

**Advanced Control System Design**  
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**Lecture No. # 39**  
**Integrator Back-Stepping; Linear Quadratic (LQ) Observer**

We are almost at the end of this course, we are just at a lecture number 39 (Refer Slide Time: 00:19). Towards the end I thought, we will study some of this modern control technique, especially for the non-linear (( )) philosophy. One of that (( )) to be **integrated** integrator back stepping in something on that we are going to study today actually.

Towards the end of this lecture, I will also talk about linear quadratic observers, which are essentially leads towards Kalman filters and all that actually. And that this two are this, not related topics just put together, because **because** of like time is sufficient to discuss both the things today actually.

**Alright**, so philosophy of non-linear control designs using Lyapunov theory is something like this they (( )) this back stepping design uses Lyapunov theory extensively. So, what is the generic philosophy, suppose somebody wants to use a Lyapunov theory for in a control design, then what is the idea there actually?

(Refer Slide Time: 01:14)

**Philosophy of Feedback Control Design Using Lyapunov Theory**


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Motivation:  $\dot{X} = f(X, U)$

Goal: Design  $U = \varphi(X)$  such that  
 $\dot{X} = f(X, \varphi(X))$  is asymptotically stable

Design Idea:

- \* Choose a pdf  $V_1(X)$
- \* Make  $\dot{V}_1(X) \leq -V_2(X)$ , where  $V_2(X) > 0$  (pdf)

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3

Something is the idea is something like this. Let us, say you have a non-linear system  $\dot{X}$  is  $f$  of  $X$   $U$ , where you want to design a control  $U$  in those straight feedback form, which is like  $\phi$  of  $X$ . So,  $U$  has to be as a function of  $X$ ,  $\phi$  of  $X$  such that, this once you put it back into the system dynamics that is  $\dot{X}$  is  $f$  of  $X$  and then,  $\phi$  of  $X$  that system  $(\ )$   $(\ )$  system dynamics should be asymptotically stable. That is **that is** the ultimate objective for Lyapunov  $(\ )$  control theory actually.

So, what is the idea there I mean how do you  $(\ )$   $(\ )$   $(\ )$  happens actually? So, the idea here is, first you choose a positive definite function  $V_1$  let say; and  $(\ )$  of  $V_1$  dot is less than equal to negative of  $V_2$ , where  $V_2$  a positive definite function. And remember these are all like sufficiency conditions and all that. So, you will not be operating in a optimal way, but you will be operating on a conservative way basically, that is **ok**.

So, **what do** what you essentially do is, we select a Lyapunov function  $V_1$  of  $X$  and make sure that  $V_1$  dot of  $X$  which is once you take  $V_1$  dot it is related to the system dynamically anyway. So, this  $V_1$  dot of  $X$  should be less than equal to minus  $V_2$  of  $X$  will be to itself is a positive definite function. So, negative of  $V_2$  is negative definite function. So, we want to make sure that  $V_1$  dot is less than equal to another negative definite function that way. So, that is the whole **whole** idea design idea basically.

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### Feedback Control Design Using Lyapunov Theory: An Example

**Problem:** Design a stabilizing controller for the following system

$$\dot{x} = ax^2 - x^3 + u$$


**Solution:** Let  $V_1(X) = \frac{1}{2}x^2$

$$\begin{aligned} \dot{V}_1 &= x \dot{x} = x(ax^2 - x^3 + u) \\ &= ax^3 - x^4 + xu \end{aligned}$$

Let us choose  $V_2(X) = x^2$

$$\therefore \dot{V}_1(X) \leq -V_2(X)$$

$$\Rightarrow ax^3 - x^4 + xu \leq -x^2$$



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4

So, let us see a small example if you are talking in lot more formal theory and think like that. So, this is a simple scalar problem, where  $\dot{x}$  is a  $x^2$  minus  $x^3$  plus  $u$ . And we want to design a straight feedback control  $u$ , so that the closed loop system is asymptotically stable, that is the objective actually.

So, we have to select  $V_1$  first. So, let say  $V_1$  will say will naturally select quadratic function half of  $x^2$ . So,  $\dot{V}_1$  happens to be  $x \dot{x}$ . Obviously, because  $\frac{d}{dt} V_1$  by  $\frac{d}{dt} x$  is  $x \dot{x}$ ; and  $\dot{x}$  is this from dynamic what you see here, so we put it back here. So, essentially  $\dot{V}_1$  is something like this (Refer Slide Time: 03:30), now this  $\dot{V}_1$  has to be less than equal to negative of a positive definite function.

So, we have to select another  $V_2$  like that. So, let us say select  $V_2$  is  $x^2$  basically let say, just you can select any positive definite function for say, this is a just one of those selections. And we want to make sure that, this in equalities valid actually. So,  $\dot{V}_1$  is less than equal to negative of  $V_2$ . So, if you put  $\dot{V}_1$  in this expression (Refer Slide Time: 03:56), so this expression is less than equal to negative of  $x^2$ .

(Refer Slide Time: 04:01)

### Philosophy of feedback control Design Using Lyapunov Theory

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$$\dot{x} \leq -x^2 + x^3 - ax^3$$

i.e.  $u = -x + x^3 - ax^2$

Analysis:  $\dot{x} = ax^2 - x^3 - x + x^3 - ax^2$   
 $\dot{x} = -x$

Advantage: The closed loop system is globally asymptotically stable.

Problem: The beneficial nonlinearity got cancelled.  
 (which is not desirable)

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So, then from where you want to solve for a controller that means this  $\dot{x} = -x^3 + u$  is less than equal to this  $\dot{V} = -x^3 + u$  expression (Refer Slide Time: 04:07), and equal to sign will also be evaluated. So, will take equal to actually and then make sure that,  $u$  is equal to that  $u = x^3$ .

So, we cancel out  $x$  in both side,  $1 - x^2$  will go from both side and then, we have the  $u$  is in minus  $x$  plus  $x^3$  minus  $a x^2$ . So, is it control good or bad I mean naturally, it is good; because we have make sure that  $V$  dot is  $\dot{V} = -x^3 + u$  negative definite function anyway. But, still just cross check is about it, is just put it back this controller,  $u = x^3$  the system dynamics and then, try to analyse what is going on there.

So, if you put this  $\dot{x} = -x^3 + u$  system dynamics is  $\dot{x} = -x^3 + u$ . So, plus  $u$  whatever  $u$  we are getting, we will put it back. So,  $\dot{x} = -x^3 + u$ ,  $u$  is that portion actually; this portion is  $u = x^3$  like plus  $u = x^3$  (Refer Slide Time: 04:55). So, that  $u = x^3$  is what do you do.

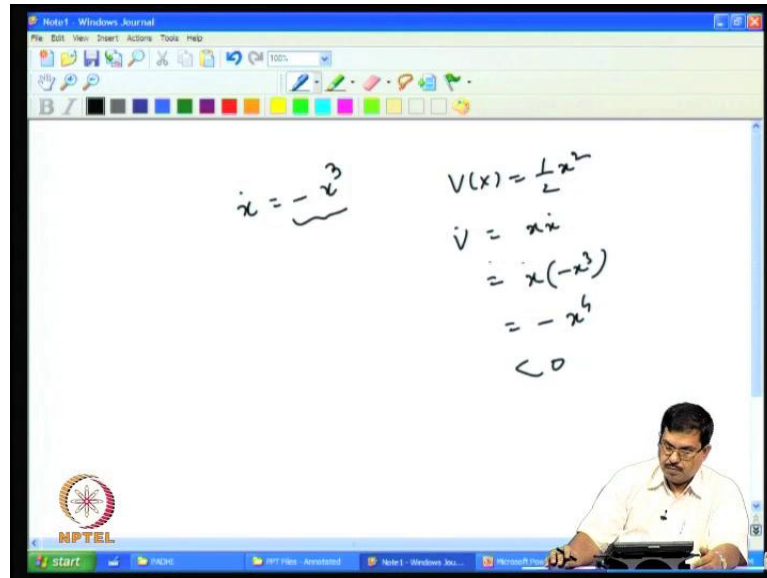
But, then once you put it back, these to these to are cancelled out (Refer Slide Time: 05:04), and plus  $x^3$  minus  $x^3$  also cancels out and you have left out is  $\dot{x} = -x^3$  actually. Then  $\dot{x} = -x^3$  is certainly a linear system dynamics actually; and obviously, because the Eigen values minus 1 obviously, the system will asymptotically stable. In fact, it is global asymptotically stable.

So, that is because this linear system dynamics ultimately, so it does not depend on cell condition  $\dot{V} = -x^3$  straight away from Eigen values you can say, it is globally asymptotically stable. So, that is the advantage here actually. So, you design a controller it is a non-linear controller in such a way that, the closed loop system becomes globally asymptotically very stable. But, what is the problem there, it is also problem it is a remember that, this  $V = \frac{1}{2} x^2$  Lyapunov theory these are like sufficiency condition and all that.

So, once you use that, the design can be actually conservative. And here, it is actually conservative design, primarily because this let us assume that; if you go back to this (Refer Slide Time: 06:08), this negative  $x^3$ ,  $\dot{x} = -x^3$  is actually stabilising term

that is **that is** also like easy to see. For example, is any **(( ))** power of like a scalar function if I take any **(( ))** power of X is a stabilising thing with negative sign.

(Refer Slide Time: 06:26)



For example, let say  $\dot{x}$  equal to minus  $x$  cube that **that** one if you are talking, then corresponding to that let us say Lyapunov function if you **if you** say it just half  $x$  square, then  $\dot{V}$  happens to be  $x \dot{x}$  this is nothing but,  $x$  times minus  $x$  cube. So, it is negative of  $x$  **(( ))**. So, this is actually negative definite function.

So, any **(( ))** power of  $x$  with a negative sign here will be actually stabilizing term. So, but that, what **what** happens here is, unnecessarily we have actually cancelled that out. So, this controller actually tries to cancel out the good part of it also basically. So, we do not want that normally. So, what we do, how do you about that? So, let us be, because this **this** small problem we should be able to try analyse this little bit more, just by looking at equations and all.

