving some kind of fermentation in the problem of the fermentation industry. Thank you very much!