

Space Flight Mechanics
Prof. M. Sinha
Department of Aerospace Engineering
Indian Institute of Technology, Kharagpur

Lecture No. # 15
Three Body Problem (contd.)

In the last lecture, we have been discussing about the three body problem. So, one of the major problem of this three body motion, what we saw that there this problem is absolutely not solvable even the two body problem, we saw that in the absolute sense the two body problem cannot be solved, only in some relative things, we were able to get some meaning full solution to that, but in the three body problem, obviously we were far away from any tangible solution, but if we do some assumption, when we make certain assumptions, then under that assumption it is a possible that the solution to three body problem can be obtained.

Say, in the case of the earth and the moon system, we can have a satellite, where which can be treated as a third body, so satellite can be treated as a mass of negligible mass. So, under that assumption, if we start working, so it is a definitely we are going to get certain solution which are very intuitive, and it gives us a feeling how the third body is moving with respect to these two primary bodies. So, let us start with the various basic assumptions, which we make for the motion of the three bodies in this case.

So from this we will call as a circularly restricted three body problem. So, the first assumption is the primary and secondary bodies move in circular orbit. Circular orbit say about their center of mass so the benefit of this assumption that the orbit is circular, you can directly see it orbit is not circular, so obviously here ω of the primary body it will be changing with primary bodies will be changing with time. So, in the circular orbit what we have that the angular motion, say the angular velocity of the satellite if this is the radius r , v is the velocity. So, in a circular orbit, this v remains a constant therefore, ω is also a constant but, in elliptical orbit we get extra complication in the sense that here ω becomes of function of r again. So, these beside this assumption, the second


assumption we make the third body the third body is very small as compared to the two larger bodies.

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3-Body Problem (Contd.)

Circularly Restricted 3-Body Problem.

① The primary and secondary bodies move in circular orbits about their center of mass.



② Third body is very small as compared to the two larger bodies so that its mass can be neglected.

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Lecture 15

So here, the primary this is assumed to be quite large as compared to the secondary body and the third body, it will be assumed to be quite small as compared to this primary and the secondary body and so that its mass can be neglected. So, mass can be neglected and the third assumption which is again which gives further restriction can be made or sometimes it is a made is that.

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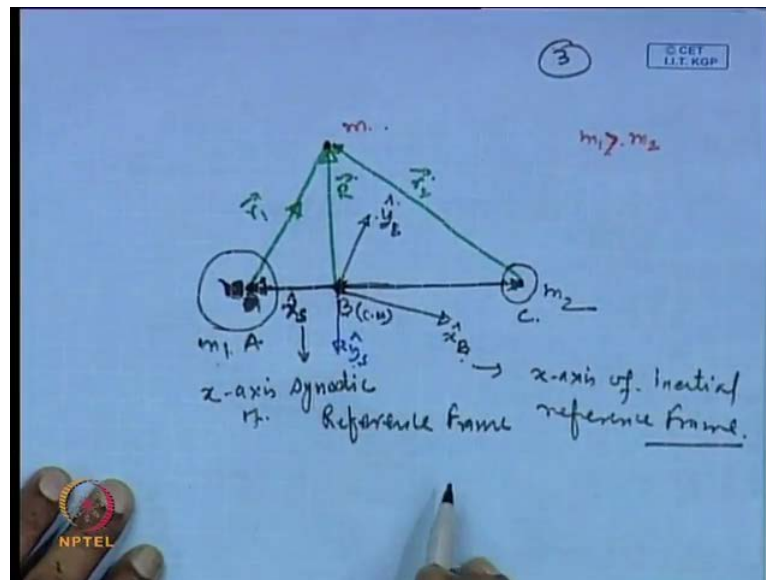
③ Additional constraint

The third body may be constrained to move in orbital plane of primary and secondary body.

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This is additional constraint, I will put this as a additional constraint only underthesetwo constraints we can work, butsometimes this may be available, so additional constraintso under this isthe third bodyconstrained to move in the orbital planarprimary and secondary body.