(Refer Slide Time: 07:15)

**Philosophy of feedback control Design Using Lyapunov Theory**

Let us choose:

$$V_2(X) = x^2 + x^4$$

Then

$$\dot{V}_1 \leq -V_2(X) \quad \text{leads to:}$$
$$ax^3 - x^4 + xu \leq -x^2 - x^4$$
$$ax^3 + xu \leq -x^2$$
$$ax^2 + u = -x \quad \text{or} \quad u = -x - ax^2$$

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So, let us see we select something like  $V_2$  I mean probably our  $V_2$  selection was wrong. So, will **will** revise this  $V_2$  selection and **(( ))** let us consider  $V_2$  as  $x^2 + x^4$  **(( ))**, this is also a positive definite function by the way. Now, if you go back to this inequality again that,  $\dot{V}_1$  is a negative less than I mean **negative** less than equal to negative of  $V_2$ .

Then the same analysis will tell that,  $u$  is instead like that (Refer Slide Time: 07:41), again you put it back; and then plus **a minus**  $x^4$  minus  $x^4$  will **will** get cancel out from both side, and you will be left out with that term actually. And here will be able to I mean cancel  $1x$  and all that actually, so anyway. So, that is **that is** what will happen here actually, so  $u$  will be like this. Again you go back and try to analyse what is a closed loop system.

(Refer Slide Time: 08:04)

**Philosophy of feedback control Design Using Lyapunov Theory**

Closed Loop system:  $\dot{x} = ax^2 - x^3 - x - ax^2$   
i.e.  $\dot{x} = -x^3 - x$

⇒ The destabilizing nonlinearity got cancelled,  
but the beneficial nonlinearity is retained !

Another Problem: If  $V_2(X) = x^2$ ,  
 $\dot{x} = -x$ , only if  $a$  is accurate

If the actual parameter value is  $\bar{a}$ , then the feedback loop operates with

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The slide features a photograph of a man in a white shirt sitting at a desk with a laptop, appearing to be presenting the content.

Then,  $\dot{x}$  is a is like this now, because that is that is my  $u$ ; in this case, this is my  $u$  now negative of  $u$ . Now, such this is plus  $u$ , because this this is our system dynamic actually. So, way to go back to this system dynamic and then, tell this is plus  $u$  here. So, you put it this  $u$ , whatever  $u$  we are getting here I will put it back; and then try to see that,  $\dot{x}$  is instead minus  $x$  cube minus  $x$ .

So, we are able to preserve this this beneficial nonlinearity by selecting a different way, so just just the message here. So, the design is not just unique design. So, it subject to different different selection of  $V_2$ ,  $V_1$  and all; you will end up with different control actually. But, all of them will be will be able to do the job, and all of them will have some degree of robustness also; because, these are all sufficiency conditions and all, robustness also comes into picture.

Now, let us see how it is say we suppose we go back to that that initial selection. Let us, say  $V_2$  whatever we selected initially is  $x$  square. So, will go back to that selection and with that selection, our closed loop system becomes something like  $\dot{x}$  equal to minus  $x$ ; but this  $\dot{x}$  equal to minus  $x$ , only if the parameter  $a$  is accurately (( )) remember that, this this entire thing, this this process of cancellation and all that. What we did here, this this a  $x$  square and a  $x$  square, what about this a  $x$  square and this a  $x$  square got cancelled out,

assuming that the way is known perfectly. But, if  $a$  is not known perfectly then, this  $a$  will be different from what is used in the controller that  $a$  will be different. And hence, you will not be able to cancel out.

(Refer Slide Time: 09:57)

**Philosophy of feedback control Design Using Lyapunov Theory**

$$\dot{x} = -x + (\bar{a} - a)x^2$$

Can be potentially destabilizing term if  $(\bar{a} - a)$  is high

i.e. The global stability reduces to local stability.

This excites robustness issues!

However, if  $V_2(X)$  is made "Sufficiently powerful", then the destabilizing effect can be minimized.

Hence, Lyapunov based designs can be "very robust"

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So, in that situation we will have additional term subject to this, this is not no more  $\dot{x}$  is minus  $x$ , this it will be  $\dot{x}$  equal to minus  $x$  plus an additional term with **with**  $x$  square actually. So, in this  $x$  square is certainly stabilizing term for I mean depending on this, how powerful is this  $\bar{a} - a$  is actually that means how much inaccuracy is there. **(( ))** whatever is inaccuracy, now because it is no more  $x$ , so it is minus  $x$ , this certainly this **this** global stabilities gone; and we can only conclude local stability, because globally this is no more valid actually, one is stabilizing term, other is **(( ))** stabilizing; so, obviously global thing no more actually.

However, if you make  $V_2$  sufficiently powerful that means  $V_2$  is large and large and thing like that; then obviously, the control will also go and take get more and more **(( ))** I mean powerful basically. So, essentially what you are telling, even in the presence of certainty like this, the design can be robust actually, because this term will not be that prominent at all actually.



If your  $V_2$  is very powerful then,  $V_1$  dot is minus of  $V_2 X$  any way. So, because that term is being very high quantity in thing like that, this will **this will** lead to  **$V_2$**  robust control actually. So, that is the whole idea, why this **this** Lyapunov theory based control are typically robust actually, **alright**. So, with that **(( ))** in the background let us study about this **this** integrator back-stepping method. And then this is generalization of this concept, what is discussed actually.

(Refer Slide Time: 11:33)

**Integrator Back-stepping**

**Problem :** Design a state feedback asymptotically stabilizing controller for the following system

$$\begin{cases} \dot{X} = f(X) + g(X)\xi \\ \dot{\xi} = u \end{cases}$$

where  $X \in \mathbb{R}^n$ ,  $\xi \in \mathbb{R}$ ,  $u \in \mathbb{R}$

Note:  $\begin{bmatrix} X \\ \xi \end{bmatrix} \in \mathbb{R}^{n+1}$ . State of the system,  $u$ : Control input (scalar)

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So for here, we need this system dynamics in a typical form and for that form will start with a simplified form of that version. And this is I mean towards end of this **this** topic we will see this is like what is call **(( ))** feedback system and all that actually. This is just one subset of that. So, what you are telling here is, let **let**  $X$  be  $n$  dimensional **(( ))**, let  $\xi$  be also state, where  $\xi$  dot simply  $u$ . So,  $X$  dot is  $f$  of  $X$  plus  $g$  of  $X$  times  $\xi$ , and  $\xi$  dot is simply  $u$  actually;  $\xi$  is scalar remember,  $\xi$  and  $u$  both are scalars actually.

So, if the system dynamics is given in this form, then I can think of using I mean this back-stepping idea and all that. So, remember that, these both together are the state vectors actually that means  $X$  and  $\xi$  together will define the states of the system. So, obviously the states of the system will be  $n$  plus  $1$  actually. And where is this **this (( ))** open think like that probably, if you see this any system dynamics in control affine form already and you want to

incorporate let us say actually dynamics also then, this is the original control variable; but, this part will be actual dynamics you want to see the total system that way, then it will **it will** **(())** something like this actually.

So, these are not very unrealistic problems in that sense basically. So, here **here** we are talking about single input, the control is scalar; and the xi state is also scalar any way. So, that is the form that you are talking.

(Refer Slide Time: 13:08)

**Integrator Back-stepping**

Assumptions:

- \*  $f, g : D \rightarrow \mathbb{R}^n$  are smooth
- \*  $f(0) = 0$
- \* Considering state  $\xi$  as a "control input" of subsystem (1) we assume that  $\exists$  a state feedback control law of the form  $\xi = \varphi(X), \varphi(0) = 0$ . Moreover,  $\exists$  a Lyapunov function  $V_1 : D \rightarrow \mathbb{R}^+$  such that

$$\dot{V}_1(X) = \left( \frac{\partial V_1}{\partial X} \right)^T [f(X) + g(X)\varphi(X)] \leq -V_1'(X), \forall X \in D$$

where,  $V_1'(X) : D \rightarrow \mathbb{R}^+$  is a pdf function.

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11

So, what are the assumption, assumption is first is f and g are both smooth I mean the derivative also continuous; f of 0 is 0 whatever f of 0 we are talking, here is should be 0. And if you consider this xi as a control input to this particulars state first part, first part of the equation is xi **(())** as a control variable.

So, if you **if you** consider that, then we assume that **(())** feedback control already in the form of xi equal to phi of X, where phi of 0 is 0. So, **that** that means assuming this is control variable, we have already within controller in appropriately I mean; so, what is that means? xi is already design as a function of X, where phi of 0 is 0. Because, it is a stabilizing controller, it also is a Lyapunov function with that.

So, the  $V_1$  Lyapunov function  $V_1$  such that  $\dot{V}_1$  which appears to be like this (Refer Slide Time: 14:04), it will be  $\frac{d}{dt} V_1$  by  $\frac{d}{dt} X$  into  $\dot{X}$ ,  $\dot{X}$  is like that anyway. So, that is less than equal to certain negative  $V_a$  of  $X$ , where  $V_a$  is a first definite function. That means, all that you are telling is first part let us consider is a as a separate problem, for which  $x_i$  is control variable; and that this  $x_i$  is actually already design as a straight feedback form with all good behaviour basically.

So, but again problem we need to design this  $x_i$  also basically that way. And as I told, this back-stepping design is kind of very popular for incorporating actual dynamics into the system and all that actually, so anyway. So, this is the assumption here. Now, what we want to do? Now, we want to design  $u$ , we can think of that as input the  $\dot{X}$  probably. So, that the overall system remains a stable actually. So, that is the problem here actually.

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### Integrator Back-stepping


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An important observation:

When  $X = 0$ ,  $\xi = \varphi(0) = 0$  &  $\dot{X} = f(0) = 0$   
 (i.e. everything is nice)

However, when  $\xi \rightarrow 0$ ,  $\dot{X} = f(X)$  and hence  $X \not\rightarrow 0$   
 in general. That is the core problem!

