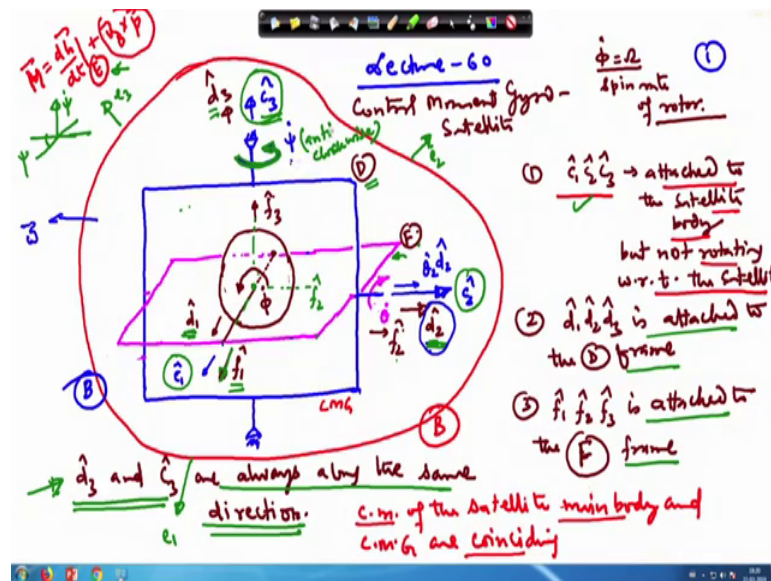


Satellite Attitude Dynamics and Control
Prof. Manoranjan Sinha
Department of Aerospace Engineering
Indian Institute of Technology, Kharagpur

Lecture - 60
Satellite Dynamics with Control Moment Gyro (Contd.)

Welcome to the lecture number 60.

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So, we have been discussing about the Control Moment Gyros. So, I have made a this figure for the control moment gyro in an advance. So, what we can see here that satellite is enclosing this control moment gyros and we are assuming that the center of mass of the satellite, main body and center of mass of the control moment gyro both are coinciding. So, center of mass of the satellite and CMG are coinciding satellite main body satellite main body and CMG are coinciding.

And therefore, the equation then becomes very easy to work with because if you remember that whenever we are differentiating this, so, we have got the term like if we have written M , the equation for the external moment, so that has appeared at $\frac{dh}{dt}$ by $\frac{d}{dt}$ with respect to the E frame and plus $\vec{v} \times \vec{p}$ ok. So, $\vec{v} \times \vec{p}$ plus $\vec{v} \times \vec{p}$, where \vec{p} is the total linear momentum of the whole body.

So, unnecessarily this term we do not have to carry if we assume this ok. So, this will simplify little bit our the whole process of working with this and its always possible that you fix your the other components such that the center of mass and the satellite the rest of the satellites and center of mass both of them coincide. So, this we are terming as B and this is your CMG.

So, here in this figure c_1 c_2 c_3 as it is written in here this is attached to the satellite body, but not rotating with respect to the satellite ok. So, it is a fixed in the satellite and there is also the body axis which I have not shown here and say that body axis if I try to show here so that I can point out along this direction. Let us say that this is this are the 3 directions in which your this is your e_1 direction body, e_2 direction body and e_3 direction of body; the small e_1 , e_2 , e_3 ; capital E always we have used for the inertial plane.

