

Aircraft Stability and Control
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Lecture-50
Dynamic Stability

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Handwritten notes on a chalkboard:

$$E = g \cos \theta_1 \{ M_x Z_u - Z_x M_u \} + g \sin \theta_1 \left[(M_u) \times \right]$$

Routh Criteria

1. $A, B, C, D, E > 0$ Let us say $\theta_1 = 0$.

$E > 0$

$E = M_x Z_u - Z_x M_u > 0$

In Routh criteria, we can apply to check whether these things are stable or not. One of the conditions is that all the coefficients A, B, C, D, E should be greater than 0. There are other conditions also, we will come. First we take A, B, C, D, E greater than 0, that means when you expand this matrix and put dynamic values, coefficients etc., etc., then you will see what is the value of A, B, C, D, E, one thing we have to ensure that if in the dynamic stable, then all the signs of A, B, C, D, E should be greater than 0.

One of those cases I will take, what do you mean what additional information we get when you say E greater than 0, okay. That is the case now we will be studying, okay. We will talk about little bit of Laplace transform and little bit of oscillatory area in our subsequent Mann Ki Baat session but we have to complete this part. So I am just for time being we will take that Routh criteria, one of the condition is A, B, C, D, E greater than 0 and we are trying to look for the significance of this sort of huge, huge expression, what is the meaning of this expression, how best we can take care of it.

So we are taking a case where $E > 0$ means what. $E > 0$ let's say $\theta_1 = 0$ okay. And we are not considering thrust part, which we not considering you know it can be easily done in similar way. θ_1 is 0 then I have $E = m \ddot{u} - z \ddot{\alpha} m u > 0$. We need to understand if θ_1 is 0 this is 1 and g is always positive, so $e > 0$ means $m \ddot{u} - z \ddot{\alpha} m u > 0$ correct.

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$$M_{\alpha} = \frac{q_1 S \bar{C}_{m\alpha}}{I_{yy}}$$

$$Z_u = -\frac{q_1 S (C_{L\alpha} + C_{D1})}{m}$$

$$Z_{\alpha} = -\frac{q_1 S (C_{L\alpha} + C_{D1})}{m}$$

$$M_u = \frac{q_1 S c (C_{mu} + C_{m1})}{I_{yy} U_1}$$

So this is the condition. Question is what does this tell us? Let's go back what was $m \ddot{\alpha}$. M_{α} was defined as $q_1 S \bar{C}_{m\alpha}$ by I_{yy} and then second term is $z \ddot{u}$, what is this $z \ddot{u}$ expression is $-q_1 S (C_{L\alpha} + C_{D1})$ by m and what is your $z \ddot{\alpha}$ $z \ddot{\alpha}$ is $-q_1 S (C_{L\alpha} + C_{D1})$ by m and what is $m \ddot{u}$. μ is said to be $q_1 S \bar{C}_{mu} + C_{m1}$ into $c m I_{yy} U_1$, right.

So, what is the condition E should be greater than 0 because you know that for Routh criteria you take it for granted at this point that all the coefficient A, B, C, D, E for that equation $s^4 + a s^3 + b s^2 + c s + d = 0$, all the coefficient will be greater than 0. So, we are taking a case where E is greater than 0 that is. I am seeing what does $E > 0$ means to us ok. So now from there we are studying a case where we are saying θ_1 will be 0. What is θ_1 ? θ_1 is the θ at the time of cruise okay.

Now again we will see the expression what the $m_{\alpha} z_u - z_{\alpha} m_u > 0$ which we have already derived and now we will put this here and see what does this finally mean to us okay. So that is lot of involved, it involved lot of code word, so don't get upset.

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The image shows a chalkboard with the following handwritten equations:

$$M_{\alpha} z_u - z_{\alpha} M_u > 0$$

$$\frac{M_{\alpha}}{z_{\alpha}} > \frac{M_u}{z_u}$$

$$\frac{M_{\alpha}}{z_{\alpha}} = \frac{q \bar{S} C_{m\alpha}}{\frac{1}{I_{yy}}} = - \frac{\bar{m} \bar{c} C_{m\alpha}}{I_{yy} (C_{L\alpha} + C_{D1})}$$

$$= \frac{-q \bar{S} (C_{L\alpha} + C_{D1})}{m}$$

So $e > 0$ means we will see that $m_{\alpha} z_u - z_{\alpha} m_u > 0$ that means $m_{\alpha} z_u > z_{\alpha} m_u$. We are seeing that we are trying to understand what additional information relating to stability we are getting through this coefficient. We know for dynamic stability all this A, B, C, D, E should be greater than 0 so you are studying a case for $E > 0$. $e > 0$ means this expression greater than 0.

