

Introduction to Finite Volume Methods-I
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Lecture – 27
Discretization of Diffusion Equation for Cartesian orthogonal systems-II

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Diffusion Equation

$-\nabla \cdot (\Gamma \nabla \phi) = Q$ stencil

$S_f =$ surface normal vector ($f = e, w, n, s$)

$a_c \phi_c + a_E \phi_E + a_W \phi_W + a_N \phi_N + a_S \phi_S = b_c$

$Ax = b$

any interior element

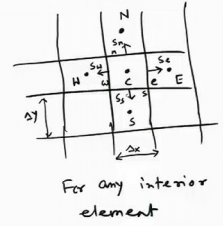
Compact form:

$$a_c \phi_c + \sum_{F \in \text{NB}(c)} a_F \phi_F = b_c$$


$$a_F = \text{Flux}_F = -\Gamma_f D_f \quad , \quad a_c = \sum_{f \in \text{NB}(c)} \text{Flux}_f C_f$$

$$b_c = Q_c V_c - \sum_{f \in \text{NB}(c)} \text{Flux}_f V_f$$

$F: E, W, N, S \text{ (elements)}$
 $f: e, w, n, s \text{ (faces)}$



For any interior element Uniform



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So welcome to the lecture of this Finite Volume Method and we will continue our discussion on Diffusion Equation. What we have done so far is that essentially looking at the 2 dimensional system and just to before begin with we just quickly give you an recap, this is the governing equation that we have looked into and the elemental control volume that we have considered is c and the ahead of it East downstream of it West, then top North and bottom South.

This was the 2 dimensional stencil or the discretized indexing that we have taken for some interior node; this is for any interior element. So, considering an interior element, we have actually derived the discretised system from this system. So, what are the convention?

So, once we finally, use that this is the face E, this is the faced West, this is the face South and North this has the surface vector that are used in the derivation of that. So, this is S e, this is S n, this is S w, this is S s. So, all this S i essentially or S f these are the surface normal vector where f goes from east, west, north, south and also this 2

dimensional grid system is uniform. So, it was a uniform system; so, we had this one Δx , similarly this one also Δy .

So, once we have done the discretization this governing equation actually gets us this $a_C \phi_C + a_E \phi_E + a_W \phi_W + a_N \phi_N + a_S \phi_S = b_C$. So, this is the discretized equation that we obtain for any interior element any interior element is governed by this particular set of.

So, essentially this discretized equation is going to get you the $A x = b$. And while doing this all our coefficients were essentially in a compact form. If one has to write in a compact form then it was $a_C \phi_C + \sum F \phi_F = b_C$. And all these coefficients like a_F was flux F_f which is $-\gamma_f D_f$; a_C was summation of small f goes from all the faces equals to flux and b_C is $Q_C V_C$ minus summation of all the small faces flux V_f .

And capital F in all these stands for east, west, north, south, this is for elements. So, the element C is sort of surrounded by all these 4 elements; east, west, north, south and small f is essentially the corresponds to the faces. So, the face like this is c ; e is a common face between element E and C , north face is a common face between N and C , west face is a common face between C and the west element and the east face is between. So, this is what we obtain and then to get the solution done; we need to apply for the boundary condition.

The first type of boundary condition that we have applied is the Dirichlet boundary condition; so, Dirichlet boundary condition.

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Diffusion Equation

I: Dirichlet B.C. : ✓ \rightarrow both of them are applied/considered at 'e' face

II: Neumann B.C. : At the boundary face - 'b'

$$-(\nabla\phi)_b \cdot \mathbf{i} = q_b$$

$$\mathbf{J}_b \cdot \mathbf{S}_b = -(\nabla\phi)_b \cdot \|\mathbf{S}_b\| \mathbf{i} = q_b \|\mathbf{S}_b\|$$

$$= \text{Flux}_C \phi_C + \text{Flux}_V b$$

$\text{Flux}_C = 0$, $\text{Flux}_V b = q_b \|\mathbf{S}_b\| = q_b (\Delta V)_c$ (sign of flux is assumed to be +ve)

Apply all of the above ,

$$a_E \phi_E + a_W \phi_W + a_N \phi_N + a_S \phi_S = b_c$$

$a_E = 0$
 $a_W = \text{Flux}_W = -\Gamma_{W,c} D_{W,c}$
 $a_N = \text{Flux}_N = -\Gamma_{N,c} D_{N,c}$
 $a_S = \text{Flux}_S = -\Gamma_{S,c} D_{S,c}$

$$a_c = \sum_{f \sim nb(c)} \text{Flux}_f = -(a_W + a_N + a_S)$$

$$b_c = a_c \phi_c - (\text{Flux}_V b + \sum_{f \sim nb(c)} \text{Flux}_f)$$

$\nabla\phi \cdot \mathbf{n}_b$
 $\mathbf{i} \rightarrow \mathbf{S}_b = q_b \mathbf{i}$
 $\Gamma_{B,c}$

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So, this one and then accordingly we have modified the system and the modified equation was obtained. Now the second kind of boundary condition; so, this was also discussed in the earlier lecture; so, the next one. So, what happens when we apply the boundary condition? Essentially this is the governing equation. Now this is actually valid for all the interior elements, but when it comes down to the boundary element or the face at the boundary, this particular equation needs to be modified.