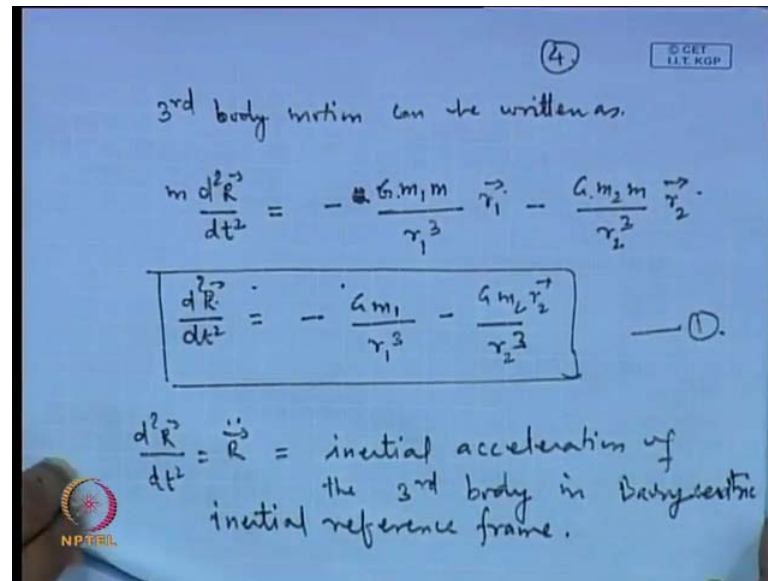
Now, let us assume that we take a reference frame which is fixed to the bary center but, not rotating along with the satellites. So, this bary center the reference frame fixed at the bary center, this will fall as a inertial reference frame, because the bary center is, we know that, if the two particles are n number of particles they are free from the external forces,if they are free from the external forces then they are center of mass most with a constant velocity.Sotherefore, we can fix an inertial reference frame at the bary center.

So, in this case we take the bary center, let us say \hat{x}_B is the unit vector and this direction and then we have \hat{y}_B is the unit vector perpendicular to the \hat{x}_B and \hat{x}_B and \hat{y}_B , they are lying in the orbital plane of m_1 and m_2 therefore, \hat{z}_B it will be coming out of this plane. So, \hat{z}_B will be perpendicular to the plane of m_1 and m_2 , the orbit of the m_1 and m_2 .

Similarly, we here this is the center of mass similarly, we fix another reference frame, which will be rotating at the same rate as this line joining the mass m_1 and m_2 is rotating means, that will be the period of the reference frame, which is fixed at this point at the bary center, but it is a rotating along with the masses and its period will be same as the period of the period of these two masses. Therefore, we take the direction of this, let us say this is the \hat{x}_s comma the \hat{x}_s cap. So, this is the \hat{x}_s of the here the subscript s stands for the synodic this is called synodic reference frame. And this is our \hat{x}_B , \hat{x} axis of the \hat{x} axis of synodic reference frame and this is the \hat{x} axis of inertial reference frame.

So, the \hat{y} axis of the synodic reference frame it will be pointing downward, so here \hat{x}_s and this becomes \hat{y}_s caps, because this is the unit vector in the \hat{y} direction for the synodic reference frame. So, the whole reference frame will be rotating along with the this to prime primary and the secondary bodies and then the \hat{z}_s which is the \hat{z}_s of the synodic reference frame, it is again coming out of the plane of the paper or the which is here in this case, we are assuming to with a plane of this two masses it is a plane of the orbit of these two masses. Let us assume that, m is the mass of the satellite which is quite negligible as compared to the mass m_1 and m_2 and we are assuming here also m_1 is greater than m_2 , r is the radius vector of the satellite in the inertial reference frame. Similarly, we can have this, we can write as r_1 and this is as r_2 , so r_1 and r_2 are the radius vector of the satellite mass m , this is the third body from the mass m_1 and from the mass m_2 .

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The image shows a handwritten derivation on a blue background. At the top right, there is a small box containing the text "CET IIT KGP". Below it, the text "(4)" is written. The main text reads: "3rd body motion can be written as." followed by the equation:
$$m \frac{d^2 \vec{R}}{dt^2} = - \frac{G m_1 m}{r_1^3} \vec{r}_1 - \frac{G m_2 m}{r_2^3} \vec{r}_2$$
 This equation is then boxed and labeled as equation (1). Below the box, the text reads:
$$\frac{d^2 \vec{R}}{dt^2} = \ddot{\vec{R}} = \text{inertial acceleration of the 3rd body in Barycentric inertial reference frame.}$$
 In the bottom left corner, there is a logo for NPTEL.

(4)

3rd body motion can be written as.

$$m \frac{d^2 \vec{R}}{dt^2} = - \frac{G m_1 m}{r_1^3} \vec{r}_1 - \frac{G m_2 m}{r_2^3} \vec{r}_2$$
$$\boxed{\frac{d^2 \vec{R}}{dt^2} = - \frac{G m_1}{r_1^3} \vec{r}_1 - \frac{G m_2}{r_2^3} \vec{r}_2} \quad \text{--- (1)}$$

$\frac{d^2 \vec{R}}{dt^2} = \ddot{\vec{R}} =$ inertial acceleration of the 3rd body in Barycentric inertial reference frame.