$\therefore$  We need some algebraic manipulation as follows.



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12

So, let us see how do you do that, but observation let say one important observation before you move further. Let us consider, what happens when  $X$  is already equal to 0,  $X$  is gone to let say  $X$  equal to 0 as already achieved then what happens. Now, remember  $\varphi$  of  $X$  by definition  $\varphi$  of 0 is a 0 anyway, that is what, that is how this  $x_i$  is already designed. So,

when  $X$  equal to 0, then  $\phi$  of 0 is 0 that means  $x_i$  is also 0. So, this part is 0 anyway. And then,  $f$  of 0 is 0 by assumption.

So,  $\dot{X}$  become 0. So, no  $(( ))$ , so when  $X$  goes to 0,  $\dot{X}$  is already 0. So, that is  $\text{that is}$  fine actually. So, the system will go to equilibrium condition and it will stay there. Then that is more important actually, that is not a problem. But, then the problem happens in another way round; like what happens when  $X$  goes to 0 nothing not a big problem actually.

But, what if this  $x_i$  goes to 0, when  $x_i$  goes to 0 this  $\text{this this}$  system dynamics, the first part of the system dynamics is almost becomes  $(( ))$  homogeneous dynamics actually,  $x_i$  can go to 0. So, this part is not there, but  $\dot{X}$  is a  $f$  of  $X$  that  $\text{that}$  system is no guarantee that,  $X$  will go to 0 that system dynamic is homogeneous dynamic. They I mean the only in the closed loops sense,  $X$  will go to 0 that that is how the guaranties already there.

That we are already design a feedback control  $\text{of that}$  for that behaviour, but for the homogeneous system  $\text{you know } (( ))$  actually that means, when  $x_i$  goes to 0 we are not very sure that whether  $X$  will go to 0 or not actually. That is not a  $(( ))$ , that is not a allowed actually, because our  $\text{our}$  total aim, the final aim is to make sure that,  $X$  goes to 0 also  $(( ))$ . So, how do you do that? So, that  $\text{that}$  is the core problem actually; so for that, we need to do some algebraic manipulation as follows.

(Refer Slide Time: 16:57)

**Integrator Back-stepping**

Step - 1:

$$\begin{aligned}\dot{X} &= f(X) + g(X)\xi + g(X)\varphi(X) - g(X)\varphi(X) \\ &= f(X) + g(X)\varphi(X) + g(X)\underbrace{[\xi - \varphi(X)]}_z \\ &= f(X) + g(X)\varphi(X) + g(X)z\end{aligned}$$

By this construction, when  $z \rightarrow 0$ ,  $\dot{X} = f(X) + g(X)\varphi(X)$  which is asymptotically stable (i.e.  $X \rightarrow 0$ )!

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So, let see what we do there. So, for this **this** particular system dynamics first part of it, it contain only this part  $f$  of  $X$  plus  $g$  of  $X$  times  $\xi$ . So, now let us add and subtracts this two terms actually. So, this will add  $g$  of  $X$  times  $\varphi$  of  $X$ , and subtract  $g$  of  $X$  times  $\varphi$  of  $X$ . when need do this operation, let us let us consider this **this** part of it, we will skip it, remember this  $\varphi$  of  $X$  is the same  $\varphi$  of  $X$  that we are talking actually here,  $\xi$  is already design in the form of  $\varphi$  of  $X$  actually.

So, it is just an algebraic manipulation sort of it actually. So, what **what** you are doing here? So, we are keeping this part of it here, then this **this** part and that part will combine and then, tell this is **this is** what will happen actually. So,  $g$  of  $X$  times  $\varphi$  of  $X$  plus  $g$  of  $X$  times  $\xi$  minus  $\varphi$  of  $X$ ; obviously, we are not changing anything here I mean a system dynamics we are just I mean playing around with little algebraic actually, without altering the system dynamic.

Now, with this change or **(( ))** this  $\xi$  minus  $\varphi$  of  $X$  let me define as something like a new variable  $z$  actually. So, I am just defining that for **for (( ))** simplicity **(( ))**. Once I do this, this definitions  $z$  then the system dynamics will nothing but **(( ))**,  $f$  of  $X$  plus  $g$  of  $X$  times  $\varphi$  of  $X$  plus  $g$  of  $X$  times  $z$  **for of  $X$  plus  $g$  of  $X$  time  $z$**  actually.

Now, what actually, earlier when zeta goes to I mean xi going to 0, then we had a problem. But, what if the same problem is there or not? When you see this system dynamics in this way that means when **when** z goes to 0, this system is no more like only f of X; this system is f of X plus g of X times phi of X. And phi of X is design will appropriately already basically. That means when z goes to 0, this system dynamics is no more and purely open loop system dynamics, actually closed loop system dynamics. And hence, this asymptotically stable anyway, so X will go to 0.

So, the problem that we had that, when xi goes to 0, X will not go to 0 in general; that does not happen, when z goes to 0. When z goes to 0, X is gone to I mean supposed to go to 0 is basically. So, that problem will overcome that way basically. Now, how do you do further algebra, because we have to put it into this form, that form has to be there actually anywhere.

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**Integrator Back-stepping**

$$\dot{z} = \dot{\xi} - \dot{\varphi}$$

$$= \underbrace{u - \dot{\varphi}}_v$$

[This is backstepping, since  $\varphi(X)$  is stepped back by differentiation]

So, we have

$$\begin{cases} \dot{X} = f(X) + g(X)\varphi(X) + g(X)z \\ \dot{z} = v \end{cases}$$

[This system is equivalent to the original system]

Note:  $\dot{\varphi} = \left(\frac{\partial \varphi}{\partial X}\right)^T \dot{X} = \left(\frac{\partial \varphi}{\partial X}\right)^T [f(X) + g(X)z]$

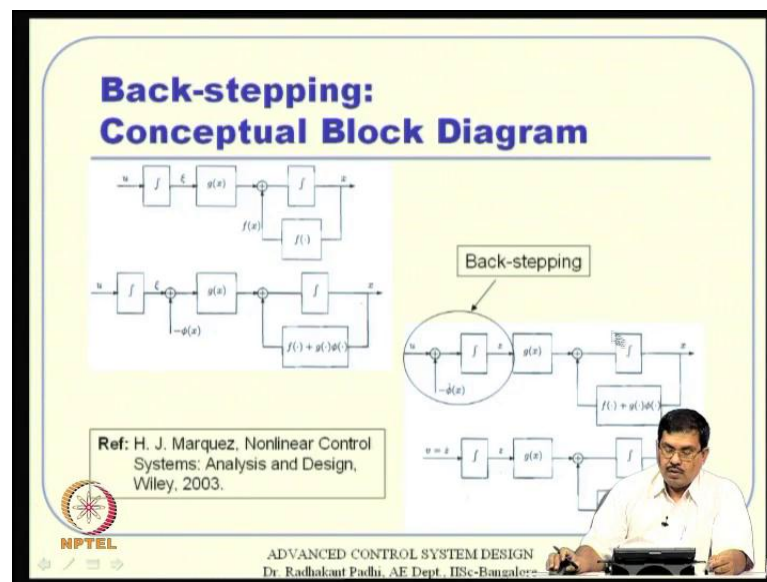
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 14

So, let us analyse this **this** z actually, z is by definition the remains as phi of X. So, we put it z dot is xi dot minus phi dot. So, if xi dot is nothing but u, so the z dot is nothing but, u minus phi dot actually. So, we have this system dynamics like this modified system dynamics in this form, where z dot is nothing but, v; v is this artificial control variable that I

am interpreting that,  $\dot{\phi}$  I am defining as  $v$ . And interpreting that  $\dot{z}$  is nothing but,  $v$  actually.

So, if you see this system dynamics, now it appears in the similar form that we started with actually. So, this **this** form is nothing but, something plus  $g$  of  $X$  times  $z$  and then the next one is  $\dot{z}$  is  $v$ . So, this system is equivalent to the original system actually. So, only thing and only problem is instead of  $I$  mean is  $\phi$  is use in the form of  $\dot{\phi}$  actually. So,  $\phi$  dot can be computable and that means  $\frac{\partial \phi}{\partial X}$  into and  $\dot{X}$  is available any way. So, that is **that is** the way, you compute  $\dot{\phi}$ .

(Refer Slide Time: 20:22)



So, what is going on in a block diagram sense, this is original system dynamics, what we started with  $u$  and then integrated goes to; see, if you see this  $u$ , if integrated **zeta that is a xi** (Refer Slide Time: 20:34). So, that is what, it happens here, if  $u$  integrate will get  $\xi$  then, it multiplied by  $g$  of  $(\xi)$  I will get  $g$  of times  $\xi$  and then, this feedback operates that way actually. So, what you see here is a  $f$  of  $X$  plus  $g$  of  $X$  times  $\xi$ . So, that is **that is**  $\dot{X}$ .

So, that how it happens, but what are doing here is, first of all we are putting a  $g$  times  $\phi$  here in this loop; and for that **for that** reason, you have to introduce negative **phi of X**  $\phi$  of  $X$  here, but we do not stop here, **this phi of** this  $\phi$  of  $X$  really not introduced here, it is

introduced **once** one block before that; and because of that, we have to introduce  $\dot{\phi}$  instead negative of  $\dot{\phi}$ . And instead of  $\phi$  of  $X$ , it introduces negative  $\dot{\phi}$  of  $X$  actually. So,  $\phi$  to  $\dot{\phi}$  is actually  $(( ))$  actually.

So, whatever is integrated that, that signal flows forward; whatever is differentiated, the signal flows backward. That is why it is called back-stepping actually, we are just stepping back in the block diagram one time and then, interpret I mean this **this** interpreting that  $u$  minus  $\dot{\phi}$  sort of thing, **because of** because this algebra basically. This entire thing is borrowed from **from** this book (Refer Slide Time: 21:49), and if anybody interested you can they can see this book also, this is a good book I think **alright**.

