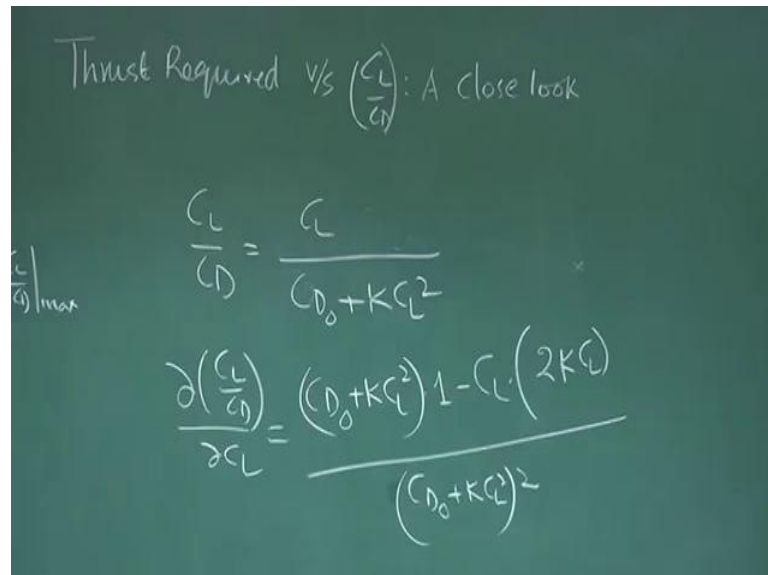


NOC: Introduction to Airplane Performance
Prof. A. K. Ghosh
Department of Aerospace Engineering
Indian Institute of Technology, Kanpur

Lecture - 14
Thrust Required: A Closer Look

Good morning friends, we have been talking about Thrust required, Power required. We have talked about for thrust required C_L by C_D should be maximum, for power required $C_L^{3/2}$ by C_D should be maximum. Now, by now aware, what will be the speed? I will be going little one step ahead in understanding, what is the meaning of thrust required minimum via C_L by C_D maximum.

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Thrust Required vs $\left(\frac{C_L}{C_D}\right)$: A close look

$$\frac{C_L}{C_D} = \frac{C_L}{C_{D0} + K C_L^2}$$

$$\frac{\partial \left(\frac{C_L}{C_D}\right)}{\partial C_L} = \frac{(C_{D0} + K C_L^2) - C_L(2K C_L)}{(C_{D0} + K C_L^2)^2}$$

So, this is thrust required versus C_L by C_D a closer look. Let us see, we are very comfortable writing this C_L by C_D and this means, thrust required minimum implies, I must fly at C_L by C_D maximum. Let us do little bit of algebra or some sort of a little mathematical insight into this C_L by C_D max. See, you know C_D is C_{D0} plus $K C_L^2$ and we know that, this is parasite drag and $K C_L^2$ is the induced drag, all these things are very clear to us.

Now, if I ask a question, what is that, that C_L I should fly, so that, C_L by C_D is maximum. If I want to find out mathematically, I can follow this few steps and get an answer. This I will write C_L by C_D as C_L by C_{D0} plus $K C_L^2$ and I will

differentiate this C_L by C_D by C_L and if I do that, I find C_D naught plus $K C_L$ square into 1 minus C_L into $2 K C_L$ divided by C_D naught plus $K C_L$ square, whole square.

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$$C_D = C_{D0} + K C_L^2$$

What is that $C_L \Rightarrow \left. \frac{C_L}{C_D} \right|_{\max}$

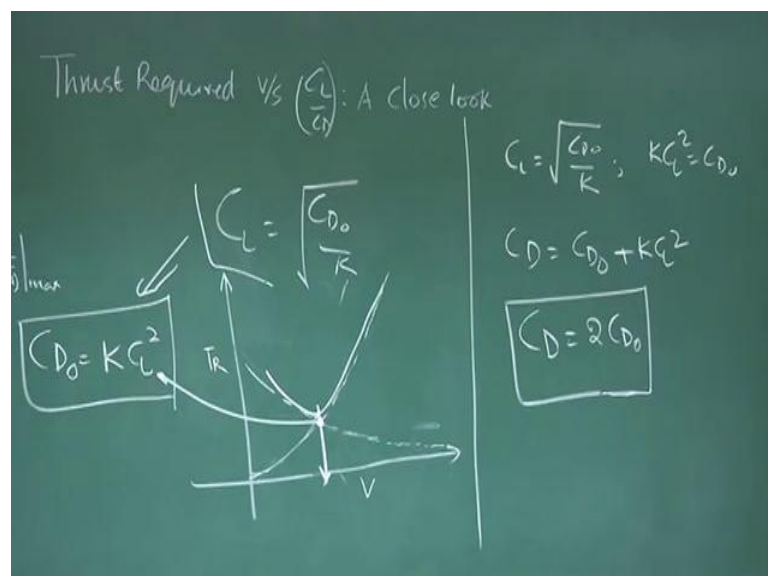
$$\frac{d(C_L/C_D)}{dC_L} = 0$$

$$C_{D0} + K C_L^2 - 2 K C_L^2 = 0$$

$$\Rightarrow C_L = \sqrt{\frac{C_{D0}}{K}}$$

Now, next step is, I find the turning point, so I put this equal to 0. If I put $d C_L$ by C_D by C_L equal to 0, then I get an expression C_D naught plus $K C_L$ square minus $2 K C_L$ square equal to 0 or I get the popular expression C_L equal to under root C_D naught by K . As simple as that, you can check the second derivative to see if it is indeed a coordination of maxima; the second derivative should be less than 0.