So, the equation of motion of the mass the body 3; so, the third body motion can be written as minus k times or G times m1 m divided by r 1 whole cube. So, our assumption that this mass third body mass is quite a small as compared to these two primary masses. So, that simplifies the situation that this two motion of this two masses can be certain quite easily as we have done earlier; for the two body case and the where the mass of the third body, because it is a very small, so it is a not at all affecting the motion of this two primary and the secondary bodies. Otherwise, if this mass becomes quite large, then the equally will affect the motion of the primary and the secondary mass and therefore, it would not be it would not be possible to solve this motion at all.

So, under this assumption we get d square R d t square, now here d square R d t square you can write this as R double dot this is nothing but, the inertial acceleration of the third body in bary centric inertial reference frame.

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The image shows a handwritten derivation of the equation of motion for a third body in a synodic reference frame. The equation is:

$$\ddot{\vec{R}} = \ddot{\vec{r}}_3 + \dot{\vec{\omega}}_s \times \vec{r}_3 + \vec{\omega}_s \times (\vec{\omega}_s \times \vec{r}_3) + 2\vec{\omega}_s \times \vec{v}_3 + \ddot{\vec{R}}_{s1} = 0$$

where:

- $\ddot{\vec{R}}$ is labeled as "inertial acceleration".
- $\ddot{\vec{r}}_3$ is labeled as "acceleration of the 3rd body in the synodic reference frame".
- $\vec{\omega}_s$ is labeled as "angular velocity of the synodic reference frame w.r. to the inertial reference frame".
- \vec{r}_3 is labeled as "radius vector of the 3rd body (satellite) in synodic Ref. frame".
- $\ddot{\vec{R}}_{s1}$ is labeled as "acceleration of the Earth origin of the synodic reference frame w.r. to the inertial reference frame".

Additional notes include $\dot{\vec{\omega}}_s = 0$ and a small diagram of a satellite in a circular orbit.

So, $\ddot{\vec{R}}$ double dot which is the inertial acceleration of the third body. So, this can be written in terms of the motion of the say, if here in this case this is our third body. So, this acceleration, we have got in terms of in the inertial reference frame but, we want to describe the motion of the third body with respect to the moving reference frame. So, what does it signify it signifies that our two masses are moving in this plane and with respect to this two masses means, the line joining this two, then how the motion of the third body can be described, one is this becomes again the relative motion this is not the motion in absolute sense.

So, this is the relative motion that, we are trying to ascertain so it is a very important that, if we have the third body moving with respect to these two primary bodies. So, what will be its location at any other time or in any other time in the future with respect to these two primary and the secondary body, so it will give us insight say, I want to locate certain satellite with respect to two bodies, then how the satellite motion will get affected with respect to these two bodies. So, that must be known before hand, so that can be done if we assume that if we try to resolve the motion the inertial motion with, if we try to get from the inertial motion the motion with respect to the moving reference frame which is the synodic reference frame here.

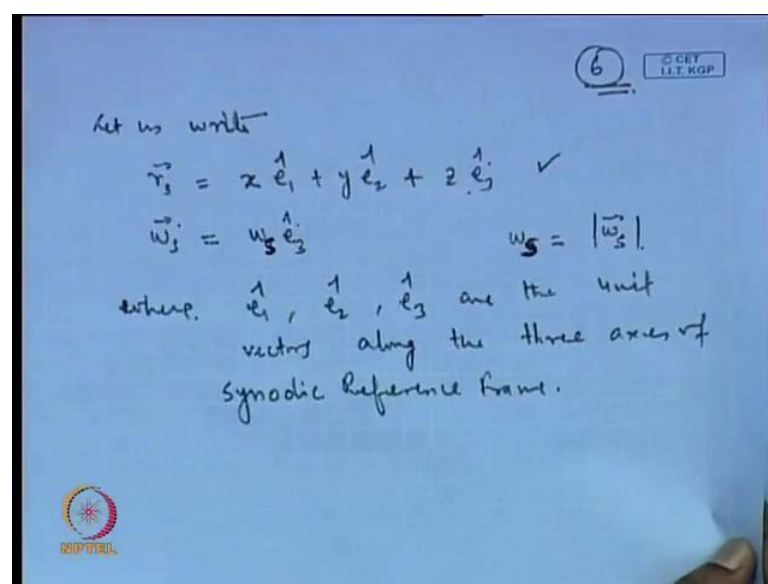
So, we tried to convert the inertial motion in synodic reference frame, so for doing that we know a very simple kinematic relationship which we have done earlier in our earlier

lecture. So, \ddot{R} which is nothing, but the inertial acceleration this can be written as \ddot{r}_s plus, so what exactly \ddot{r}_s is, I will come to know that so here this part this is the acceleration of the origin of the synodic reference frame with respect to the inertial reference frame. So because the synodic reference frame is fixed at the bary center, so it is not having any translational motion and therefore, this quantity becomes equal to 0.