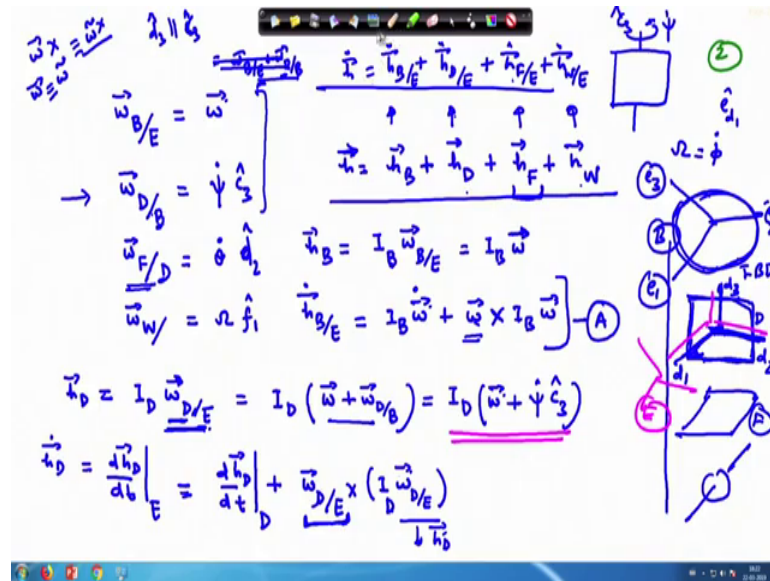
So, in this body then your c_1 c_2 and c_3 they are fixed. So, here is your c_1 , this is c_2 and c_3 . These are the fixed direction, they are not going to change. Thereafter we have chosen a frame which is attached to the frame external frame D ok, which I have shown as d_1 ok, d_2 which is going here; d_1 , d_2 and d_3 . This is rotating along with the frame D. But there is 1 point to note; d_3 and c_3 they are always along the same direction ok. So, this d_3 and c_3 which is written here shown here ok. So, they are always along the same direction because this frame w frame shown by blue which is the D frame it is a rotating about this axis its rotating like this.

So, this rotating in anti clockwise direction; anti clockwise. So, this two are not going to they are always in the same direction. So, this way we have defined d_1 , d_2 , d_3 . So, your d_1 and d_2 will change direction as the angle size changes. If this frame it rotates and comes to this place new place which I have shown your earlier also this is the whole place and this rotates by here this ψ angle. So, this you are showing as $\dot{\psi}$ ok. So, if it comes to this place you will see that this will change its position and this will also change its position with respect to the satellite body ok. Thereafter we have fixed 1 frame to the inner ring this is your inner ring. So, to this the frame we have fixed such that your along this direction you have f_1 ; f_1 is coming here this is your f_1 ok.

So, from this place f_1 is being shown from his place then outward this is your f_2 which is shown here. So, f_2 is here f_2 cap and similarly in the upward direction then your f_3 is

shown. So, this frame is rotating along with the pink frame which is here F frame ok. Now we can start all the things I have written here f_1 f_2 is attached to the frame F; d_1 d_2 d_3 is attached to frame D and c_1 c_2 c_3 attached to the satellite body and its non rotating frame. It will rotate only along with the satellite, but not with respect to the satellite, this frame.

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Next we can start composing our problem. So, we will write as ω angular velocity of the main body which is your B this part ok, angular velocity of the moment body with respect to the inertial frame and this we will write as simply as ω . Then angular velocity of the D frame with respect to the; with respect to the B frame because your this is the frame here and this frame is rotating here $\dot{\psi}$. So, and this direction is c_3 cap. So, only this part will appear here ok.

So, D with respect to B frame ok. Thereafter, the angular velocity of the F frame with respect to the D frame that will be $\dot{\theta}$ times d_2 cap which I have shown here ok; $\dot{\theta}$ here is in this direction. This vector goes here in this direction multiplied by the corresponding unit vector. So, I am not using this notation e_d cap and something like that because again we have to carry so many subscript another thing.

So, this is easier to comprehend here in this place and thereafter the lastly we have the angular velocity of the wheel with respect to the which frame? This is rotating with

respect to the F frame ok, this is attached to the F frame; axle of the wheel it is attached to the F frame ok.

Therefore, this we can write as capital omega. So, capital omega we have written for $\dot{\phi}$ which is a spin rate of the wheel. So, capital omega times f_1 cap. Now f_1 cap will change direction, d_2 cap will change direction with respect to the satellite all of them are changing ok. So, with respect to the satellite f_1 will change and also this changes with respect to the D frame and so on. So, this procedure we have to carry out ok. Now here the total angular momentum it can be written as the summation of the main body frame and the main body and then the outer frame which we are noted as D and then the outer frame we have written as D and then the F frame and then the angular momentum of the wheel ok.

So, this approach that we are taking here this is showing you these are the absolute angular momentum not a relative one. Just as in the previous lecture, we have done that and then we have combined to get a derivation which was in the sense relative sense with respect to the satellite. Here all these are the absolute angular momentum ok. So, we are making free body diagram of each and every one. This is your satellite this is your outer frame then this is your inner frame and to this attached is the wheel.