Which tells $m_{\alpha} z_u > z_{\alpha} m_u$ and now I substitute $m_{\alpha} z_u$ in this expression and then what will happen you see. $M_{\alpha} z_u$ will be nothing but let me write $q \bar{S} C_{m\alpha} / I_{yy}$ that is y that is $m_{\alpha} q \bar{S} C_{m\alpha} / I_{yy}$ $q \bar{S} C_{L\alpha} + C_{D1}$ by m right.

$q \bar{S} C_{L\alpha} + C_{D1}$ by m . if I divide this I get this expression as $- \bar{m} \bar{c} C_{m\alpha} / I_{yy} (C_{L\alpha} + C_{D1})$ ok. So what is the final equation $m_{\alpha} z_u$ is this ok. Similarly we find out what is the second term $m_u z_u$.

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$$\frac{M_u}{Z_u} = \frac{q_1 \bar{s} c (c_{mu} + 2c_{m1})}{\frac{I_{yy} u_1}{-q_1 s (c_{lu} + 2c_{l1})}} \Rightarrow \frac{M_u}{Z_u} = \frac{-m \bar{c} (c_{mu} + 2c_{m1})}{I_{yy} (c_{lu} + 2c_{l1})}$$

$$\frac{-m \bar{c} c_{md}}{I_{yy} (c_{lu} + 2c_{l1})} > \frac{-m \bar{c} (c_{mu} + 2c_{m1})}{(c_{lu} + 2c_{l1}) I_{yy}}$$

so m_u by z_u when I am doing I know the expression of m_u so I put $q_1 \bar{s} c$ by $I_{yy} q_1$ into $c_{mu} + 2c_{m1}$ is divided by $-q_1 s c_{lu} + 2c_{l1}$ by m_u . You could see that we have to substitute the expression for z_u and if z_u here. It is wrongly written so let me correct it and you also correct it should be. Z_u should be $-q_1 s c_{lu} + 2c_{l1}$ divided by m_u ok.

So that was wrongly written please correct it so here it will be $q_1 s c_{lu} + 2c_{l1}$ by m_u . So once I do that I get an expression is m_u by $z_u = -m \bar{c} c_{mu} + 2c_{m1}$ divided by $I_{yy} c_{lu} + 2c_{l1}$ please understand you should do it yourself otherwise there is possible chance to mixed up you know.

Writing this expression not a simple thing is a real challenge you should get de focused ok. So what we are doing. We are trying to extract maximum information from this relationship which has come because of the condition through routh criteria that all the co efficient with that equation A, B, C, D, E should be greater than 0. So let's moving what happen what information when condition e greater than 0.

So from there we have come here now we know this expression one is m_α and z_α we know this and m_u by z_u is this so now we will write like this that $-m \bar{c} c_{m\alpha}$ by $I_{yy} c_{l\alpha} + c_{d1}$. What is this, this is basically are m_α by z_α see $m \bar{c} c_{m\alpha}$ by I_{yy}

if this is simply greater than m_u by z_u with this expression that is $-m_c \bar{c}_m u + 2 c_m l$ divided by $c_l u + 2 c_l l$ into $I y y$.

$c_l u + 2 c_l l$ $I y y m c$. now how do simplify this you know this $c_m l$ is 0 this is at trim this value is 0 or trim. Or trim in cruise this value is 0 so. Now further if I manipulate this expression. we get interesting result and all this efforts were for that if I further simplify this.

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The image shows a chalkboard with handwritten mathematical derivations. At the top left, it says $\frac{\partial \bar{c}_m}{\partial \bar{c}_l} < 0$ V.O.K. and $C_{mu} = M_1 \frac{\partial \bar{c}_m}{\partial M}$. To the right, $\frac{M_u}{Z_u} =$ is written. Below these, the inequality $-\frac{C_{m\alpha}}{(C_{L\alpha} + C_{D1})} > \frac{C_{mu}}{(C_{Lu} + 2C_{L1})}$ is shown. An arrow points from this inequality to a boxed expression $\frac{C_{m\alpha}}{C_{L\alpha}} < \frac{C_{mu}}{(C_{Lu} + 2C_{L1})}$. To the right of the boxed expression, it says $\frac{\partial \bar{c}_m}{\partial \bar{c}_l} = ? < 0$ and $\frac{\partial \bar{c}_m}{\partial \bar{c}_l} < \frac{C_{mu}}{(C_{Lu} + 2C_{L1})}$. At the bottom right, it says "Subsonic case. $C_{mu} = 0$ ".