So, this integrator back-stepping, now we have to I mean see that, how do you design this  $V$  of  $X$  and thing like that. Now, we are talking about this system dynamics  $(( ))$ . So, how do we do that? So, let us start with this  $V$  of  $X$ , now we have to define a Lyapunov function inclusive of  $z$ .

So, will define something like  $V_1$  of  $X$  plus half  $z$  square sort of thing. So,  $\dot{V}$  is nothing but,  $\frac{d}{dt} V_1$  by  $\frac{d}{dt} X$  times  $\dot{X}$ , and  $\dot{X}$  is all that; because  $\dot{X}$  is, is what it what we derived actually. So, the entire expression will put it back, once you put the entire expression this plus this  $z$  time's  $\dot{z}$ . So, this **this** term will give us  $z$  times  $\dot{z}$ , and  $\dot{z}$  is nothing but  $v$ . So, this  $\dot{z}$  is  $v$  that is what we will put here actually. So, that is how we will end up here.

So, but this part of the system I mean this part of the algebra is nothing but, negative of  $V$  of  $X$ ; that is what it is all are assuming that is already **already** designed that way. So, this is available to us actually **right** by the **by the** way we started with, we will start **ok** that this  $\xi$  is already designed with associated Lyapunov function we satisfy this **this** inequality. So,  $(( ))$  is available to us. So, we use that **ok**.



(Refer Slide Time: 23:17)

### Integrator Back-stepping

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Step-2: Let  $V(X, z) = V_1(X) + \frac{1}{2}z^2$

Then  $\dot{V} = \left(\frac{\partial V_1}{\partial X}\right)^T \underbrace{[f(X) + g(X)\varphi(X) + g(X)z]}_{\leq -V_a(X)} + zv$

$$\leq -V_a(X) + \left[\left(\frac{\partial V_1}{\partial X}\right)^T g(X) + v\right]z$$

Let  $v = -\left(\frac{\partial V_1}{\partial X}\right)^T g(X) - kz, \quad k > 0$

Then  $\dot{V} \leq \underbrace{-V_a(X)}_{\text{ndf}} - \underbrace{kz^2}_{\text{ndf}} < 0 \quad (\text{ndf})$



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16

So, this nothing but, less than equal to V a of X. So, we keep this part is less than equal to V a of X. Now, if you see this part this one and that one to get that sort of thing and that is **that is** what we will combine actually. So, then once you combine this two part, this **this** first part and this **this** X this term and then, you have z time's v actually.

So, when we combine this two term will **will** end up with this negative V a of X here, and that is already available to us anyway plus this additional term actually. Remember, z is common to both actually, so I can **I can** take out z actually. So, that is what happens here. Now, the question here is how do you measure, how do you design v such that, this entire thing is negative definite that **that** is the one point actually.

So, when you see something like this, the very natural the idea that comes to mind is let me design v this way. So, I will cancel out this term and whatever is left out, it will generate something like a negative k time's z square, where k is positive. So, naturally I will selective v, which negative of this quantity minus k z; so that, when minus k z is left out here, it will generate a minus k z square term actually.

So, that is the whole idea. So, now V dot turns out to be less than equal to a negative definite function that it is already available minus k z square **which is** which is also negative kind of

semi definite and all that actually. Because, if you **if you** see the total things, so if you see the total things like total system dynamic the entirely Lyapunov function must contain both X as well as z actually **right**, then only the system dynamics we can conclude something actually; if any part is left out will have a negative semi definite sort of idea there.

So, when you see this **this** entire function, the first part assures that, it is negative definite for the first part of the system dynamic. In the second part, will assures that, it is also negative kind of semi definite for the second part; **combine the (( ))** together sort of thing, they will have a negative definite function for the **for the (( ))** total system actually. So, that is the way it will have a negative definiteness actually.

So, whole idea what is that actually? Now, the whole idea is v turns out two like this, and v is an also known to us already; v by definition is u minus phi dot, phi dot is anywhere available. So, using all that, I will be able to extract u basically **ok**.

(Refer Slide Time: 26:00)

**Integrator Back-stepping**

Control Solution:

$$v = u - \dot{\varphi} = -\left(\frac{\partial V_1}{\partial X}\right)^T g(X) - k z$$

$$u = \dot{\varphi} - \left(\frac{\partial V_1}{\partial X}\right)^T g(X) - k [\xi - \varphi(X)]$$

where,  $\dot{\varphi} = \left(\frac{\partial \varphi}{\partial X}\right)^T [f(X) + g(X)\xi], k > 0$

[Note: In the design, there is a need to design  $\varphi$ ]

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So, v is already u minus phi dot. So, and phi dot mean that expression is available to us any way, because v is already, v is designed like that. So, that is equal to that and phi dot is **(( ))** there. So, u equal to phi dot minus there and phi dot is like this already there actually. So, that is how we **we** design the control u basically.

So, but also note that, in this entire exercise first one should, first design this  $\phi$  of  $X$ , because without that, it will not proceed further, but that is anyway there actually. For this method to start, the  $\phi$  of  $X$  should be design actually first. What you are assuming here that, there exist a feedback law for  $x_1$  equal to  $\phi$  of  $X$  with  $\phi(0) = 0$ . So, that is to be design first. Then we design this  $u$  and all that. So, let us see a simple example again, like  $\dot{x}_1$  is the same example probably what you go back, instead of  $u$  we will put  $x_2$ ; and then  $\dot{x}_2$  equal to  $u$ , that is how we will make it as a system. So, that it is compatible with the theory that we discussed. So, ultimate objective here is  $u$  has to be designed. So, that over all system becomes asymptotically stable.

Now, we have already designed  $x_2$  before and let us repeat the exercise one more time. So, you will consider a  $x_2$  control variable for the first equation and then, we will I mean either you and put this entire like identify which one is what and just into the formula get the answer; or you can stop from the beginning and get the answer like that actually.

So, you have this  $V_1$  of  $X$  is like that. First of all, you have to find the  $\phi$ , for finding that we will take  $V_1$  as half  $x_1$  square. Then  $\dot{V}_1$  is like that, and this will be less than equal to some  $V_a$  of  $x_1$ . And that previous example that, we started with the same example we will take  $x_1$  square plus  $x_1^4$  th, which will not cancel out the good non-linearity part of it; we will keep it that way.

(Refer Slide Time: 28:02)

### Integrator Back-stepping: An Example

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$$\begin{aligned} & ax_1^3 - \dot{y}_1^d + x_1 x_2 \leq -x_1^2 - \dot{y}_1^d \\ & x_1 (ax_1^2 + x_2) \leq -x_1^2 \end{aligned}$$

Let  $ax_1^2 + x_2 = -x_1$


$$\Rightarrow x_2 = (-ax_1^2 - x_1) \triangleq \varphi(x_1)$$

Modified system:  $\dot{x}_1 = ax_1^2 - x_1^3 + \varphi(x_1) + \overbrace{[x_2 - \varphi(x_1)]}^z$

$$\dot{z} = v \triangleq (\dot{y}_2^d - \dot{\varphi}(x_1))$$

Let  $V(x_1, z) = V_1(x_1) + \frac{1}{2}z^2$

$$\dot{V} = \dot{V}_1 + z v = \left( \frac{\partial V_1}{\partial x_1} \right) [ax_1^2 - x_1^3 + \varphi(x_1)] + \left( \frac{\partial V_1}{\partial x_1} + v \right) z$$



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19

And hence, we will cancel out all the thing and design this **this** x 2, this is earlier we design it as u, but this time it is x 2 basically. So, this turns out to be phi of x 1. So, that is how we got phi of x 1 basically. Now, will go back and the modified system dynamics we have to write. So, we will add and subtracts and things like that.

So, will **will** write this x 1 dot in this form and where this z dot is v; and v is defined as u minus phi dot. So, that way we will define actually. So, we have to take this V as V 1 of x 1 plus half z square again, that is a following the same theory that we just discussed actually here. So, will put that the same idea back in here, **(( ))** is V 1 of x 1 plus half z square. So, V dot is nothing but, V 1 dot plus z time's v, z time's z dot, z dot is v anyway.

So, that is just what it is. This entire algebra gives us like this. And then will be locate this v has to be I mean this algebra whatever we see here, v has to be minus del V 1 by del x 1 minus k z square. So, that is I mean minus k z basically.

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### Integrator Back-stepping: An Example

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Let  $v = -\left(\frac{\partial V_1}{\partial x_1}\right) - k z, k > 0$


$$u - \dot{\varphi} = -x_1 - k [x_2 - \varphi(x_1)]$$

$$u = \frac{\partial \varphi}{\partial x_1} (ax_1^2 - x_1^3 + x_2) - x_1 - k [x_2 - (-ax_1^2 - x_1)]$$


$$= (-2ax_1 - 1)(ax_1^2 - x_1^3 + x_2) - x_1 - k [x_2 + ax_1^2 + x_1]$$

$$u = -(1 + 2ax_1)(ax_1^2 - x_1^3 + x_2) - x_1 - k(x_1 + x_2 + ax_1^2)$$

where  $k > 0$



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So, that is what it is. So, if you put it back and try to solve for  $(\dot{\varphi})$  control  $v$  is nothing but,  $u$  minus  $\dot{\varphi}$ . So,  $u$  equal to  $\dot{\varphi}$  minus  $x_1$  minus  $k$ , about  $\dot{\varphi}$  is a nothing but,  $\frac{\partial \varphi}{\partial x_1}$  into  $x_1$  dot;  $x_1$  dot is like that minus  $x_1$ , so minus  $x_1$  minus  $k$  times  $(\dot{\varphi})$ , so minus  $k$  times  $(\dot{\varphi})$ ,  $\varphi$  of  $x_1$  is that way anyway.

So, you now you expand all the thing, algebra and then get a control  $(u)$  that form actually. So, this  $k$  becomes gain value, which is positive number which needs to be tune for your good performance basically. That is how **that is that is**  $(u)$  example actually.