So, all of them are the free body diagram FBD. So, for all of them we are writing here like this. Now we have to compose each of the term here. So, the first term h_B this will be equal to moment of inertia of the B frame. B frame means it is at the main satellite body which excludes the CMG ok. So, I_B times $\omega_{B/E}$; this is the angular momentum of this and this we are writing as I_B times for convenience this will just write as I_B times omega. Thereafter we need to also. So, your \dot{h} then will be written as \dot{h} equal to \dot{h}_B plus \dot{h}_D and all of them with respect to E frame \dot{h} ok. So, you can see that we have written all of them with respect to means we are considering the free body diagram.

So, therefore, $\dot{h}_{B/E}$ this quantity will be written as I_B times omega. So, there is a frame fixed into this which we are writing as the e_1 e_2 and e_3 this is your body frame attached to the main body this B ok. So, in this body frame the moment of inertia of this main body is not going to change and therefore, we can write it like this; times omega cross I_B times omega. I am not putting here dot just 1 necessarily. This I am

considering that this part will give you a vector and this is multiplied by a vector. So, it is very simple unnecessarily complicating a complicating in terms of the dyadic it will not benefit here in this place.

So, it is a follow this omega cross here omega cross what we have written omega cross this is simply implies this is nothing but omega filled a cross which is a matrix and this omega here this omega this implies that this is nothing but identical to omega tilde equivalent to omega tilde ok. So, this way you equation then gets simplified. So, this is your equation number let us say A. Now we take the next one which is $h D$; $h D$ now this is your D frame. So, D frame to this we have attached one frame which is d_1, d_2 and d_3 and this frame will be rotating with respect to the satellite.

So, in the D frame the moment of inertia because it is a fixed to the outer frame and its rotating along with the outer frame ok. Therefore, moment of inertia of this frame in d_1, d_2, d_3 is not going to change and it makes us easier to write. So, I can write it like $I D$ times omega D cross E. Here see the difference; this is D cross B D this is B. This is with respect to B ok. Here I am writing omega D square E; so this angular velocity of the frame D with respect to frame E which is an inertial frame. So, this can be written as $I D$ then the angular velocity of the main body and this is because it is embedded in this main body. So, we can write this as $\psi \dot{}$. So, or we can write as omega times omega D with respect to the B frame ok.

So, this will be equal to this summation is equal to this part which will write as omega times $\psi \dot{}$ c 3 cap because $\psi \dot{}$ is lining along the c 3 cap direction ok; c 3 cap and $d_3 \text{ cap}$ they are along the same direction all the time c 3 cap and $d_3 \text{ cap}$. And therefore, $d_3 \text{ cap}$ can be replaced by this and it makes easier, some of the steps can be skipped. Now we can write here $h \dot{}$. So, $h D \dot{}$ then it becomes $dh D \text{ by } dt$ with respect to E frame and this we can then expand as $dh D \text{ by } dt$ with respect to the D frame and plus omega D slash E cross remember the first derivation we have done.

Omega this is $I D$ times omega D slash E this is nothing, but your the $h D$ term ok. So, this term is your $h D$. So, this is the way we have written it. You have to particularly take care of the terms while I am writing here this is omega D slash E ok. If we look here in this place this was omega ok. So, this is the difference here which we have to take care of because this is now frame your considering this frame here this particular frame and this

is the you are considering with respect to the E frame each of them you are make as a free body diagram and then you are considering ok. So, in that case this is the way you will write ok. Now, h D is given to be this quantity ok. So, we can expand it in the next step.