I will get $-c_m \alpha$ by $c_l \alpha + c_d l$ is greater than $c_m u$ by $-c_m u$ by $c_l u + 2 c_l l$ you could see here this m get cancelled c gets cancelled $I y y$ get cancelled $c_m l$ is 0 so this is nothing but m_u , $c_m u$ ok. So that is what is prevailing here $c_m l$ is of course is 0 now if I say $c_d l$ is less compared to $c_l \alpha$ is very true $c_d l$ could be 0.025 $c_l \alpha$ around 5.5 so it will be good approximation and then what we will get which is as $c_m \alpha$ by $c_l \alpha$ less than $c_m u$ by $c_l u + 2 c_l l$ you could see this sign has changed to less than greater than - - sign by multiply - sign in both sides naturally this becomes less.

What is the meaning for $c_m \alpha$ by $c_l \alpha$ let us understand. What is ratio $c_m \alpha$ by $c_l \alpha$ this is nothing but dcm by dcl right. And what is this, this is you know - static margin so what we are getting from here the dcm by dcl should be less than $c_m u$ by $c_l u + 2 c_l l$ for dynamic stability the condition is dcm by dcl should be less than $c_m u$ by $c_l u + 2 c_l l$.

Now for subsonic case, you know for subsonic case this $c_{mu} = 0$ so naturally we have this condition dcm by dcl less than 0 we are ok with this right. But for supersonic case, c_{mu} will be negative right. You know c_{mu} is negative. Subsonic case c_{mu} is less than 0 that you know because c_{mu} is nothing but m 1 into dcm by $d m$ and what happens as the aircraft goes subsonic increase the speed the center pressure anatomic center of tail goes backward so these tail moment have increases that gives that nose down moment and give tunnel effect right.

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$$\frac{\partial C_m}{\partial C_L} = \frac{C_{mu}}{(C_{L_u} + 2C_{L_1})} = \text{supersonic } C_{mu} = A^*$$

$$\frac{\partial C_m}{\partial C_L} < A^* \quad \underline{A^* < 0} \quad \text{sup, } C_{mu} \neq 0, < 0$$

$$\frac{\partial C_m}{\partial C_L} < 0, \quad C_{mu} = 0$$

So this is negative so dcm by dcl again negative what is the difference in the first case when c_{mu} was 0 dcm by dcl should be negative its ok statically stable. Second case also dcm by dcl less than 0 so this is negative again dcm by dcl less than 0 so there is no violation in the static stability however what is the different let us see that.

So we see here the dcm by $dcl =$ or should be less than c_{mu} by $cl_u + 2cl_1$. We know c_{mu} is negative for supersonic case so dcm by dcl less than 0 is fine but what is let's say this number for supersonic case is A^* I can get the value of c_{mu} and c_{l1} so this is negative that you know so this will be indeed less than 0.

dcm by dcl ok it = A^* well A^* is less than 0 fine, this supersonic case for The subsonic case same it is given dcm by dcl is less than A^* and less than 0 because c_m equal to 0 here c_{mu} not

equal to 0 in fact the less than 0. What is dcm by dcl. dcm by dcl is that you understand let me erase this part.

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$$\frac{\partial C_m}{\partial C_L} = -(\bar{N}_0 - \bar{X}_{CG})$$

$$= \bar{X}_{NP} - \bar{X}_{CG}$$

$$C_{mu} = M_\infty \frac{\partial C_m}{\partial M}$$

Diagram: A horizontal line represents the chord line. A point \bar{X}_{CG} is marked on the left. A point \bar{N} is marked on the right. A double-headed arrow between them is labeled \bar{B} . Below the line, the text "No Sub" is written.

$$\frac{\partial C_m}{\partial C_L} < 0, \text{ it is also to be ensured}$$

$$\frac{\partial C_m}{\partial C_L} < A^*$$

So what is dcm by dcl we have seen dcm by dcl is nothing but - starting margin that is - x or - neutral point - x c g bar or we can write as x c g bar - n not bar. N not is the neutral point. For subsonic case what is just simply telling is that if this is the n not ok. Aircraft will be subsonic right from there what I am saying getting is dcm by dcl should be 0.