Besides, $\dot{\omega}_s$ this quantity equal to 0, why this is so because we are assuming that the two primary and the two secondary bodies, these two bodies they are moving in a circular orbit and therefore, the ω_s is the rate at which these two are moving about their center of mass and therefore, if we fix a reference frame at this point at the bary center and let it move at the same rate means the ω_s in the reference frame will also move at the same rate. So therefore, the benefit of the circular orbit is that here we are not getting any change in the angular rate of the synodic reference frame and therefore, $\dot{\omega}_s$ can be set to 0.

So, this two greatly simplifies our situation, now \ddot{r}_s this is the acceleration of the third body in the synodic reference frame in a small r_s , this is the radius vector of the third body which here in this case is a satellite in synodic reference frame. So, we have $\dot{\omega}_s$ equal to 0 and \ddot{R}_o this quantity also equal to 0.

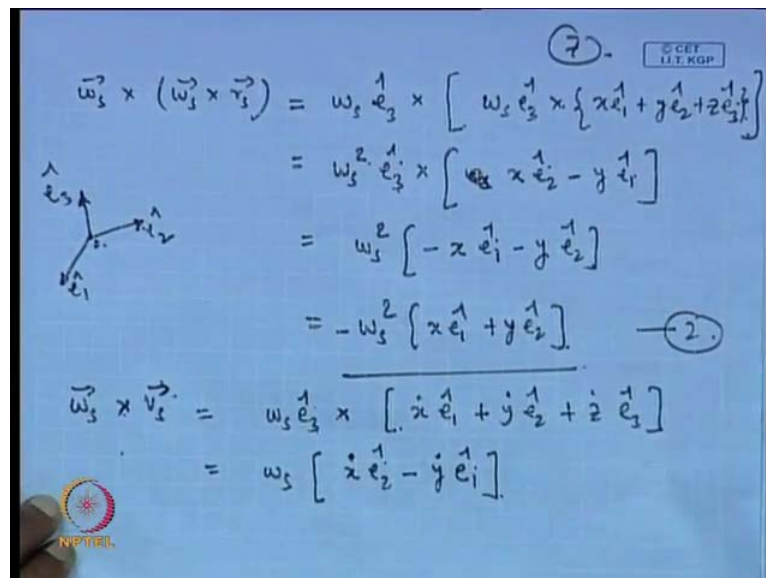
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Now let us write, so here \hat{e}_1 , \hat{e}_2 and \hat{e}_3 are the unit vector in the along the three axis of the synodic reference frame. So here, we have actually used the notations in this place this is the unit vector along the x direction and similarly, this is the unit vector along they direction, so this thing actually becomes \hat{e}_2 and this becomes nothing but, \hat{e}_1 cap and \hat{e}_3 cap will be coming out of this. So, this is just for the age of notation writing this is much easier so we can follow this, so \vec{r} is equal to x times this \hat{e}_1 cap plus y times \hat{e}_2 cap and z times \hat{e}_3 cap this is a simple relationship. Similarly, $\vec{\omega}_s$ the angular velocity of the synodic reference frame it can be written as ω_s times \hat{e}_3 cap. So, where ω_s is the magnitude of the $\vec{\omega}_s$ vector and \hat{e}_3 is the unit vector in the along the z axis of the synodic reference frame. ω_s is nothing but, or ω_s we can write as this as ω_s along the three axis of synodic reference frame, now we can evaluate the $\vec{r} \cdot \ddot{\vec{r}}$.

Now, we can evaluate this is the inertial acceleration, so by inserting all this quantities here so for this $\vec{\omega}_s \cdot \vec{r}$ this becomes equal to 0. So, one by one we will be able to a certain all of them and therefore, we can express the inertial acceleration in terms of the components of the quantities which are given here.

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The image shows a handwritten derivation on a blue background. On the left, there is a 3D coordinate system with axes labeled \hat{e}_1 , \hat{e}_2 , and \hat{e}_3 . The derivation consists of two main parts:

Part 1: Calculation of $\vec{\omega}_s \times (\vec{\omega}_s \times \vec{r})$.

$$\begin{aligned} \vec{\omega}_s \times (\vec{\omega}_s \times \vec{r}) &= \omega_s \hat{e}_3 \times \left[\omega_s \hat{e}_3 \times (x \hat{e}_1 + y \hat{e}_2 + z \hat{e}_3) \right] \\ &= \omega_s^2 \hat{e}_3 \times [x \hat{e}_2 - y \hat{e}_1] \\ &= \omega_s^2 [-x \hat{e}_1 - y \hat{e}_2] \\ &= -\omega_s^2 [x \hat{e}_1 + y \hat{e}_2] \end{aligned}$$

Part 2: Calculation of $\vec{\omega}_s \times \vec{v}_r$.