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The image shows a handwritten derivation on a whiteboard. At the top left, there is a diagram of a cube with axes labeled $\hat{c}_1, \hat{c}_2, \hat{c}_3$ and a point D . The main derivation starts with the equation:

$$\dot{h}_D = \frac{d}{dt} \left[I_D (\vec{\omega} + \dot{\psi} \hat{c}_3) \right] + \vec{\omega}_{D/E} \times (I_D \vec{\omega}_{D/E})$$

This is then expanded into:

$$\dot{h}_D = {}^D I_D (\dot{\vec{\omega}} + \ddot{\psi} \hat{c}_3 + \dot{\psi} \vec{\omega} \times \hat{c}_3) + \vec{\omega}_{D/E} \times {}^D I_D \vec{\omega}_{D/E}$$

Below this, the derivative is taken with respect to the E frame:

$$\dot{h}_F = \frac{d h_F}{dt} \Big|_E = \frac{d}{dt} \left(I_F \vec{\omega}_{F/E} \right) = I_F \frac{d}{dt} \vec{\omega}_{F/E} + \vec{\omega}_{F/E} \times I_F \vec{\omega}_{F/E}$$

Further expansion shows the derivative of the inertia tensor and the angular velocity vector:

$$\dot{h}_F = I_F \left[\frac{d}{dt} \left(\vec{\omega} + \dot{\psi} \hat{c}_3 + \dot{\theta} \hat{d}_2 \right) \right] + \vec{\omega}_{F/E} \times I_F \vec{\omega}_{F/E}$$

$$\dot{h}_F = I_F \left[\dot{\vec{\omega}} + \ddot{\psi} \hat{c}_3 + \dot{\psi} \vec{\omega} \times \hat{c}_3 + \ddot{\theta} \hat{d}_2 + \dot{\theta} (\vec{\omega} + \dot{\psi} \hat{c}_3) \times \hat{d}_2 \right] + \left[\vec{\omega}_{F/E} \times I_F \vec{\omega}_{F/E} \right]$$

So, we have h dot D dh D by d t. So, this is the quantity h D we have to insert there with respect to the D frame and this is omega plus psi dot times c 3 cap and then I D is also there. So, I D we have to put that the I D is there and this plus omega D E cross I D times omega D slash E ok. Now this part we will expand.

So, in the D frame I D does not change. So, I D will simply come out, omega gets differentiated and this is with respect to. So, your d omega by dt while you are writing here this subscripted D, but this is identically equal to this is what we have done earlier also. This is with respect to basically E frame while we differentiate the angular velocity, so, this goes with the E frame.

So, this way if we write it here in this place. So, I D times omega dot and then plus psi double dot then c 3 cap and then psi dot and this c 3. W what this c 3 how it is going to change; d by dt with respect to the D frame and here is your c 3 cap. So, c 3 cap is a vector which is fixed in the body ok. This is your c 3 cap vector and this body itself this is rotating at the rate omega ok. Therefore, we will write here this is omega times c 3 cap. So, this is the expansion of this term and rest we can copy like this.

So, this is your equation number B and I D is common to all of them. So, I D we can keep it outside here ok. In the next step then we have to take the F frame. So, \dot{h}_F and this we have to do with respect to \dot{h}_F with respect to the E frame ok. So, h_F now we have to pick up; h_F is your this frame, the horizontal one which is the inner frame this is the F frame. So, this will be I_F times the corresponding movement of inertia. So, ω_F this with respect to E; moment of inertia I and then ω_F / E means the velocity angular absolute angular velocity of the frame F with which we are writing with respect to frame E.

Now, this I_F we are writing this is defined in the F frame itself ok. So, F frame we have shown previously this is your F frame. So, along the f_1, f_2 and f_3 vector it will it is defined. So, as this F frame rotates. So, f_1, f_2, f_3 will rotate and therefore, in the F frame the corresponding moment of inertia I_F does not change ok. So, this you have to do with respect to E frame and then we write this as $I_F \frac{d}{dt}$ with respect to the F frame ω_F / E and plus ω_F / E cross ok.

This term we need to expand this is as usual. So, this becomes I_F times now $\frac{d}{dt}$ and remember while I am writing here I D, so, this is defined in the D frame itself this is defined in the F frame itself here this is defined in the F frame itself. Putting so many subscript it makes the things complicated. Understanding the control moment gyros complete function is not impossible or very difficult, but we have to take care of all the subscript and other things and rest we have to write for ω_F / E .