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Now, the interpretation demands C_L equal to C_{D0} by K , when I write like this, you know once I solve this what did I get, I get C_{D0} equal to $K C_L^2$. How do I give an interpretation? Let us draw thrust required versus speed and we by now know that, this is the induced drag or induced thrust component and another was parasite and this was the net thrust required. And this was the point where thrust required was minimum and thrust required was minimum as far we understand, this is the point corresponds to C_L by C_D maximum.

But, from this analysis or this one, what did I get that is the point where the parasite drag equal to induced drag, this is in terms of coefficient. So, I call C_{D0} equal to $K C_L^2$ square and you could see that, this is indeed the point of intersection of parasite and induced drag. So, this point and this point are same point. So, we are now trying to add little bit of mathematical value to our understanding.

Second thing, so if I am flying at C_L equal to C_{D0} by K ; that means, what is the C_D of flying actually, I know C_D equal to C_{D0} plus $K C_L^2$ square. Since, at this point C_L is nothing but, C_{D0} by K or $K C_L^2$ square is nothing but, C_{D0} . So, my overall C_D becomes twice C_{D0} , this is very important. So, you can understand, if we are flying at thrust required minimum; that means the airplane designer should ensure that C_{D0} should be as low as possible.

That means, it calls for aerodynamics to work more and make sure the drag component at α equal to 0, which is C_{D0} or C_D at C_L equal to 0, C_{D0} should be as low as possible. It should have a lesser skin friction drag, less lesser pressure drag and that is what is important for our interpretations; that one should be very, very careful and translate this to designers mind.

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Required $v/s \left(\frac{C_L}{C_D} \right)$: A close look

A/c. $AR=20$
 $e=1$
 $(C_D)=0.020$

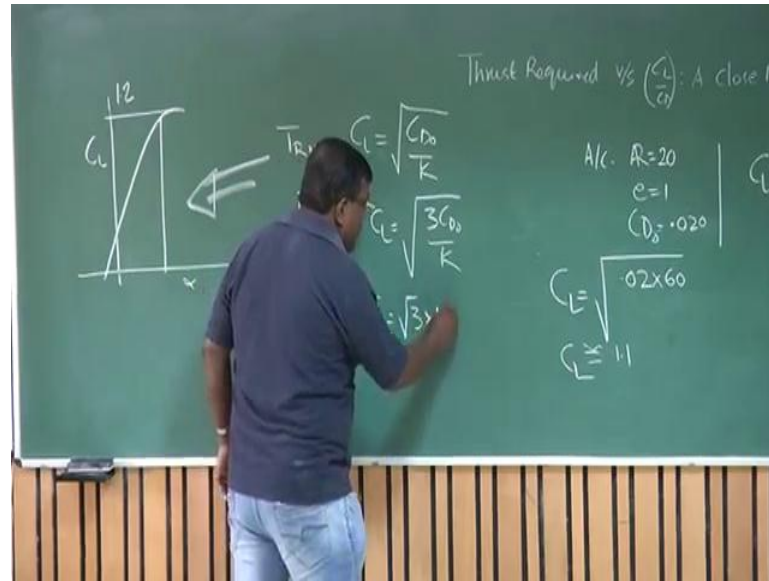
$C_L = \sqrt{\frac{C_D}{K}} = \sqrt{\frac{0.02}{K}}$
 $K = \frac{1}{\pi AR e} = \frac{1}{\pi \times 20 \times 1} \approx \frac{1}{60}$

Now, the second part we will see, seeing for flying with thrust required minimum, we have this flying with power required minimum, we have already seen that, it is $3 C_D$ naught by K . Let us take an example, let us take an airplane, whose aspect ratio is let us say 20, large aspect ratio like a glider and large aspect ratio, why we are tempted to a large aspect ratio. Because, if we are thinking one dimensional that induced drag should be low, induced drag should be low, then one of the option is make the aspect as high as possible.

So, it is aspect ratio is 20 and let us take e is 1, let us say elliptic distribution and C_D naught realistic value, I will take as 0.20, which is little oversight, but a good airplane will have this range of C_D naught. If this is the data I have or what does this mean as far a C_L is concerned, C_L is C_D naught by K ; that is for thrust required minimum. So, that will be 0.02 divided by K . What is the value of K ? K is 1 by π aspect ratio e and that is 1 by π into 20 and into 1, I have taken the value of e assuming perfect elliptic distribution.