$$\begin{aligned} \vec{\omega}_s \times \vec{v}_r &= \omega_s \hat{e}_3 \times [\dot{x} \hat{e}_1 + \dot{y} \hat{e}_2 + \dot{z} \hat{e}_3] \\ &= \omega_s [\dot{x} \hat{e}_2 - \dot{y} \hat{e}_1] \end{aligned}$$

So, taking first $\vec{\omega}_s$ cross, one by one we work it out so we have \hat{e}_1 , \hat{e}_2 and \hat{e}_3 . So, $\hat{e}_3 \times \hat{e}_3$, this is nothing, but \hat{e}_2 . So, this becomes ω_s , ω_s we have already taken out so this is x times \hat{e}_2 then we have $\hat{e}_3 \times \hat{e}_2$, so $\hat{e}_3 \times \hat{e}_2$ this is minus

\mathbf{e}_1 and this is y times \mathbf{e}_1 and \mathbf{e}_3 cross \mathbf{e}_3 this becomes 0. Now, again working out this, so \mathbf{e}_3 cross \mathbf{e}_2 , \mathbf{e}_3 cross \mathbf{e}_2 , this is minus \mathbf{e}_1 so x times \mathbf{e}_1 cap and \mathbf{e}_3 cross \mathbf{e}_1 is nothing but, \mathbf{e}_2 so this is minus y times \mathbf{e}_2 cap this is our equation number 2. Also, we can estimate here itself $\boldsymbol{\omega}$ cross \mathbf{v}_s so \mathbf{v}_s is the velocity of the satellite for the velocity of the third body with respect to the synodic reference frame this become $\boldsymbol{\omega}_s$ \mathbf{e}_3 cap cross \mathbf{e}_3 cross \mathbf{e}_1 this is \mathbf{e}_2 so $x \dot{\mathbf{e}}_2$ cap \mathbf{e}_3 cross \mathbf{e}_2 is minus $y \dot{\mathbf{e}}_1$ cap and \mathbf{e}_3 cross \mathbf{e}_3 is 0.

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Handwritten mathematical derivation on a blue background:

$$\ddot{\mathbf{r}}_3 = (\ddot{x}\mathbf{e}_1 + \ddot{y}\mathbf{e}_2 + \ddot{z}\mathbf{e}_3) + \underbrace{-\omega_s^2 (x\mathbf{e}_1 + y\mathbf{e}_2)}_{+ 2\omega_s [\dot{x}\mathbf{e}_2 - \dot{y}\mathbf{e}_1]}$$

$$\ddot{\mathbf{r}} = -\frac{Gm_1}{r_{1s}^3}\mathbf{r}_{1s} - \frac{Gm_2}{r_{2s}^3}\mathbf{r}_{2s}$$

$$\mathbf{r}_{1s} = \mathbf{r} - \mathbf{r}_{B_1s}$$

$$= x\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3 - r_{B_1s}\mathbf{e}_1$$

$$= (x - r_{B_1s})\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3$$

Definitions on the right:

$$\mathbf{r}_F = \mathbf{R} - \mathbf{r}_{B_1}$$

$$\mathbf{r}_2 = \mathbf{R} - \mathbf{r}_{B_2}$$

$$\mathbf{r}_1 = \mathbf{r}_{1s}$$

$$\mathbf{r}_2 = \mathbf{r}_{2s}$$

Therefore, $\ddot{\mathbf{R}}$, this can be written as, so $\ddot{\mathbf{r}}_s$. Now, the quantity we have shown here $\ddot{\mathbf{r}}_s$ this is a acceleration of the third body in the synodic reference frame. So this will be nothing but, $\ddot{x}\mathbf{e}_1 + \ddot{y}\mathbf{e}_2 + \ddot{z}\mathbf{e}_3$ cap and rest put other things so $\boldsymbol{\omega}$ cross \mathbf{r}_s this quantity, we have just now determined this quantity is minus $\omega_s^2 x\mathbf{e}_1$ cap plus $y\mathbf{e}_2$ cap and then the third quantity which is remaining is two times $\boldsymbol{\omega}$ cross \mathbf{v}_s , so this becomes two times ω_s times. So, this is the inertial acceleration which are expressed in terms of the acceleration along the body, this synodic reference frame components this are the acceleration with respect to the synodic reference frame of the third body and these are raising because of the rotation of the synodic reference frame itself. So, if we can recognize these acceleration this acceleration is nothing but, the coriolis term.