For example when we had a boundary at east face; the contribution for this cell will get drops down, at the same time some terms will appear at the source term due to the specified variable. Similarly if the boundary face belongs to north automatically these guy would go up the north contribution if it is at the west; the a W phi W goes up; if it is the south a S phi S goes up. So, that is how for a Dirichlet boundary condition one can arrive the cell. Now will look at the second type of boundary condition is the Neumann boundary condition.

So, for that if you just look at that element then you see how that Neumann boundary condition can be applied. So, this is my face and this would be the boundary face; this is element C, this is South, this is West, this is North, this is North West, this is South West and this face is the and here now this is the point b and that Neumann condition. So, this is the direction of the surface vector this will be the direction of the south face surface vector S W, S N.

Now, the Neumann condition is nothing, but something the gradient is minus $\nabla \phi_b \cdot \mathbf{n}_b$ equals to q_b specified. So, that is the Neumann boundary condition; so, essentially what does that mean the gradient at that particular face. So, now, if you look at that element C which actually one of its face the east face belongs to the boundary the gradient condition is prescribed. So, the condition which is prescribed at the boundary face that is b is minus $\gamma \nabla \phi_b \cdot \mathbf{i}$ equals to q_b .

In other words, one can write the diffusion flux at \dot{b} equals to minus $\gamma \nabla \phi_b \cdot \mathbf{S}_b$, which will be $q_b S_b$ which is equivalent to the flux which is defined there $C_b \phi_C$ plus flux V_b and these are the coefficients. So, this coefficients one need to find out and if you look at this particular condition they turn out to be the flux C_b would be 0 and the flux V_b would be $q_b S_b$ which is essentially $q_b \Delta y_c$.

So, that is what you get; now one thing you can note here the sign of the flux component, the sign of flux is assumed to be positive that is why it has been considered pointing outward. Now, this equation of the q_b or the information of the q_b this could be directly included in the system. And like this could be directly imposed in this particular equation and what we can get. So, once you apply all of the above conditions what we get a $C \phi_C$ plus a $W \phi_W$ plus a $N \phi_N$ plus a $S \phi_S$ equals to b_c .

So, again if you look at this particular equation it looks exactly similar to the condition that we derived for the Dirichlet boundary condition. So, but that does not mean they would be of similar expression the mathematical expression or the discretised system looks similar; the reason being both the boundary condition whether the ϕ_b specified that Dirichlet boundary conditions or the Neumann boundary condition current now currently which we are talking or discussing both of them have been applied at this particular face which is at the east face.

So, the commonality between them is that both of them are applied or considered at east face that is why the representative discretized equation they look similar. But the points which are going to be different is that a is 0 here, a_W would be flux F_w which is minus $\gamma_w D_w$; a_N is flux F_n which is minus $\gamma_n D_n$, a_S is flux F_s which is $\gamma_s D_s$ and we have a C ; which is summation of faces and flux c_f ; essentially that becomes a W plus a N plus a S ok.

And the difference would appear in this particular source term the b_c ; which is going to be; now $Q_c - b_c$ minus flux V_b plus summation of over the faces flux V_f . Now this is the difference that would appear for the Dirichlet a Neumann boundary condition. Now, there are few important comments.

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Diffusion Equation

Comment: (i) Neumann B.C. does not result in a dominant a_c coefficient.

(ii) If both q_b & s_c are zero, then ϕ_c is bounded by its neighbors.
 $\phi \equiv T$, $q_b = \text{H. Flux}$.

(iii) Once ϕ_c is computed, the boundary value ϕ_b can be computed as

$$\phi_b = \frac{\Gamma_b D_b \phi_c - q_b}{\Gamma_b D_b}$$

(iv) Neumann \rightarrow natural B.C. for FVM.