(Refer Slide Time: 29:50)

**Integrator Back-stepping:  
An Example**

Note: The composite Lyapunov function is:

$$\begin{aligned} V &= V_1 + \frac{1}{2} z^2 \\ &= \frac{1}{2} x_1^2 + \frac{1}{2} [x_2 - \varphi(x_1)]^2 \\ &= \frac{1}{2} x_1^2 + \frac{1}{2} (x_2 + x_1 + \alpha x_1^2)^2 \end{aligned}$$

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So, what is the associate Lyapunov function for this? The composite Lyapunov function turns out to be  $V_1 + \frac{1}{2} z^2$ . So,  $V_1$  is obviously already there and  $z^2$  is nothing but,  $z$  is by definition  $u - \dot{\varphi}$  sort of thing right, so that that  $(\dot{\varphi})$  sorry. So,  $z$  is nothing but this what is that, that definition of this one extra minus  $\dot{\varphi}$  of  $x_1$  that is that is, so you put  $x_2 - \dot{\varphi}$  of  $x_1$  that is that part of it.

So, this is a composite Lyapunov function for the total system actually. First part is only for the first equation; when you put the second one, it becomes Lyapunov function for that total system actually. Now, more general case this is all about like, we have this  $\dot{x} = Ax + Bu$  type of system dynamics to be started with.

This is the foundation is to anywhere, so we started with where  $X$  is  $n$  dimensional state, and one more state is the  $\dot{x}$  that is equal to  $u$ . So, that is how we start with. What about more general case actually. So, when you take more general case and all, so this all happens to be not that  $(\dot{x})$   $(\dot{x})$ .

(Refer Slide Time: 31:05)

**Integrator Back-stepping:  
More General Case**


System Dynamics:

$$\dot{X} = f(X) + g(X)\xi_1$$
$$\dot{\xi}_1 = \xi_2$$
$$\dot{\xi}_2 = u$$

Idea : Successive iteration.

[Note: The procedure for  $n^{\text{th}}$  order system is entire]

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Let us, consider this one as a natural extension actually. We have  $\xi_1$  here, where  $\dot{\xi}_1$  is  $\xi_2$  and then  $\dot{\xi}_2$  is  $u$ . So, obviously the idea is successive iteration actually; like if you consider only this system first, the first two equations first, once you have done with that, will get  $\xi_2$ . And then you consider this first sub system is one and then you add one more  $\dot{\xi}_2$  is here **ok**.

So, successively **have to** we have to design two times actually. And this it is the system dynamic is analogous that means let say, this is **(( ))** sequence does not stop here; but it is like  $\dot{\xi}_2$  is  $\xi_3$ ,  $\dot{\xi}_3$  is  $\xi_4$ , and  $\dot{\xi}_4$  is  $\xi_5$  like that. And then somewhere let us say  $\dot{\xi}_{10}$  is  $u$  like that. So, you have to repeat this exercise like ten times actually.

(Refer Slide Time: 32:00)

**Integrator Back-stepping:  
More General Case**

Step-1: Consider the subsystem

$$\dot{X} = f(X) + g(X)\xi_1$$
$$\dot{\xi}_1 = \xi_2$$

Assumption:

$\xi_1 = \varphi(X)$  is a stabilizing feedback law for

$$\dot{X} = f(X) + g(X)\xi_1$$

and  $V_1^*(X)$  is the corresponding Lyapunov function.

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So, we concentrate only on this. So, where we talk about this  $\xi_2$  dot is  $u$  and then, let us see what happens actually. So, first will consider only first two equations. For the first equations we have just down everything, this first is like  $\xi_1$  and for the  $\xi_1 = \varphi(X)$  like exists already. And we have to design something like  $\xi_2$  considering that this equation together.

So, we will proceed the exactly same thing that we just discussed and will tell this **this**  $V_1$  like the corresponding Lyapunov function is available, **(( ))** one can be done, the way we just discussed actually. So, then will take by the time by the way that, just I mean, so this **this** part of it, so we just do that. So, **so** the analogous I mean **the then** the inference we can directly write  $\xi_2$  instead of **(( ))** about all the derivation one more time.



(Refer Slide Time: 32:49)

### Integrator Back-stepping: More General Case

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Step-1: Consider the subsystem

$$\dot{X} = f(X) + g(X)\xi_1$$


$$\dot{\xi}_1 = \xi_2$$

Assumption:

$\xi_1 = \varphi(X)$  is a stabilizing feedback law for

$$\dot{X} = f(X) + g(X)\xi_1$$

and  $V_1(X)$  is the corresponding Lyapunov function.



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23

So, let us write  $\xi_2$  and  $\xi_2$  has to be in this form,  $\frac{\partial \varphi}{\partial X}$  into a  $\dot{X}$  dot minus this **this** term minus that term and all that actually. So, that is available and also we have a composite Lyapunov function **for this to** for this system, which is like  $V_1$  plus this one. That also we just discussed. Now, what about extending to one more actually; so, if we want to extend this step, this is about step 1 sort of thing that we just derived.

(Refer Slide Time: 33:16)

### Integrator Back-stepping: More General Case

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Step - 2:



$$\dot{X}_1 \triangleq \begin{bmatrix} \dot{X} \\ \dot{\xi}_1 \end{bmatrix} = \begin{bmatrix} f(X) + g(X)\xi_1 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \xi_2$$

$f_1(X_1)$                        $g_1(X_1)$

$$\xi_2 = u \quad \text{where, } X_1 \triangleq \begin{bmatrix} X \\ \xi_1 \end{bmatrix}$$

$\therefore$  Using the same idea,

$$u = \left( \frac{\partial \varphi_1}{\partial X_1} \right)^T \left[ f_1(X_1) + g_1(X_1)\xi_2 \right] - \left( \frac{\partial V_2}{\partial X_1} \right)^T g_1(X_1) - k_1 [\xi_2 - \varphi_1(X_1)]$$

$$V = V_2 + \frac{1}{2} [\xi_2 - \varphi_1(X_1)]^2 = V_1 + \frac{1}{2} [\xi_1 - \varphi(X)]^2 + \frac{1}{2} [\xi_2 - \varphi_1(X_1)]^2$$



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Now, where step 2 we have to consider this **this this** one more **(( ))** into the picture basically; so, will tell this **this** type is first **first** it is like that, first subsystem will like this. And then we are an adding one more  $\dot{x}_2$  equal to  $u$ . So, you consider this part of it something like  $f_1$  of  $X_1$ , where  $X_1$  is  $X$  and **zeta 1 I mean**  $x_1$  together. And then tell this a  $x_2$  term here, so I will put **(( ))**. So,  $\dot{X}_1$  dot is this expression, so  $f_1$  of  $X_1$  plus  $g_1$  of  $X_1$  time's  $x_2$ . So,  $X_1$  by definition like that.

So, this expression what is **what is** here the first part of it, I will just change it the definition is  $X_1$  instead of  $X$ . So, it is  $\dot{X}_1$  dot is whatever that is in the first equation, then  $\dot{x}_2$  dot **(( ))**. Then again we know what **how to do** how to do it. So, will do this algebra again and then tell  $u$  now becomes like that actually.

So, entire **(( ))** expression what we have operated here, instead of  $X$  we will have to operate it based on **(( ))** dynamics actually. And **V 2**  $V$  is to be  $V_2$  plus  $x_2$  minus  $\phi_1$  of  $X_1$ . So, that **that** is to be carefully noted actually and this  $\phi_1$  happens to be all that by the way **this enter thing** this entire thing is  $\phi_1$ .

So, **(( ))** algebra is a necessity in this approach anyway. So, **(( ))** have to **(( ))** should not get I mean impression with algebra and all that. What essentially its **its** lot more **(( ))** keeping rather than too much difficulty actually. If you once you understand one or two steps, then is just extension of that same idea basically.

So, we have this and then, put it back here and then tell using the same idea will get a  $u$ . And the composite Lyapunov function for the entire system that means this system together  $\dot{X}$  dot  $x_1$  dot and  $\dot{x}_2$  dot **(( ))** to be like that. And as I told you before this **this this** is actually not very unrealistic, because if you see this  $x_1$  has control **(( ))** to the original plan; but this second this will like a second order actual dynamics.

First order actual dynamics is what we **(( ))** I mean we just discussed in this first part of the thing, first order actual dynamics that will happen that way. If you have a second order actual dynamics that will I mean the two equations that will happen that way actually.

So, this is this will be augmented to the system dynamic. We want to design robust a etcetera input and all that. So, then this is procedure, one of the procedure that is available to

you is back-stepping actually. So, will go that and then, this is about that. And then we talk about what is best the generalization that you can have this **this** approach actually? The best generalization turns out to be in this strict feedback system and all those thing that we discuss are subsets of that anyway.

(Refer Slide Time: 36:09)

**Integrator Back-stepping for Strict Feedback Systems**

System Dynamics

$$\begin{aligned}\dot{X} &= f(X) + g(X)\xi_1 \\ \dot{\xi}_1 &= f_1(X, \xi_1) + g_1(X, \xi_1)\xi_2 \\ \dot{\xi}_2 &= f_2(X, \xi_1, \xi_2) + g_2(X, \xi_1, \xi_2)\xi_3 \\ &\vdots \\ \dot{\xi}_k &= f_k(X, \xi_1, \dots, \xi_k) + g_k(X, \xi_1, \dots, \xi_k)u\end{aligned}$$

Strong Assumption:

$$g_1(X, \xi_1), g_2(X, \xi_1, \xi_2), \dots, g_k(X, \xi_1, \dots, \xi_k)$$

over the domain of interest  $\forall t$

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So, strict feedback system is something like this, we have  $\dot{X}$  is like that, **zeta 1** **xi 1** dot is like this, where  $\xi_2$  is an input;  $\dot{\xi}_2$  is like this, so  $\xi_3$  is input like that it will continue to some arbitrarily or arbitrary order  $k$  basically. So, if it happens like that and there is a very strong assumption here by the way. What it tells you is? All this function that, you looking at not the first one, starting from  $g_1$   $g_2$  up to  $g_k$ , all this functions are certainly not equal to 0, over the entire domain of interest for all time. That is actually very strong assumption, but with that assumption, we should be able to solve it is actually.