While this term you can visualize as the, what you call as the centripetal acceleration, so it is a very easy to work it out and look into this so whenever some particles for

somebody is moving with respect to a rotating reference frame to it fills some the what is called the coriolis force, so the this is expressed here this is the coriolis term this is the centripetal term coriolis. So, also \ddot{R} this we can write as we have earlier written as $-\frac{GM}{r^3}$. Now, if we look into the original figure this figure s or 1 is a in this equation r_1 is basically this is with respect to the inertial reference frame means these are taken in barycentric reference frame. But if we look into the this quantity and our reference frame which is a synodic reference frame this is rotating at ω , but what happens either we take the inertial reference frame or the synodic reference frame these are the invariant quantities, they do not differ only the components along their body axis will change but, as you hold this quantity remains invariant.

So therefore, we can express this r the r_1 and this r_1 and r_2 in the synodic reference frame itself and therefore, we can compute the corresponding sum, so what exactly we are doing so we know the acceleration here in the synodic reference frame and the left hand side is the inertial reference frame acceleration in the inertial reference frame. So, inertial reference frame components can be broken along the synodic reference frame and that makes us easier to put this all these expression in a compact form. So, following this we can put a subscript here to indicate this these are in the synodic reference frame because these are the invariant quantities so we have r_{1s} which is nothing but, the r vector minus the mass of the or we write it as r_{1B} which is the radius vector of the this quantity we can write as r_{1B} this is the vector from here to here.

So to the mass 1 this is the vector r_{1B} so r_1 becomes r minus r_{1B} similarly, we here we can write this as r_{2B} so r_2 that can be written as so we can write here as r_1 equal to r minus r_{1B} and r_2 is equal to r minus r_{2B} . Now, more over a in the same notation will also follow in the quantity r_1 and r_2 they are invariant so these are equivalent to r_{1s} and r_2 to r_{2s} . So, we can replace in terms of this here in this quantities, so once we replace it so this expression will become further simplified. So, r_{1s} r_{1s} then we can write as $x e_1$ means, then we are expressing in terms of the synodic reference frame so r minus where r is the radius vector of the third body with respect to the synodic reference frame. So, this becomes r minus r_{1B} in the synodic reference frame.

So, this we can then express as x times e_1 cap plus y times e_2 cap plus z times e_3 cap minus r_{1B} and because this is in the synodic reference frame this is directed along the x axis.

So here, we will have this as \hat{e}_1 and this is you can see here this is directed along the synodic body x therefore, whatever the magnitude of this vector is this and this is multiplied by the unit vector. This again we can bring together and write them as $x\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3$.

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$$\begin{aligned}
 &= (x\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3) - r_{B,S}(-\hat{e}_1) \\
 &= (x + r_{B,S})\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3 \\
 \ddot{\mathbf{r}} &= (\ddot{x} - \omega_s^2 x - 2\omega_s \dot{y})\hat{e}_1 \\
 &\quad + (\ddot{y} - \omega_s^2 y + 2\omega_s \dot{x})\hat{e}_2 + \ddot{z}\hat{e}_3 \\
 &= -\frac{Gm_1}{r_{1,2}^3} [(x - r_{B,S})\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3] \\
 &\quad - \frac{Gm_2}{r_{2,3}^3} [(x + r_{B,S})\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3]
 \end{aligned}$$

Similarly, we can write for the r_2 also, so r_2 this can be written as r minus r_2 b s which is $x\hat{e}_1 + y\hat{e}_2 + z\hat{e}_3$ and minus $r_{B,S}$ and this is directed along the r_2 b, r_2 b is here just directed opposite to the even direction it is here and therefore, we can write this as and \hat{e}_1 is positive in this direction so minus \hat{e}_1 cap so this becomes x plus r_2 b s \hat{e}_1 cap plus $y\hat{e}_2 + z\hat{e}_3$. So, once we have written in this fashion then we can assemble all the things together look into this equation $\ddot{\mathbf{R}}$ double dot here the \hat{e}_1 term can be brought together \hat{e}_2 terms can be brought together and \hat{e}_3 will be left alone and we can simplify this equation.

So $\ddot{\mathbf{R}}$ double dot, now this can be written as x double dot minus x times or $\omega_s^2 x$ minus $2\omega_s y \dot{x}$ times \hat{e}_1 cap plus y double dot minus $\omega_s^2 y$ plus $2\omega_s x \dot{y}$ times \hat{e}_2 cap and lastly the $z\hat{e}_3$. The z component it can be brought. So, once we have expressed this so this will be equal to nothing but, G times m_1 r_1 s whole cube and then r_1 s vector we have to bring in here so that is x minus $r_{B,S}$ $z\hat{e}_3$ cap minus $G m_2$ divided by r_2 s cube x plus $r_{B,S}$ x plus $r_{B,S}$ times \hat{e}_1 plus $y\hat{e}_2$ cap plus $z\hat{e}_3$ cap. Now, you can see that on the left hand side

all the terms are grouped together with e_1 , e_2 cap and e_3 cap similarly, on the right hand side we can bring the terms together with the e_1 cap, e_2 cap and e_3 cap and compare them so we get three second order differential equation. So this three second order differential equation they describe the relative motion of the third body with respect to these two primary and the secondary bodies.