That means x could be anywhere as long as it is in this side correct, but for supersonic case what is dcm by dcl when it takes care of dynamic stability also it is not just less than 0 it is also to be ensured that dcm by dcl is less than A star where A star is negative which is given by $c_{mu} \text{ by } c_{lu} + 2c_{ll}$ so that means just putting c g here ahead of n not will not be sufficient we have to ensure that x c g is such that $n \times c g - n \text{ not}$ this separation now will be governed by this should be less than A star that is this distance ok if I said B would be subsonic case this B should be less than A star ok. This part clear.

dcm by dcl should be less than A star here we know that A star is negative this is positive this is positive and this can be neglect very small. This is positive this is negative so this values less than 0 this is fine. So that is what you should be very very clear. But for dynamic stability

supersonic case how c_{mu} which is nothing but $c_{m\alpha}$ plays an important role through the phenomenon called tuck under this speaking supersonic.

A c of the tail goes backward so tail momentum increases and additional nose down moment comes which is known as tuck under effect ok. This is clear. So c_{mu} plays important role which restrict the stability margin to ensure it is also dynamically stable and this will be derived from the condition that E is greater than 0 ok. Which is condition for dynamic stability through Routh criteria ok?

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Handwritten mathematical derivation on a chalkboard:

- Top left: $+DS+E=0$
- Top center: $E > 0$
- Center: $\frac{\partial C_m}{\partial \alpha} < \frac{C_{mu}}{C_{Lu} + 2C_{L1}}$
- Below center: $C_{mu}=0; \Rightarrow \frac{\partial C_m}{\partial \alpha} < 0$
- Below center: but $C_{mu} \neq 0; C_{mu} = M, \frac{\partial C_m}{\partial M} < 0$
- Right side: $A^* = \frac{C_{mu}}{C_{Lu} + 2C_{L1}} = -0.1 (\text{say})$
- Below center: $\frac{\partial C_m}{\partial \alpha} < A^*$
- Bottom center (boxed): $\frac{\partial C_m}{\partial \alpha} < -0.1$ with a double-headed arrow pointing to the right.

So we try to revisit this E greater than 0 this condition which is came from the characteristic equation $A s^4 + b s^3 + c s^2 + d s + e = 0$ and you know from last criteria one of the conditions satisfies all this co efficient greater than 0 and there are other condition that will come and by using this condition one case E greater than 0 what does it mean and we got the relationship wonderful relationship.

$\frac{d c_m}{d \alpha} < \frac{c_{mu}}{c_{Lu} + 2 c_{L1}}$ ok and you know from this relationship it realize that if $c_{mu} = 0$ this implies simply $\frac{d c_m}{d \alpha} < 0$ which is very familiar with the slope of c_m by $d \alpha$ at equilibrium simply as a 0.

But high speed c_{mu} is not equal to 0 then what, then at high speed c_{mu} you know is nothing but $m \dot{d}c_m$ by $d m$ and which is less than 0 then this condition says $d c_m$ by $d c_l$ should be less than A_{star} but what is A_{star} . A_{star} is nothing but c_{mu} by $c_{lu} + 2c_{l1}$ typically let us say this value ok let say - point 1. c_{mu} is negative ok if this is - .1 for sake this is an example telling to understand this that means the condition is just not $d c_m$ by $d c_l$ less than 0 the condition is $d c_m$ by $d c_l$.

Yes indeed less than 0 but should be less than point 1 that is the modified condition on undertaking dynamic stability also into account so the location neutral point and c_g because this is extremely important it has to satisfy this condition as well. Which includes the condition that $d c_m$ by $d c_l$ is less than 0 but $d c_m$ by $d c_l$ is less than this value says for example we have taken - .1? This should be understood very carefully ok.

Why this is important because we have taking care of fact that I know as speed increases a c of the tail goes backward and the tuck under phenomenon ok. And then this is one another way to be friendly with big big equation is we see that what finally this expressions are meant for us. Let's take one example let's say for the flying jet airplane all those derivative were computed and after solving we found that value of A, B, C, D, E which are dependent upon the geometric and aerodynamic coefficient or derivatives.