So, K is roughly equal to 1 by 60, the approximation with π I have taken just 3, not 3.1416. So, if I put that value of K in this expression, what the C_L I get, this 0.02 into 60 and that is, if I calculate, it will be around 1.1, because this is around 1.2, under root of 1.2, 1.1. So, what is the message, message is, if I want to fly at thrust required minimum, the C_L should be 1.1.

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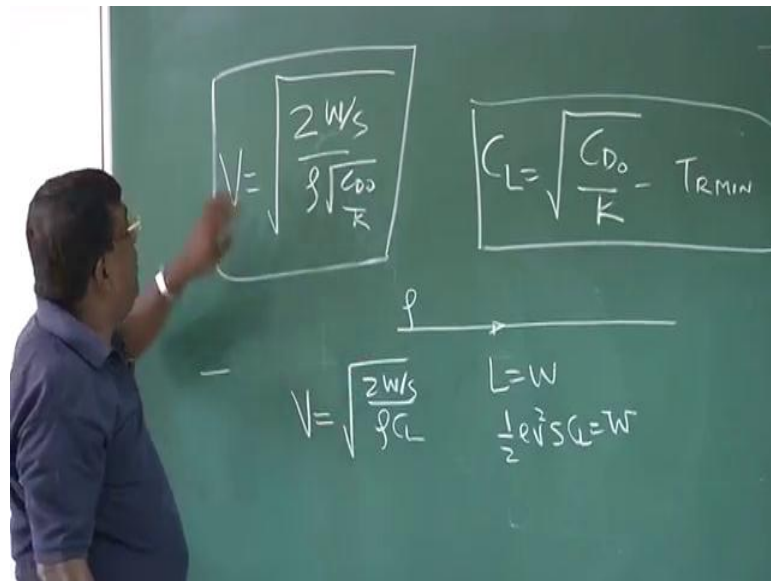


Now, the moment C_L is 1.1, I get an alarm, I immediately see, what is the C_L versus alpha for my aircraft and we know that, this maximum value is for normal case without any high level devices, etcetera. This value is typically for most of the business aircraft of six seaters, seven seaters, eight seaters, they are around 1.2. Even, without any high lift devices most of the airplane will have C_L maximum value of around 1.2.

Now, you are demanding the pilot to fly at C_L 1.1, see the problem slight, already he is operating somewhere here. So, he is near this region. So, just putting up a condition that C_L you need 1.1 is not sufficient. So, your design should ensure that, whatever C_L you are demanding to get thrust required minimum, it should be consistent with this back of mind, are you able to get this understanding.

Because, you see the seriousness, if I want to fly at C_L power required minimum, then this C_L value will be furthermore root 3 times 1.1, where from you will get that C_L from normal aircraft. So, the question come, should we go for aspect ratio 20, although induced drag was reducing, but there are so many other issues. So, as a designer you have to be multidimensional, you cannot go on giving maximum vortex to only one parameter; that is why I wanted to share this experience with you.

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We should also be careful to know, what are the other salient features, which is to be known before I talk about fly at C_D naught by K , etcetera, this is for thrust required minimum. This is fine that you need to fly at C_L equal to C_D naught by K to ensure thrust required minimum, know what is contesting. But, what is our main purpose? Main purpose is, I want to fly at a particular altitude. Let say that altitude is ρ , I am talking about density.

My purpose is, I have to ensure that lift equal to weight; that is I have to ensure that half ρv square $S C_L$ is equal to weight and that means, I need to fly at $2W$ by S by ρC_L and this C_L is nothing but, dictated by this for thrust required minimum. So, this is $2W$ by S , ρC_D naught by K . Now, see interesting part, if we are flying at a particular altitude, the velocity should be this much.

To ensure that thrust required is minimum, when you are flying means you are cruising at altitude where density is ρ , but this will give some value of V . Now, where from I will get the V , the moment there is the V , I know that I need to have an engine, which should be able to give me enough power or thrust to generate that V . That is thrust equal to half ρv square $S C_D$, I need to have enough thrust, so that I get this much of V , because as the V is increased or for a particular V , this airplane will experience a drag.

So, I have to ensure that, I have my engine is enough powerful to give that much of thrust. So, there again I go back to the engine site, whether really this velocity is

achievable or not. If it is achievable fine, if it is not, then I will be, if we want to reduce this V , I will try to play around with the wing loading W by S , I will try to reduce the wing loading.

And that is how this iteration will go on happening and finally, you get a configuration, where you are giving enough bandwidth to your pilot, so that, he can get those solution by looking at the instrument getting those numbers in their plate to that conditions. Because, if your design does not have those conditions, which can be expected by a pilot, then he will not be able to fly at that conditions. So, it is a primary role of a designer to make sure, you have given all those solution in the design itself and the pilot starts gaining into those domain and try to fly the way it should be flown.