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collecting the similar terms together

$$\ddot{x} - \omega_s^2 x - 2\omega_s \dot{y} = -\frac{Gm_1}{r_{1s}^3} (x - r_{1s}) - \frac{Gm_2}{r_{2s}^3} (x + r_{2s})$$

$$\ddot{y} - \omega_s^2 y + 2\omega_s \dot{x} = -\frac{Gm_1}{r_{1s}^3} y - \frac{Gm_2}{r_{2s}^3} y$$

$$\ddot{z} = -\frac{Gm_1}{r_{1s}^3} z - \frac{Gm_2}{r_{2s}^3} z$$

$Gm_1 = \mu_1$
 $Gm_2 = \mu_2$

These 3 diff. Eqs. describe the relative motion of the 3rd body w.r.t. the two primary & secondary bodies.

So, collecting the similar terms together we can write $x \ddot{} - 2\omega_s y \dot{} = -\frac{Gm_1}{r_{1s}^3} (x - r_{1s}) - \frac{Gm_2}{r_{2s}^3} (x + r_{2s})$ this will be equal to $-\frac{Gm_1}{r_{1s}^3} x + \frac{Gm_1}{r_{1s}^3} r_{1s} - \frac{Gm_2}{r_{2s}^3} x - \frac{Gm_2}{r_{2s}^3} r_{2s}$. Similarly, the other 2 equations can be written, so the other 2 equations then for the y motion $y \ddot{} + 2\omega_s x \dot{} = -\frac{Gm_1}{r_{1s}^3} y - \frac{Gm_2}{r_{2s}^3} y$, this will be equal to $-\frac{Gm_1}{r_{1s}^3} y - \frac{Gm_2}{r_{2s}^3} y$. And lastly, the z double dot this can be written as $z \ddot{} = -\frac{Gm_1}{r_{1s}^3} z - \frac{Gm_2}{r_{2s}^3} z$, for simplification we can assume Gm_1 is equal to let us say μ_1 and Gm_2 is equal to μ_2 . Now, these are the three differential equations which describe the these three differential equations, describe the relative motion of third body with respect to the two primary and secondary bodies with respect to the primary and secondary bodies. Now, to solve this equations so let us term this equation as a this as b and this as c.

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we need to solve these equations. But we do it in implicit way -

Multiplying equation (A) by $2\dot{x}$, (B) by $2\dot{y}$ and eq. (C) by $2\dot{z}$ and adding them up.

$$2\ddot{x} + 2\ddot{y} + 2\ddot{z} - 2\omega_s^2 (\dot{x}x + \dot{y}y) + 4\omega_s \dot{x}\dot{y} + 4\omega_s \dot{x}\dot{y} = -2\dot{x} \left[\frac{\mu_1}{r_1^3} (x - r_{B1x}) + \frac{\omega_e}{r_2^3} (x + r_{B2x}) \right] + \text{other terms on the right hand side}$$

To solve these equations, but we do it in an implicit way, but we do it in an implicit way and this we achieved by multiplying equations A, B and C. These are the equations A, B and C, and this we multiply by $2\dot{x}$, $2\dot{y}$ and $2\dot{z}$ respectively, and add them up. So, multiplying equations A by $2\dot{x}$, B by $2\dot{y}$ and equation C by $2\dot{z}$ and adding them up. So, you can see that the terms that we get this will be $2\dot{x}$ times x double dot which is coming from this equation. Similarly, from the equation we will get the term $2\dot{y}$ times y double dot and from the equation c, we get $2\dot{z}$ times z double dot. Now, next we take these two terms; $\omega_s x$, $\omega_s^2 x$ and $\omega_s^2 y$ and here, we do not give any other term, so only one term is present in the equation number c.

So, next we get two times ω_s^2 and \dot{x} times x plus \dot{y} times y and thereafter, we have these two terms and these two terms are of opposite sign and this, we are multiplying by \dot{x} and this by \dot{y} , so they will cancel out each other but, still I write here in this place, so we will have two into two, this is four and this is four times ω_s^2 times $\dot{x}\dot{y}$ and plus four times ω_s^2 times $\dot{x}\dot{y}$. So, these two terms will cancel out. On the right hand side, we will have minus $2\dot{x}$ times rest other terms from here, we have to multiply by \dot{x} , $2\dot{y}$ and $2\dot{z}$ and copy it here in this place. So, Gm_1 we are writing as μ_1 , so $2\dot{x}$ dot μ_1 by r_1^3 times x minus r_{B1x} next this term we have to pick up so this equation is a bit long.