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$$AS^4 + BS^3 + CS^2 + DS + E = 0$$

$A = 675.9$
 $B = 1371$
 $C = 5459$
 $D = 86.3$
 $E = 44.78$

$\lambda_{1,2} = -1.008 \pm j(2.651)$
 $\lambda_{3,4} = -0.0069 \pm j(0.0905)$

$\omega_{n3,4} = 0.091 \text{ rad/s}$
 $\zeta = 0.076$

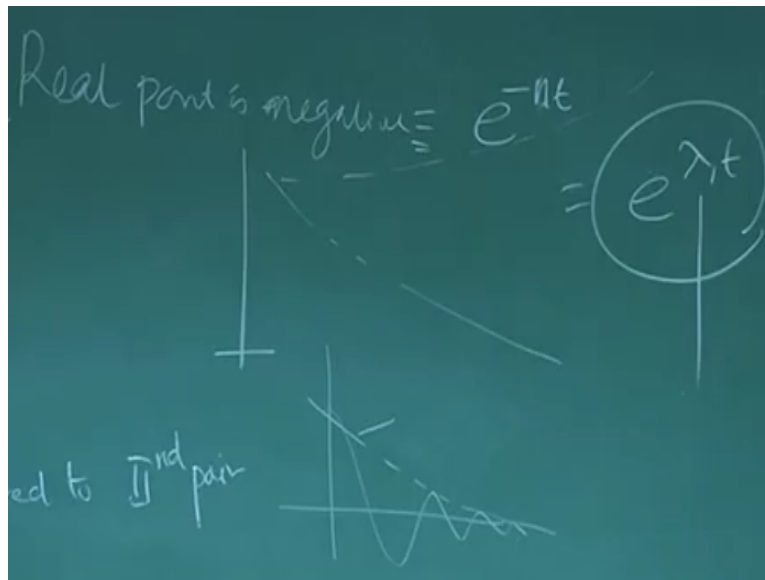
1st pair: Real Negative; large
 $\omega_n = 2$
 $\zeta = 0$

Lets us see the A value, A is 675.9, B is 1371 and c is 5459 and D is 86.3 and E is 44.78 and let us see the all efficient unit. At this point let us talk about the signs and all. You could see A, B, C, D, E all are greater than 0. One of the conditions for Routh criteria for its stability is satisfied ok. Now If I can solve this equation, and I can find out the roots so numerical methods which is possible. Let's see that has been done and the roots are lambda 1, 2 roots are $-1.008 + j$ as complex 2.651 and another pair of roots 3, 4 which is $-0.0069 \text{ plus } -j, j \text{ small } j .0905$.

Typically if I most case of jet airplane if you get the co efficient that have solve this equation will find it will get segregate that into one pair here one pair here so two second order system behavior then the beauty of longitudinal dynamics find in most of the airplane response or its response will have two types of excitation one thing is that they are having the complex parameter in oscillatory response ok for stable system.

So oscillatory response that is why this is complex here or here but what is the difference you see in first pair you can find real root. First pair ok this typically we can see in most of the airplane. First pair in real negative and it is very large compared to the second pair. Large compared to second pair. You could see here this is -1.008 here -0.0069 .

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What does this real root does, real value of this root does you know that this L is the real part is negative that means it means it difficulty form of E to the power $-t/n$ right. It will put envelop for decaying the amplitude will go on decaying. If the real root is positive then it will go on growing in root will be go on going in because this is typically e to the power λt . If λ is negative the real part is negative which is here both are negative both are trying to cut down the amplitude and it is oscillatory also so if you see the root typically root like.

So this envelop will be governed by the real negative root and where ever this root is last negative they will decay fast compared to the smaller one here so I could see here there are two more excited where one is decaying very fast another is taking long time taking long period. This is long period and this is short period mode short period mode. Both are being like a second order system both this mode right.

Now come back to the airplane what happen if the airplane is moving like this we give this disturbance. In one way it is get excited is that is like this and call that two equilibrium other is other could be goes like doing like this and finally come back. Second one this one is nothing but nothing but longer period this real root is smaller negative. First one this one is short period is this one. So we will characterize this λ_1 λ_2 at short period root and this as long period root or we also says phugoid roots.