So, what is the first the whole idea here, I mean we will not worry so much about this **this** functional dependence and all. Let us consider only this first I mean first two terms sort of thing.

(Refer Slide Time: 37:12)

**Integrator Back-stepping for Strict Feedback Systems**

Special Case:  $\dot{X} = f(X) + g(X)\xi$   
 $\dot{\xi} = f_a(X, \xi) + g_a(X, \xi)u$

Solution:  
Define  $\dot{\xi} = v$  and carryout the design for  $v$  as before.

Finally  $f_a(X, \xi) + g_a(X, \xi)u = v$

i.e.  $u = \frac{1}{g_a(X, \xi)} [v - f_a(X, \xi)]$

Note: By assumption,  $g_a(X, \xi) \neq 0 \forall t$

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Then this, whatever is **whatever is** appearing here  $1 + g_1 \xi_2$ , I will simply define it is some sort something like a new variable sort of thing. So, let us consider only that part of it. So,  $\dot{X} = f + g \xi$ , where  $\dot{\xi} = f_a + g_a u$ , so that way. And what you are defining is, this  $\dot{\xi} = v$  and you carryout all the algebra, because **(())**  $v$  know how to do it. And ultimately once you have done with  $v$ , you can abstract  $u$  from that actually, this is by definition  $v$ . So, this is equal to  $v$ .

So, then if I solve it for  $u$  this simply algebraic equation anyway. So, I will simply **(())** and solve for  $u$  basically, once I solve for  $u$  this is this expression that I will end up get actually. And I can do that, because by assumptions  $g_a$  is not equal to 0 anyway. So, that is **that is** anyway there actually.

So, with that I think will I mean without this **this** topic **(())** sufficient **(())** anybody to work with this **this** back-stepping idea and all that. So, you can see, one of the idea's that we use for I mean this analysis to **(())** no theory, before you have seen how it is useful for **for (())** adaptive design. Now, this class we will see, how it is useful in back-stepping design directly actually. And ideas, various ideas **(()) (())** in the literature, where you can think of let say use that in **in** observer setting also like how do you design observer based on Lyapunov theory.

So, it is very generic tool, where you can think of exploiting that for **for** design purpose as well actually. So, with that exposure I think I will proceed to a different topic now. And then, we will rest of the time we will talk about that actually **alright**.

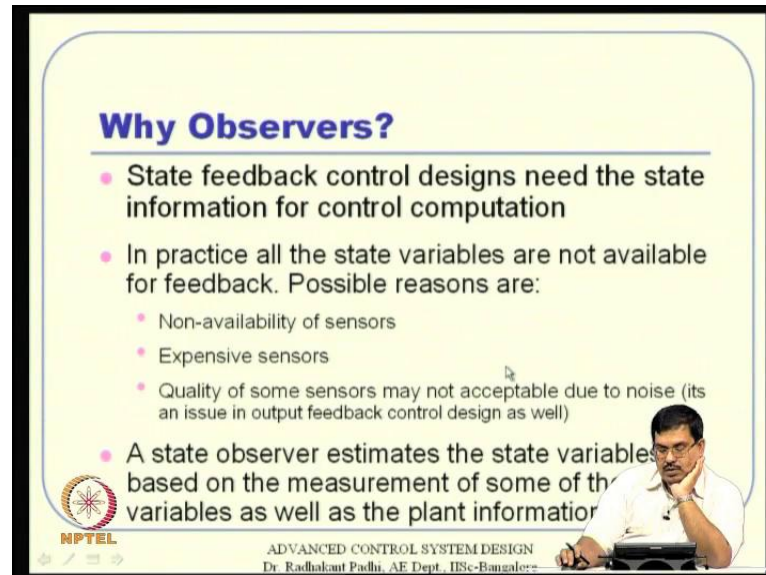
So, this **this** topic is linear quadratic observer (Refer Slide Time: 39:03). So, this is what will see before in that I mean sometime back is this **(( ))** type of observer, this is **is** valid for single input system and all. The moment it was multiple input and all, there is lot ambiguity confusion and all that, how do you do that. There are suggestion and all that, but then it is not very unique way of doing things.

So, this **this** particular observer design is it does not is not restricted to that. In other words, you can have multiple input system for the control design; and hence, for the **(( ))** system we have multiple output also. So, the **(( ))** placement type of observer is valid for only singular output system, whereas this L Q observer is valid for multiple output system directly basically.

We can have a number of measurements many basically. That is the advantage that you talk about LQ observer. Second this bigger advantage is this gives us a platform to develop towards **(( ))** filter which is even more elegant actually. Having said that, you can also note that this L Q observer is actually nothing but, a **(( ))** filter. So, a special **(( ))** filter sort of thing you can think about.

And then hence, even if you have this noise input in the system, then also it **it** is take a it is take a **(( ))** filtering it out actually. So, we will see that little bit **(( ))** of that, because I thought without this **(( ))** of L Q observer and little bit of **(( ))** filter at least, now control theory course is complete actually. Thus, most of the times where we have to use some problem of observer or filter like that actually.

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### Why Observers?

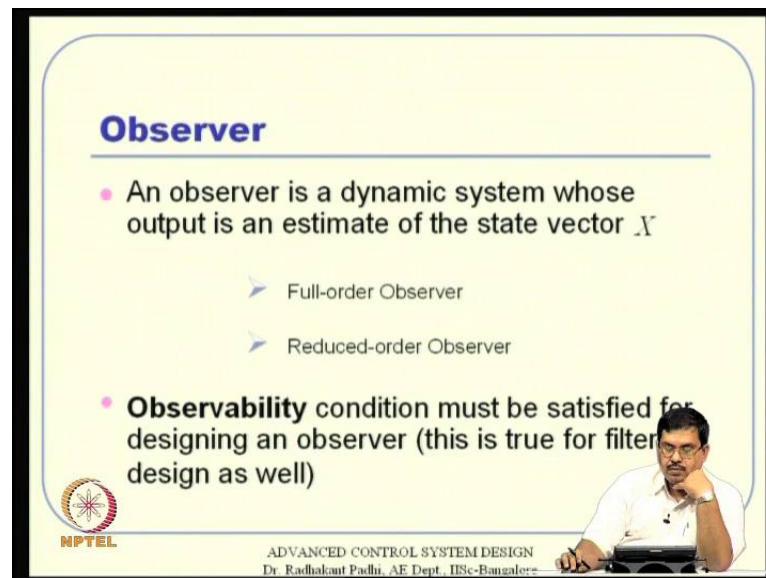
- State feedback control designs need the state information for control computation
- In practice all the state variables are not available for feedback. Possible reasons are:
  - Non-availability of sensors
  - Expensive sensors
  - Quality of some sensors may not be acceptable due to noise (its an issue in output feedback control design as well)
- A state observer estimates the state variables based on the measurement of some of the variables as well as the plant information

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So, let us see what is going on here. So, why observers, we have seen this before that, the state feedback control designs need the state information for control computation. And in practice, all states may not be available and possible reasons can include let us say: sensors are not available, sensors can be very expensive, sensor and quality of the sensors may not be acceptable due to the noise content in that also. So, you probably if given a choice, we will not want to use that **that** sensor actually.

So, what do you what is the alternative? Let us say, we use limited a sensor which are of good quality anyway. And then, rest of the states we want to kind of have an estimate of that, based on those measurements in a sequential manner actually. **(( ))** will take measurements multiple time and from them from that information, we want to observe or we want to estimate what **what** should be my state and think like that actually.

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**Observer**

- An observer is a dynamic system whose output is an estimate of the state vector  $\hat{X}$ 
  - Full-order Observer
  - Reduced-order Observer
- **Observability** condition must be satisfied for designing an observer (this is true for filter design as well)

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Image of a man in a white shirt sitting at a desk, likely the presenter.

So, what is an observer? An observer is nothing but, dynamical system whose output I mean output of the observer is an estimate of the state vector  $X$  actually. So, that is what you are primarily **( )** estimate of the state vector  $X$ . Obviously, observer can be full order **( )** sort of thing like that, **( )** topics further discussion thing like that; we will not talk about that, we will simply confine our full order observer you can **( )** actually.

Now, also remember that before talking an observer, the observability condition is a must actually and this also true for filter design as well, is the system is not having observability property, then we cannot design an **( )** ok. So, that means we easily need extra additional sensors, some information that you cannot capture using limited sensor and all that actually **alright**. So, observability condition must be there and we are interested in full order observer and we are a interested in linear quadratic observer that is the objective here actually.

(Refer Slide Time: 42:37)

**Observer Design for Linear Systems**

Plant :  $\dot{X} = AX + BU$   
 $Y = CY$  (sensor output vector)

Let the observed state be  $\hat{X}$  and the Observer dynamics be

$$\dot{\hat{X}} = \hat{A}\hat{X} + \hat{B}U + K_e Y$$

Error :  $\tilde{X} \triangleq (X - \hat{X})$

The slide also features a block diagram of a control system with an observer. The plant block contains blocks for input  $U$ , gain  $B$ , integrator  $I$ , gain  $A$ , and output  $Y$ . The observer block contains blocks for gain  $\hat{B}$ , gain  $\hat{A}$ , gain  $K_e$ , and integrator  $I$ . The error signal  $Y$  is fed back into the observer through the  $K_e$  block. The output of the observer is  $\hat{X}$ . The slide includes the NPTEL logo and the text 'ADVANCED CONTROL SYSTEM DESIGN Dr. Radhakant Padhi, AE Dept., IISc-Bangalore'.

So, let us see what is what we are interested in here. So, let us plant is  $\dot{X}$  all I am talking about linear system again actually. So, it  $\dot{X}$  is  $AX + BU$  and  $Y$  equal to  $CX$ , so this is nothing but, the sensor output vector. Sensor, whatever sensors you are getting that, you are writing as a linear equation,  $Y$  equal to  $CX$ .