So, ω_F / E will be consisting of ω first ω is the angular velocity of the main body then the D frame is rotating with respect to the main body. So, therefore, for this we have to keep it here and thereafter your F frame is rotating with respect to the D frame ok. So, that is given by $\dot{\theta}$ times \hat{d}_2 and in the corresponding D frame the corresponding unit vector is the $\dot{\theta}$ times \hat{d}_2 cap ok. So, $\dot{\theta}$ times \hat{d}_2 cap ok.

So, what this quantity is this is your $\omega_{\psi} \cdot \psi \cdot v$. We have written as $D \times B \omega_{D/B}$ and then there after F with respect to D. So, this is $\omega_{D/B}$ this is $\omega_{D/B}$ and this part is ω this for the D frame with respect to the B frame or with respect this is ok. This is with respect to the B frame and the lastly we have used the notation $\dot{\theta}_D$, here this is F frame with respect to the D frame.

So, this is the ω_F frame with respect to the D frame. So, this ψ are added to get this ω_F / E . Now we expand this. This quantity will which simply $\omega \cdot$ this quantity will be $\psi \ddot{\psi}$ and then c_3 . As earlier how this is changing that we have to write here. So, that becomes $\psi \ddot{\psi} c_3$ and plus this will change because of the rotation of the D frame, sorry this is fixed in the c_3 frame, sorry what I am stating that this is your D frame and this is along the c_3 cap direction $\psi \dot{\psi}$ is along the c_3 cap direction.

So, this is because of the rotation of the main body. Your this quantities c_3 cap will change as we have done earlier. So, therefore, we write here $\psi \dot{\psi} \times \omega \times c_3$ and then we go to the next term. So, this is $\theta \ddot{\theta} d_2$ cap and how the $\theta \dot{\theta}$ is going to this d_2 vector is going to change. So, $\theta \dot{\theta} \times \theta \dot{\theta} \times$. Now, this $\theta \ddot{\theta} d_2$ cap. This is a vector which is d_2 cap is a vector which is fixed in the this pink frame fixed in the blue frame and it is a pointing here in this direction. So, the question is how we are going to change this part.

So, $\omega \times c_3$ cap and then $\theta \ddot{\theta}$ is coming here; ω_F we are taking here ok. Next part we have to write here the proper cross d_2 cap and then there bracket will be closed and thereafter this part $\omega_F / E \times I$ this $F F \omega_F / E$. So, this part we are keeping as it is and the other part we are expanding ok. So, the question is how your d_2 vector is changing. So, d_2 vector will change and already the ψ vector we have taken care of. ψ vector is changing because of the ω only and d_2 will vector will change because of ω and plus ψ because d_2 is here in this place. So, this body is rotating at ω and also together with this frame is rotating at the $\psi \dot{\psi}$ to which your d_2 vector is attached ok; d_2 the D frame and D frame is rotating at $\psi \dot{\psi}$.

So, we have to take care of these 2 factors. So, this is $\omega + \psi \dot{\psi} \times c_3$ cap. This is the angular velocity of the frame, the outer frame ok. So, the outer frame angular velocity. So, this part is nothing but your here this part is ending this part is nothing but your ω frame D with respect to frame E. Here this is not a cross product. Here just we have written it like this. This is $\theta \dot{\theta} \times \omega$. ω is the main body angular rate and D frame is rotating, so that we are adding. So, D / E this becomes. So, $\omega \cdot D / E$ perhaps we have used for some other notation; D / B we have written here. What D / E we have written ok?

So, if you add these two so your omega B slash E plus omega D slash B that gives you the total omega D with respect to the E frame; omega of D with respect to the E frame. So, this part I am not writing here this is obvious and we can expand it and write it. So, this constitutes your angular the equation for the fl the frame F and thereafter we have to write the equation for the will. So, you considered how much complication is arising. If you take the exact equation for the CMG; Control Moment Gyros and that too we are assuming that the center of mass of the control moment gyros and rest of the satellite it is a conceding. If you do not assume that then the system will be equation will be further complicated.