We will discuss about short period mode and phugoid mode in detail but just see in the beautiful equation also use ugly root expression in formatives. Now how do I handle what information more I should extract from this, if it is second order system? What I look for is natural frequency I look for damping ratio. Let us see if I can use this equation short period natural frequency and long period natural frequency and damping ratio let's do that.

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The image shows a chalkboard with handwritten mathematical work. At the top, the identity $(a+ib)(a-ib) = a^2 - (ib)^2 = a^2 + b^2$ is written. Below this, a characteristic equation is derived from two roots: $s^2 - (\text{Sum of the roots})s + \text{Product of the roots} = 0$. The roots are identified as $\lambda_{1,2} = -1.008 \pm j(2.651)$. The sum of the roots is -2.016 and the product is $(-1.008)^2 + (2.651)^2 = 7.036$. The characteristic equation is then written as $s^2 + 2.016s + 7.036 = 0$. This is compared to the standard second-order form $s^2 + 2\xi\omega_n s + \omega_n^2 = 0$. From this comparison, the natural frequency $\omega_n = 2.836 \text{ rad/s}$ and the damping ratio $\xi = 0.355$ are determined.

If I take this since I have seen this is at typical second order response so I write this as characteristic equation as $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$ you know this is typically second order characteristic equation in terms of ω_n and ζ and so I construct this equation from this root this form. So I write $s^2 - \text{sum of the roots into } s + \text{product of the root equal to } 0$.

So if I take this first equation first root for $\lambda_{1,2}$ this equation becomes $s^2 - \text{sum of the roots will be what } -1.008 + j 2.651$ This $+$ $-$ is 2.651 ok this is one root $+$ again $+$ $-1.008 + -$ now $j 2.651$ ok this becomes sum of the roots. First root is I miss that the $-$ sign here $+$ $-$ complex sphere complex sphere so what we note is $-1.008 + j 2.651$. Second root is $-1.008 - 2.651$ into sum of the root into $s + \text{product of the root you know how to find out product of the root}$.

So this will be $-1.008 + j 2.651$ into $-1.008 - j 2.651$ and that equal to 0 if you do like this you will get this equation in this forms $s^2 - \text{sum of the root } + \text{product of the root when we}$

compare it with this equation and you will get $s^2 - 2\zeta\omega_n s + \omega_n^2 = 0$ and this get added so this becomes $+ 2\zeta\omega_n s$ into 1.008 then $+ \text{product of the root}$ so that will be $- 1.008 + 2.651j$ ok into $- 1.008 - 2.651j$ which should be equal to 0. This is nothing but $a + b$ into $a - b$ so you will get equation where 2 into these into s will be there put s here let's erase this. $S +$

So I know I compare this with this equation $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$ for $2\zeta\omega_n$ I will write this equal to this compare this and ω_n^2 square I compare with this product should be typically will be $- 1$ point $A + b$ into $a - b$ so $a^2 - b^2$ and j is there become $a^2 + b^2$ little bit typically where not mistaken this value will be $- 1.008$ whole square $+ 2.651$ square so $a + b$ into a .

$A + j b$ $a - j b$ equal to $a^2 - j b$ whole square equal to $a^2 + b^2$ so you can see that this will be this product will be a^2 that is $- 1.008 + b^2$ square is 2.651 this square this will be equal to 0 so I compare ω_n^2 square equal to this term and $2\zeta\omega_n$ equal to this term and by solving that I will get ω_n equal to 2.836 radian per second and ζ I will get around 0.355 this is clear how to do it.

You could see I could use this equation and find out the roots similarly for this also I can find out in similar way and you are supposed to do it and find that ω_n 3,4 will be equal to 0.091 radian per second and ζ equal to 0.076 .

And you could see that gets for first one is very high compared to second one that is why second one is the phugoid mode long period mode it goes on doing like this. Goes on converting kinetic potential energy among each other and then it process and that equilibrium. First one is simply like this that's why ζ is 0.355 compared to 0.076 same thing deflected in ω_n this is much larger in short period then ω_n is for phugoid this you must do one exercise yourself and this is very straight forward thing.

We will solve one or two example for this so that it was handy this lecture was meant to be give an idea how to handle this big big equation and find some value and number here today I will

end in next class I will start from here another example so that you will get familiar to what we have been.

Thank you.