And the let the observed state be  $\hat{X}$ ; and the observer dynamics that is what you have to we want to have an estimate; so, that is that let denote that is  $\hat{X}$  and  $\dot{\hat{X}}$  is nothing but, that actually; that is almost same thing as that  $\hat{A}\hat{X} + \hat{B}U + K_e Y$ , but this plus  $K_e Y$  is an additional term that you are interested to put in this. So, that is how will inject sensor information into the dynamics actually.

So, what is our objective,  $\hat{X}$  should go to  $X$  as soon as possible. So, when I define this error  $\tilde{X}$  as  $X - \hat{X}$ , that means  $\tilde{X}$  should go to 0 basically that is thing. And remember, when you are talking about observer, we are not talking about any noise in the system; neither process noise is there in the system dynamics nor sensor noise is there. So, in that setting talking that, only we are telling that all states I mean not available from the sensors from that we will try to estimate something actually.



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**Observer Design for Linear Systems**

Error Dynamics:  $\dot{\tilde{X}} = \dot{X} - \dot{\hat{X}}$   
$$= (AX + BU) - (\hat{A}\hat{X} + \hat{B}U + K_e Y)$$

Add and Subtract  $\hat{A}\tilde{X}$  and substitute  $Y = CX$

$$\begin{aligned}\dot{\tilde{X}} &= AX - \hat{A}\tilde{X} + \hat{A}\tilde{X} - \hat{A}\hat{X} + BU - \hat{B}U - K_e C X \\ &= (A - \hat{A})\tilde{X} + \hat{A}(\tilde{X} - \hat{X}) + (B - \hat{B})U - K_e C X \\ &= \hat{A}\tilde{X} + (A - \hat{A} - K_e C)\tilde{X} + (B - \hat{B})U\end{aligned}$$

Goals: 1. Make the error dynamics independent of  $X$   
( $\because X$  may be large, even though  $\tilde{X}$  may be small)  
2. Eliminate the effect of  $U$  from error dynamics

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So, when you define error like that, so obviously the error dynamics is also associated with that. So,  $\dot{\tilde{X}}$  is  $\dot{X}$  minus  $\dot{\hat{X}}$ ; the  $\dot{X}$  is  $AX + BU$ ,  $\dot{\hat{X}}$  is that, I just put it that. And then, do this simplified algebra, you can do this add and abstract this  $\tilde{X}$  and **and** thing like that, it will end up with something like this.

Now, we have some thing whenever we have something like this obviously, we do not want to see I mean given a choice, if it is possible we do not want to see this **this** error dynamic is a function of original **(())** original control. So, you want to see the error dynamics as a function of error itself primarily.

So, if you **if you** can do that that is the **(())** actually and because, **because** this coefficient are available, probably we can do that actually. Because, we are now selected what **(())**, so far we have not told, what is  $\hat{A}$  and what is  $\hat{B}$ . So, this will actually give us platform to actually tell what is  $\hat{A}$ , what  $\hat{B}$ , because will **will** make sure that, the coefficient go to 0 that we will get  $B = \hat{B}$  and  $A = \hat{A} - K_e C$ ; but as a by product of that as a good by product in fact, the objective of what we wanted, that means the error dynamics is a function of error itself is happening actually.

So, it is now decouple from **from**  $X$  and  $U$ , because  $X$  can be large and  $\tilde{X}$  can be small; similarly,  $U$  can be large,  $\tilde{X}$  can be small there will be lot of numerical **(( ))** issues and all that **(( ))** actually. So, why **(( ))** that, so what you are telling, this coefficient have to be 0. So, the once we have this coefficient 0, this results is  $\hat{A}$  is nothing but,  $A - K e C$  that is what it is, and  $\hat{B}$  is nothing but  $B$ . So, once you have this, then you go back to **this system dynamics** this observer dynamics and tell now,  $\hat{A}$  is nothing but,  $A - K e C$  and  $\hat{B}$  is  $B$ . So, let me put it back and then once I put it back, I get something like this (Refer Slide Time: 45:52), **right**.

So,  $\dot{X}$  **(( ))** dot is  $A \hat{X} + B U + K e (Y - C \hat{X})$ , and this  $Y$  is your actual like sensor output, and  $C \hat{X}$  is estimated sensor output; let me  $Y - C \hat{X}$  is a also called innovation residual and thing like that actually. This is  $Y - C \hat{X}$  is that **that** part of it is **is** called typically it is called innovation actually in the **(( ))** setup. That is **that is** the extra error information that you are giving to the filter dynamics or the observer dynamics to get it gets some better estimate of the state basically **right**.

So, **what is what is your** what is our interest here. Now, if you go back to the error dynamics part of it, **our observe** our objective was this should go to 0 **right** that is a primary objective, this go to 0 as soon as possible. That means **y** if I see this, this residual error dynamics then that error dynamic should be asymptotically stable actually.

(Refer Slide Time: 46:54)

**Comparison of Control and Observer Design Philosophies**

Control Design	Observer Design
<ul style="list-style-type: none"><li>CL Dynamics</li></ul> $\dot{X} = (A - BK)X$	<ul style="list-style-type: none"><li>CL Error Dynamics</li></ul> $\dot{\tilde{X}} = \hat{A}\tilde{X} = (A - K_e C)\tilde{X}$
<ul style="list-style-type: none"><li>Objective</li></ul> $X(t) \rightarrow 0, \text{ as } t \rightarrow \infty$	<ul style="list-style-type: none"><li>Objective</li></ul> $\tilde{X}(t) \rightarrow 0, \text{ as } t \rightarrow \infty$
	<ul style="list-style-type: none"><li>Notice that</li></ul> $\lambda(A - K_e C) = \lambda[(A - K_e C)^T] = \lambda(A^T - C^T K_e^T)$

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So, that is what I will do here. And tell what is my residual error dynamic, this  $\tilde{X}$  dot is now,  $\hat{A}\tilde{X}$  that **that** is only this part is left out. And  $\hat{A}$  is nothing but,  $A - K_e C$ . So, what I am left out with,  $A - K_e C$  actually. So, that is my error dynamics.

Now, let us go back and see, what is what we have done in the L Q control design that is Linear Quadratic control design using L Q theory and all that. There, if you design a controller in such a way that, the closed loop system dynamics happen to like this, this  $\dot{X}$  equal to  $A - B K$  times  $X$ .

And here, if the closed loop system dynamics, the error dynamics in fact, which is like  $\dot{\tilde{X}}$  equal to  $A - K_e C$  times  $\tilde{X}$ . Here, the objective was to make sure that the  $X$  goes to 0, as  $t$  goes to infinity; here also the same objective  $\tilde{X}$  goes to 0, as  $t$  go to infinity. So, almost very parallel what you have seen there actually, but only the difference is this  $K$  appears to be in the right hand side here; but, where this  $K_e$  appears to be left hand side here actually,  $K_e$  stands for let say estimated gain actually I mean gain of the estimator basically.

So, to avoid this problem **what you** what we note is that, this particular matrix all that we want is this is  $(( ))$  that means Eigen value of this matrix has to be all in the left hand side;

and you see, if I really I am in interested in only in Eigen values, then I can very well visualize that transpose of this matrix as well.

Now, if I visualize a transpose of this matrix this matrix is nothing but, A transpose minus this transpose will now change this order, so it will have C transpose K e transpose. So, **what is what you** what appears what happens I mean what appears in the left hand side now appear in the right hand side; and hence, the problem is **(( ))**, provided we interpreted this A as A transpose here, and this B happens to be C transpose. So, A is equivalent to A transpose, B is equivalent to C transpose, then K e transpose is something that is equivalent to our kind of controller gain actually.

So, is any way that is compatible with what we call is to **(( ))** system and all. We have all discussed about this dual system dynamic when we are discussing about controllability observability and observer and all that actually there. Though if you are **(( ))** you can revise those lectures to see **(( ))** those actually. So, this is the observations. So, **in a** in control design, we have come up with something like close loop system dynamics like this, objective was like that.

Observer design that we are talking here is the close loop system dynamics is like this, objective is also like that. To make sure that, the gain appears in the right hand side, visualize the transpose problem and the transpose problem happens to be like that actually.

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### Algebraic Riccati Equation (ARE) Based Observer Design

System	Dual System
$\dot{X} = AX + BU$ $Y = CX$	$\dot{Z} = A^T Z + C^T V$ $n = B^T Z$
$M = [B   AB   \dots   A^{n-1}B]$	$M = [C^T   A^T C^T   \dots   A^{n-1} C^T]$
$N = [C^T   A^T C^T   \dots   A^{n-1} C^T]$	$N = [B   AB   \dots   A^{n-1}B]$
<p style="text-align: center;"><b>LQR Design</b></p> $= -KX$	

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36

So, now we overcome see something like a like this dual system idea that is talking about. So, (( )) as a summary something like this, system is original system is like this, the dual system that we visualize is some thing like that. Now, if you see the control ability matrix and observability matrix here and similar thing here, then the control ability matrix (( )) to observe abilities here and and vice versa, observability matrix here turns out to be controllability matrix ok.

So, (( )) of designing like another observer something what it what you really do is, we design a (( )) for the dual system actually that that will be become an observer for the actual system.

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**ARE Based Observer Design**

<p><b>CL system (control design)</b></p> $\dot{X} = (A - BK)X$ $X \rightarrow 0 \text{ as } t \rightarrow \infty$ $K = R^{-1}B^T P, \quad P > 0$ <p>where,</p> $PA + A^T P - PBR^{-1}B^T P + Q = 0$	<p><b>Error Dynamics</b></p> $\dot{\tilde{X}} = (A - K_e C)\tilde{X}$ $(A - K_e C)^T = A^T - C^T K_e^T$ <p><b>Analogous</b></p> $K_e^T = R^{-1}CP$ <p>where,</p> $PA^T + AP - PC^T R^{-1}CP + Q = 0$ <p><b>Observer Dynamics</b></p> $\dot{\hat{X}} = A\hat{X} + BU + K_e(y - C\hat{X})$
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Acts like a controller gain

Anyway, so the L Q R designs we already know how to do it, U equal to minus K X. So, using this philosophy, you will be able to directly derive a gain for the filter I mean for the observer. So, let us go back to that, so this is closed loop system dynamics. And this gain that we are talking here was designed as something like R inverse B transpose P, where P (( )) P is positive definite matrix which comes out as a I mean which is found from the solution of the algebraic (( )) equation. So, this (( )) (( )) like that.