But we have to write it here, so this is $G m$, so $G m^2$ we replace as μm^2 . So, this is μm^2 divided by r^2 s whole cube and x plus r^2 s x plus r^2 s this term the term which is present here this is appearing and we close the bracket here. So, we will have to take to the next page plus other terms other terms on next page. So, left hand side we cancel out these two terms.

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$$\begin{aligned}
 & -2\dot{y} \left[\frac{\mu_1}{r_1^3} y + \frac{\mu_2}{r_2^3} y \right] - 2\dot{z} \left[\frac{\mu_1}{r_1^3} z + \frac{\mu_2}{r_2^3} z \right] \\
 \text{L.H.S} &= 2(\dot{x}\ddot{x} + \dot{y}\ddot{y} + \dot{z}\ddot{z}) - 2\omega_s^2(\dot{x}x + \dot{y}y) \\
 &= \frac{d}{dt}(\dot{x}^2 + \dot{y}^2 + \dot{z}^2) - 2\omega_s^2 \frac{d}{dt}(x^2 + y^2) \\
 &= \frac{d}{dt} \left[\dot{x}^2 + \dot{y}^2 + \dot{z}^2 - \omega_s^2(x^2 + y^2) \right]
 \end{aligned}$$

Here, so the other remaining terms are, then these terms is to be multiplied by 2 y dot. So, minus 2 y dot times $\mu_1 G m_1$, we are writing as μ_1 by r_1 s cube plus y this term becomes μ_2 by r_2 s whole cube and this is also y minus sign has gone outside in. Here, in this place and then the last term is remaining here which is again minus sign, we can take it out side and this is 2 z dot multiplied by this is μ_1 and this is μ_2 . So, accordingly we write here μ_1 by r_1 s whole cube and then multiplied by z plus μ_2 by r_2 s whole cube multiplied by z . So after completing this, then the whole equation can be written as two times the L.H.S can be written as, two times x dot times x double dot plus two times y dot times y double dot plus two times z dot times z double dot equal to plus the other terms we have minus 2 times ω_s square times x dot x plus y dot y this the we are writing the L.H.S, L.H.S equal to this.

So, this becomes the first term becomes d by $d t$ x dot square plus y dot square plus z dot square if you differentiate you get this quantity and these term similarly, we can write here 2 ω_s square times x square plus y square and this is d by $d t$ so d by $d t$ here we

write so this is your L.H.S. So, this gets reduced to $\frac{d}{dt} (x^2 + y^2 + z^2 - \omega_s^2 (x^2 + y^2))$ plus z^2 dot square minus. The factor two which is appearing here, this factor will not be there, because once we differentiate this quantity here. So, two will be appearing so two is that two gets accounted here, so another way if we are writing it in this format this two gets absorbed here this side similarly, this two has got absorbed here in this side. So, this we get ω_s^2 and plus x^2 plus y^2 .

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$$\frac{d}{dt} \left[\dot{x}^2 + \dot{y}^2 + \dot{z}^2 - \omega_s^2 (x^2 + y^2) \right] = -2\dot{x} \left[\frac{\mu_1}{r_{1s}^3} (x - r_{1s}) \right]$$

$$+ \frac{\mu_2}{r_{2s}^3} (x + r_{2s}) \Big] - 2\dot{y} \left[\frac{\mu_1}{r_{1s}^3} y + \frac{\mu_2}{r_{2s}^3} y \right]$$

$$- 2\dot{z} \left[\frac{\mu_1}{r_{1s}^3} z + \frac{\mu_2}{r_{2s}^3} z \right]$$

$Gm_1 = \mu_1$
 $Gm_2 = \mu_2$

So finally, our equation gets reduced to the format $\frac{d}{dt} (x^2 + y^2 + z^2 - \omega_s^2 (x^2 + y^2))$ plus z^2 dot square minus ω_s^2 times x^2 plus y^2 this is equal to the all other terms. Now, we have to mention in this place, so this is equal to $-2\dot{x} \left[\frac{\mu_1}{r_{1s}^3} (x - r_{1s}) + \frac{\mu_2}{r_{2s}^3} (x + r_{2s}) \right] - 2\dot{y} \left[\frac{\mu_1}{r_{1s}^3} y + \frac{\mu_2}{r_{2s}^3} y \right] - 2\dot{z} \left[\frac{\mu_1}{r_{1s}^3} z + \frac{\mu_2}{r_{2s}^3} z \right]$. So, and where we have written Gm_1 is equal to μ_1 and Gm_2 is equal to μ_2 so we have got equation in this format, but still it is not complete we need to integrate it. So, we will do that integration in the next lecture, time is getting over. So thank you very much we continue in the next lecture with the remaining portion.