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Handwritten equations on a whiteboard:

$$\dot{\vec{h}}_{F/E} = {}^F I_F \left[\vec{\omega} + \dot{\psi} \hat{c}_3 + \dot{\theta} \hat{d}_2 + (\vec{\omega} + \dot{\psi} \hat{c}_2) \times (\dot{\theta} \hat{d}_2) + \vec{\omega} \times \dot{\psi} \hat{c}_3 \right] + \vec{\omega}_{F/E} \times {}^F I_F \vec{\omega}_{F/E} \quad \text{--- (C)}$$

Similarly for wheel equation can be written

$$\begin{aligned} {}^W \dot{\vec{h}}_W &= I_W \dot{\vec{\omega}}_{W/E} \\ &= I_W \left[\vec{\omega}_{W/F} + \vec{\omega}_{F/D} + \vec{\omega}_{D/B} + \vec{\omega}_{B/E} \right] \\ &= I_W \left[\dot{\theta} \hat{f}_1 + \dot{\theta} \hat{d}_2 + \dot{\psi} \hat{c}_3 + \vec{\omega} \right] \end{aligned}$$

$\left. \frac{d\vec{h}_W}{dt} \right|_E$

4

$\dot{\phi} = 2$

So, we can wind up here. We can write as h F slash E h dot F slash E this we have written as h dot F this part and then the other part. So, I F psi double dot c 3 cap; just rearranging the terms theta dot d2 cap this is this part. So, this part lastly I am writing omega cross this omega cross psi dot c 3 cap and plus I F F and times this cross. So, this is your equation number C. This we could have this term we could have written before this that is fine does not matter. Similarly, we write for similarly for the wheel equation can be written ok.

So, in that case h wheel we are writing that we are writing in the wheel frame itself ok. So, wheel is attached to the frame F which is a rotating frame ok. Omega wheel with respect to E this is the basic equation and omega wheel we can write as angular velocity

of the wheel with respect to the F frame plus angular velocity of the F frame with respect to the D frame and then angular velocity of the D frame with respect to the B frame. We are not writing with respect to the C frame because C and C is also fixed in the body and B is also fixed in the body. So, it is a just in matter of orientation ok. It is not rotating and this can be expanded as $I \omega_D + \omega_{D/B}$ and one more term is there $\omega_{B/E}$.

So, this is the rotation rate of the angular velocity of the body with respect to the E frame then with respect to the V frame, the outer frame angular velocity with respect to the outer frame and inner frame angular velocity and with respect to the inner frame wheel angular velocity. So, these are the four terms which are appearing here in this place. So, we can write this part is simply your $\dot{\omega}$ as per our earlier notation. $\omega_{D/B}$ this we have written as $\omega_{D/B} \psi \dot{c}^3 \text{ cap}$. So, this is $\psi \dot{c}^3 \text{ cap}$ and $\omega_{F/D}$. This is $\theta \dot{c}^2 \text{ cap}$ and this capital omega this is nothing but capital omega along the 1 direction of the frame F.

So, this is capital omega times $f_1 \text{ cap}$ ok. Now we need to differentiate this part again. This is not omega dot this is just omega, dot will come in the next step and here this capital omega which we have replaced phi dot by capital omega; you can keep phi dot as well it does not matter ok. So, the next step involves getting the dot of this means we have to differentiate this dh by dt . Write it in this format with respect to the E frame with respect to the inertial frame how it is changing. So, that we can do it on the next phase.

changing. And this particular part is called variable speed control moment gyros; this is variable speed CMG means you are changing also this and this provided 3 degree of control ok. Earlier with if your this wheel. If you cannot speed up this wheel say if $\dot{\omega}$ is not present $\dot{\omega}$ is 0, so, only 2 controls 2 access controls you are getting.

One along the this axis which is the outer frame and another you can get along this axis ok. If you restrain along this axis you get output here depending, if you are torquing along this you will get output along this axis, if you torque along this you will get output along this axis.

So, you just have to look into where the resultant control moment will be. So, under this assumption, now we can if we differentiate this; so, we can write here $I \dot{\omega}$ outside and then with respect to the F frame and this is $\dot{\omega} + \dot{\psi} \times \hat{c}_3 + \dot{\theta}_2 \hat{c}_2$ and $\hat{c}_1 \omega$ times f_1 cap and plus; so, this quantity is your ω wheel with respect to the E frame. So, here this will come as ω wheel with respect to E frame and cross I wheel times ω wheel. This from we need to expand here. Thank you for listening, we will continue in the next lecture.

Thank you very much.