Similarly, the error analogues system you see here, this is like transpose and all, this acts like a controller gain as I told. And this controller gain can be directly written as something like this, remember R inverse, B transpose is equivalent to like B transpose equivalent to C, so we will put C; and this P is P, but the P is solution of observer (( )) equation not the controller (( )) equation ok.

So, you see that equivalent system whatever A transpose, C transpose, B transpose that we have, we can (( )) and then tell ok, this is what what should happen actually. So, this this start this this type of like this equation is called I mean filter regard equation or observer regard equation. So, we get a solution of this system dynamics sorry this regard equation. And then whatever solution you get you put it back that will become your K e transpose it is

it is no more  $K e$ . But, if you take the transpose of that, you get  $K e$  basically, once you get  $K e$  this is your observer dynamics.

So, this observer dynamics can be propagated and as you propagate, it will ensure that,  $\tilde{X}$  goes to 0; and hence,  $\hat{X}$  will go to  $X$  actually, that is how it operate actually. So, this is the algebraic regard equation based observer design. So, it is nothing but, L Q observer design, a linear quadratic theory is coming into picture. And this particular idea that we just discussed can be extended to this Kalman filter design in the linear time invariant system case, so in continues time case actually.

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**Problem Statement**

System Dynamics:  $\dot{X} = AX + BU + GW$      $W(t)$ : Process noise vector  
 Measured Output:  $Y = CX + V$              $V(t)$ : Sensor noise vector

Assumptions:

- (i)  $X(0) \sim (\bar{X}_0, P_0)$ ,  $W(t) \sim (0, Q)$  and  $V(t) \sim (0, R)$   
 are "mutually orthogonal" [ $X(0)$ : initial condition for  $X$ ]
- (ii)  $W(t)$  and  $V(t)$  are uncorrelated white noise
- (iii)  $E[W(t)W^T(t+\tau)] = Q\delta(\tau)$ ,  $Q \geq 0$  (psdf)  
 $E[V(t)V^T(t+\tau)] = R\delta(\tau)$ ,  $R > 0$  (pdf)

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So, very quickly will see some summary sort of thing here, what it tell is system dynamics is something like this, now it is  $A X$  plus  $B U$  plus  $G W$ , and  $Y$  is nothing but,  $C X$  plus  $V$ . And this  $W$  and  $V$  are process I mean  $W$  is process noise,  $V$  is sensor noise, and they are vectors in general and thing like that.

And there are assumptions here, that this first of all, this  $W$  and  $V$  has to be like 0 mean the first is 0, that means 0 mean; and then, they have to be like mutually orthogonal, they have to white noise and thing like that.  $W$  and  $V$  are uncorrelated white noise actually they are not correlated to each other. And they are like white noise definition if you see, they

are I mean this I mean there is something called this (( )) property and all that, they have to be satisfied. Lot of too much tell in this lecture, just remember that they have to be like white noise actually.

And then it also talks about like when we talk about W W transpose and then take (( )) value it will have only Q there; remember this is (( )) translated in the time actually. So, if I take only the same time, I will get some value; if I have any difference in time, it will not they will that will be 0 actually, delta delta definition is like that; so, similarly for V also there actually.


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**Problem Statement**

**Objective:**

To obtain an estimate of the state vector  $\hat{X}(t)$  using the state dynamics as well as a "sequence of measurements" as accurate as possible.

i.e., to make sure that the error  $\tilde{X}(t) \triangleq [X(t) - \hat{X}(t)]$  becomes very small (ideally  $\tilde{X}(t) \rightarrow 0$ ) as  $t \rightarrow \infty$ .

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40

So, all this definition (( )) all this assumption where I mean with all this assumptions, we are still putting there objective that, let us estimate X hat. So, that the error goes to 0 actually as t goes to infinity. Now, can we do that, so the entire derivation I will not do it anything out of that here.



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### Observer/Estimator/Filter Dynamics

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$$\dot{\hat{X}} = A\hat{X} + BU + K_e(Y - \hat{Y})$$

where (i)  $\hat{X} = E(X)$  : Estimate of the state  $X$   
(ii)  $\hat{Y} = E(Y)$  : Estimate of the output  $Y$   
     $= E(CX + V)$   
     $= E(CX) + E(V)$   
     $= CE(X) \quad (\because E(V) = 0)$   
     $= C\hat{X}$   
(iii)  $K_e$  : Estimator/Filter/Kalman Gain

**Problem :** How to design  $K_e$  ?

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Let us, see in the summary sense this **this** is something very parallel to what we have done before, we will still take an estimated dynamics. And here, this  $K_e$  is called Kalman gain actually or estimator gain or filter gain whatever you can talk about, exactly same as what we discussed in the **in the** observer actually. Whatever observer equation is there, it is same as that actually, **(( ))** this is  $\hat{X}$  actually. So, that is exactly same as what you have discussed actually.

Now, you tell  $\hat{X}$  **(( ))** expected (Refer Slide Time: 54:48), now  $\hat{X}$  what we are talking actually, not the directly the same **(( ))** or something. Now, it will have estimate of the state itself what you called as expected value of  $X$ , expected value like **like** an average value for **for** many measurements I mean many cases and all. If you take a lot of these values and all, then take average and think average value, then that is nothing but expected value.

So all the thing that, we are discussing here is in the **estimated value sense sorry** expected value sense that means average value sense basically. Then similarly, the  $\hat{Y}$  will be expected value of  $Y$  and then, when you put  $Y$  is nothing but,  $CX + V$  and then, **(( ))** the expected value is linear operative.

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**Problem Statement**

System Dynamics:  $\dot{X} = AX + BU + GW$   $W(t)$ : Process noise vector  
Measured Output:  $Y = CX + V$   $V(t)$ : Sensor noise vector

Assumptions:

- (i)  $X(0) \sim (\bar{X}_0, P_0)$ ,  $W(t) \sim (0, Q)$  and  $V(t) \sim (0, R)$   
are "mutually orthogonal" [ $X(0)$ : initial condition for  $X$ ]
- (ii)  $W(t)$  and  $V(t)$  are uncorrelated white noise
- (iii)  $E[W(t)W^T(t+\tau)] = Q\delta(\tau)$ ,  $Q \geq 0$  (psdf)  
 $E[V(t)V^T(t+\tau)] = R\delta(\tau)$ ,  $R > 0$  (pdf)

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So, you can separate it out, and then  $C$  will come out, and then this is 0 by definition, the respected value this is 0 mean actually (Refer Slide Time: 55:36), both  $W$  and  $V$  are 0 mean. So, **that will** that will **(( ))** that expected value of **(( ))** is 0. So, we will end up with  $\hat{Y}$  is nothing but,  $C \hat{X}$  actually. So, whatever  $\hat{Y}$  you are talking here nothing but,  $C \hat{X}$  hat.

So, very similar to what you have done before, only difference is this  $\hat{X}$  hat is expected value of straight now, is no more deterministic value.

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**Solution: Summary**

- (i) Initialize  $\hat{X}(0)$
- (ii) Solve for Riccati matrix  $P$  from the Filter ARE:  
$$AP + PA^T - PC^T R^{-1} CP + GQG^T = 0$$
- (iii) Compute Kalman Gain:  
$$K_e = PC^T R^{-1}$$
- (iv) Propagate the Filter dynamics:  
$$\dot{\hat{X}} = A\hat{X} + BU + K_e(Y - C\hat{X})$$
  
where  $Y$  is the measurement vector

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ADVANCED CONTROL SYSTEM DESIGN  
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So, the question here is we know the system I mean the filter dynamics, now how do you design this  $K_e$  and that part, I will not talk anything here, but the summary turns out to be like that. You design  $K_e$  exactly like what you have done before, but this  $P$  that the Riccati matrix will be a solution of that. And if you see this, the only difference that we see here compare to this, this equation is (Refer Slide Time: 56:22), if you see this equation and this equation, the only difference is this part actually.

So, earlier there was no  $G$ , here  $G$  transpose there now it has actually. So, if you assume that, this system dynamics has  $G$  as identity, then that is nothing but, the  $LQ$  observer is nothing but, the Kalman filter with the assumption that  $G$  is identity. So, that is **that is** how it operates.

So, **what is** what is the thing here? So, we have a filter dynamics like this, which we need to propagate. So, we initialize something and start propagating, **but in the** but we need a **(( ))** value here  $K_e$ ,  $K_e$  can be computed that way. But, in this expression we need a  $P$ , so  $P$  can be computed from this equation (Refer Slide Time: 57:05). So, you have to implemented it, then implementations **(( ))** has to be something like this.

You first initialize  $\hat{X}_0$  and **and** solve for this P matrix from this **this**  $(( ))$  equation; once you get  $(( ))$  matrix, you compute the gain filter gain. Once you get the gain, you know the filter dynamics anyway, the filter dynamics  $(( ))$  initial condition is available, so simply propagate this equation  $(( ))$  time actually. And it all make sure that, your error goes to 0 in an expected values sense actually now,  $(( ))$  mean will have to 0 and then, you will get a I mean your noise will get filter out and then  $(( ))$  that actually.

So, this is all happening if the this all happiness in continues time linear term in variant system Kalman filter theory. There  $(( ))$  much more be given that, we talk about discreet time implementation, then continuous discreet time, continues time system propagation, and discreet time measurement implementation  $(( ))$  continues discreet version; then there are extensions to make it operate for the non-linear system that is **that is** external Kalman filter and thing like that actually.

These are all available, but also remember that, without knowing this some of the estimation **estimation** theory, control design, perhaps slightly kind of incomplete actually. So, I will encourage all of you to study further in this field and then get  $(( ))$  with all that actually. So, with that I will stop this **this** lecture, thank you.