(v) Mixed B.C.
 Heat Transfer Coeff. = (h_x)
 $J_b^q \cdot s_b = -(\Gamma_b \nabla \phi)_b$. $i s_b = -h_x (\phi_x - \phi_b) (\Delta y)_c$
 $-\Gamma_b s_b \left(\frac{\phi_b - \phi_c}{\Delta x_b} \right) = -h_x (\phi_x - \phi_b) s_b$

x boundary face

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So, or observation for this things; one of the important observation is that this Neumann boundary condition, Neumann boundary condition does not result in a dominant a_c coefficient. That is a very important observation, number 2 if both q_b and s_c are 0 then ϕ_c is bounded by its neighbours; otherwise what can happen? ϕ_c can exceed or fall below the neighbour value of ϕ whichever is admissible.

Now for example, and you can get it more clear. For example, if ϕ let us say represent temperature, ϕ is equivalent to temperature. If ϕ is temperature and q_b represents the heat flux; so, heat flux applied at the boundary; that means, either the heat is added or heat is taken out from the boundary, then the region close to that boundary it is expected to have higher or lower temperature compared to that interior. So, that is what it says that; whatever information you have accordingly they would be bounded.

Now, third point once ϕ_c is computed; once that is computed the boundary value ϕ_b can be computed; as ϕ_b equals to $\Gamma_b D_b \phi_c - q_b$ divided by $\Gamma_b D_b$. So, from the ϕ_c once that elemental variable is calculated, you can calculate back the specified value. And the last one is that actually this Neumann condition this

Neumann condition can be treated as natural boundary condition for Finite Volume Method for boundary condition for FVM. Because this means whenever we are dealing with some flows or heat transfer related problem; if the flux is specified that is quite handy to implement infinite volume method.

So whether the in terms of discretization of that particular face element or other way round; so, these are certain observation that is there. Now the third kind of boundary condition is the mixed boundary condition. So, mixed boundary condition which will mean if we again draw this; elements and apply the boundary condition. So, this is my element C, this would be north, this is west, this is south and the boundary condition which is applied here this is point b.

So here the boundary condition which is applied at ϕ_{∞} and ϕ_b ; so, both of them are specified. So, these are the surface normal vector north west south west and this is the face of the boundary; so, this is the boundary face. Now again the condition here is specified to the mixed condition. So, you have a some sort of a heat transfer coefficient or convective heat transfer coefficient is specified which is based on h_{∞} .

Now the flux which one can write for that is $-\gamma \nabla \phi_b \cdot \mathbf{i}_S$; which is going to be $-\gamma_{\infty} (\phi_{\infty} - \phi_b) / \Delta Y$ ok. So, here you got the both the information in the mixed boundary condition, which is another way people call it a robin boundary condition or mixed boundary condition where you have both the Neumann kind of boundary condition given a flux and also the specified value is also provided. So, both of them are acted simultaneously at the same face.

So, if you rewrite this expression one can write $\gamma_b S_b (\phi_b - \phi_C) / \Delta x_b$ which is $-\gamma_{\infty} (\phi_{\infty} - \phi_b) / \Delta Y$; so, that is what it gets you back.

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Diffusion Equation

Find out ϕ_b from the above expression:

$$\phi_b = \frac{h_\infty \phi_c + (\Gamma_b / \delta x_b) \phi_c}{h_\infty + (\Gamma_b / \delta x_b)}$$

Input this to the flux expression,

$$J_b \cdot S_b = - \underbrace{\left[\frac{h_\infty (\Gamma_b / \delta x_b)}{h_\infty + (\Gamma_b / \delta x_b)} S_b \right]}_{R_{eq}} (\phi_\infty - \phi_c)$$



$$= \text{Flux } C_b \phi_c + \text{Flux } V_b$$

$\text{Flux } C_b = R_{eq}$, $\text{Flux } V_b = -R_{eq} \phi_\infty$

obtained discretized eqn:

$$a_c \phi_c + a_w \phi_w + a_n \phi_n + a_s \phi_s = b_c$$

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Now once you get back these you can find out ϕ_b from the above expression which is going to be as $h_\infty \phi_c + \Gamma_b / \delta x_b \phi_c$ divided by $h_\infty + \Gamma_b / \delta x_b$.

Now, this one you apply it back in this particular flux information. So, the information of ϕ_b ; once you input this to the flux expression; one can get $J_b \cdot S_b$ equals to minus $h_\infty \Gamma_b / \delta x_b$ divided by $h_\infty + \Gamma_b / \delta x_b$; S_b into $\phi_\infty - \phi_c$. And this particular term one can think about as an resistance or some sort of a equivalent resistance and you represent this one as R_{eq} .

So, it is an some kind of an resistance which is applied here which is also it can be written as 2 coefficient; one is flux $C_b \phi_c$ plus flux V_b . So, you got the expression for the flux which is applied there and using the information of the given value you find out these coefficients; where flux C_b is nothing, but this R_{eq} and flux V_b is minus $R_{eq} \phi_\infty$.

So, once you use this information and again put it in the. So, the obtained discretized equation would have the expression like $a_c \phi_c + a_w \phi_w + a_n \phi_n + a_s \phi_s = b_c$; again if you look at the similarity between your Neumann condition, the expression which is obtained here and the expression which is obtained for the mixed condition; they look similar algebraically or notation wise they look exactly similar.

And the reason is as I have said earlier this is going to be applied at the east face of this cell. This is my C element and all these boundary conditions are applied at the east face if it would have been applied to the other faces like west north or south; those corresponding contribution terms would go away, but the difference is lie in the calculation of these coefficients and also b c.

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Diffusion Equation

$$a_E = 0$$

$$a_W = \text{Flux } F_w = -\Gamma_w D_w, \quad a_N = \text{Flux } F_n = -\Gamma_n D_n, \quad a_S = \text{Flux } F_s = -\Gamma_s D_s$$

$$a_C = \text{Flux } C_b + \sum_{\text{func}(c)} \text{Flux } C_f = \text{Flux } C_b + \text{Flux } C_w + \text{Flux } C_n + \text{Flux } C_s$$

$$b_C = Q_C V_C - \left(\text{Flux } V_b + \sum_{\text{func}(c)} \text{Flux } V_f \right)$$

IV: Symmetric B.C.

→ Normal flux to the boundary of a scal variable $\phi = 0$

≡ Neumann B.C. $\Rightarrow \text{Flux } C_b = \text{Flux } V_b = 0$

$a_C \phi_C + a_W \phi_W + a_N \phi_N + a_S \phi_S = b_C$

applied at 'e' face

$$a_E = 0, \quad a_W = -\Gamma_w D_w, \quad a_N = -\Gamma_n D_n, \quad a_S = -\Gamma_s D_s; \quad a_C = -(a_W + a_N + a_S)$$

$$b_C = Q_C V_C - \sum_{\text{func}(c)} \text{Flux } V_f$$

So, in the similar fashion for this mixed case we get a E equals to 0, a W would be flux F w which is minus gamma w D w; a N is flux F n which is minus gamma n D n; a S is flux F s which is minus gamma s D s and a C is flux C b plus summation over faces of flux C f, which is going to be flux C b plus flux C w plus flux C n plus flux C s. And my b c is the Q c V c minus flux V b plus summation over faces for flux V f ok.

So, though the discretized algebraic equation looks similar for all sort of conditions like Dirichlet condition, Neumann condition and mix condition, but the differences lie in the expression of this coefficients and the source term. Now have been said that will move to the these are the primary 3 boundary conditions which one can come across while applying the boundary conditions for a physical problem.

Either you have a specified value or you will have an applied flux; let us say for example, if you are dealing with a flow through a channel. This is the inlet this is the outlet at the outlet one can always assume the flux is 0. So, that is a short of a Neumann

boundary condition or in some cases where you may have both the Dirichlet and Neumann applied together which correspond to the mixed condition.

Now moving ahead there would be fourth type of boundary condition which can be also used which is a symmetric boundary condition. Now typically along a symmetric boundary the normal flux to the boundary of a scalar variable ϕ is 0. So, symmetry boundary condition is sort of equivalent to Neumann kind of boundary condition; Neumann boundary condition.

So, there is a equivalency between symmetric boundary condition with the Neumann boundary condition because what it says that is the normal to that boundary the flux of the variable is 0. So, if it is equivalent to the Neumann boundary condition so; that means, it will give rise to that flux C_b or flux V_b they are 0. So, the discretized equation which can be modified for symmetry boundary condition and again can be written as if the symmetry boundary condition again applied at the east face this is my C_e ; it is applied at east face.

So, the discretized equation would look like $a_C \phi_C$ plus $a_W \phi_W$ plus $a_N \phi_N$ plus $a_S \phi_S$ equals to b_c ; where again you get a E_0 a W is nothing, but my γ_w D_w ; a north is $\gamma_n D_n$, a S minus $\gamma_s D_s$ and a C is nothing but minus a_W a N plus a_S and b_c would be my $Q_c V_c$ minus summation of faces flux V_f .

So, we have actually looked at a particular stencil when it exposed to the boundary condition or rather different kind of boundary condition starting from Dirichlet boundary condition, Neumann type boundary condition, mixed boundary condition and symmetry boundary condition; they the discretized equation can be obtained and the corresponding coefficients can also be obtained accordingly.

Now, if in all these cases that we have discussed we have applied the condition at the east face. So, if we apply the condition on the other faces then as I have been saying that the respective coefficients will go away and corresponding contribution or equivalent contribution should appear in the source term. So, that actually talks about the application of these boundary condition. So, will stop here and.

Thank you.