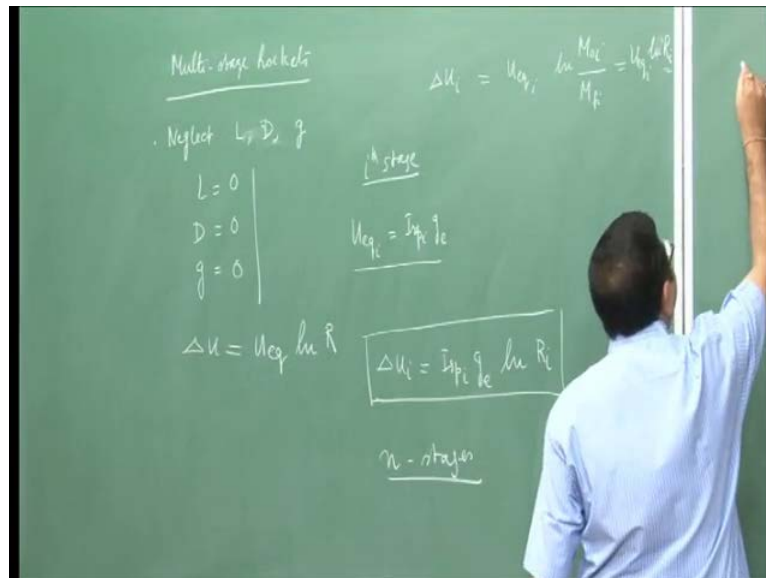


Jet and Rocket Propulsion
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Lecture - 11

Welcome back. So in the last lecture, we started discussing Multi-stage rockets, we have discussed the nomenclature that we used to represent the performance of multi stage rockets. We have also discussed that why do we need multi stage rockets, what are the performance improvements that we can gain by going from a single stage to a multi stage design.

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Next, what we will do now is to talk about the performance, we will derive the expressions which represent the performance of a multi stage rocket. Before we do that first let us make the assumptions that we will be talking about, we will be neglecting the lift, neglecting the drag and neglecting the gravity that is L is equal to 0, D is equal to 0, g is equal to 0.

Now, as for the last few lectures we have been talking about these assumptions. First of all, lift as we have seen typically works perpendicular to the flight path. So, if lift is non zero, the vehicle will start to deviate from the intended path sight path, therefore we always like to have lift to be 0, because these are non lifting vehicles. So, therefore, this is not an assumption is actually a practical reality. Coming to the drag, on the ground

or close to the ground, because the atmosphere is very, very dense we will have some drag.

But the point is that the rocket vehicles, travel extreme distances and as we go up high in the altitude the densities falls rapidly. So therefore, as we go high and high, the density will drop, therefore the drag is also going to go down. So, essentially the drag although towards the beginning in the booster stage is important, as we go further up out towards the edge of the atmosphere drag becomes a very small amount and in the outside the atmosphere, drag is practically 0.

Therefore neglecting drag also is something that is reasonable assumption and coming to the gravity, well gravity is going to be there, but the effect of the gravity, once we go to outer space is not very large. But, as when we come to space dynamics we can see that all our mission is actually dictated by gravity. Gravitational force is the most important parameter in rocket propulsion, so gravity is going to there, but the magnitude is not going to be very large.

So, for practical applications when initial design, let me put it this way the initial design when we are designing the rocket initially for a given mission, we can safely neglect the effect of gravity as well. And by neglecting particular drag and gravity our rocket dynamic equation, which is a differential equation becomes independent of time; therefore, we do not have to integrate over time, to get the velocity increment.

Therefore, neglecting gravity and drag actually simplifies our calculation and then as we have seen for the single stage rockets, the velocity increment, becomes a function of equivalent velocity and the mass inverse of mass ratio R . Now, this was the starting that we have proven for the single stage rocket.

Now the same thing now can be applicable to a multi stage rocket, so if I write the same equation for a Multi-stage rocket, I will write it like this $\Delta u_i = u_{eq,i} \ln \frac{M_{f,i}}{M_{i,i}}$, which is essentially equal to $u_{eq,i} \ln R_i$. Here, i represents the i th stage of a multi stage rocket, we have discussed the nomenclature in the previous lecture, that we have n number of stages.

Every stages is designated by subscript i can be 1, 2, 3 up to n depending on the number of stages. So, this is the expression for the velocity increment under these assumptions

for the i th stage. So, Δu_i then is the velocity increment for the i th stage, that is the difference of velocity at the end of burning for the i th stage minus the difference in velocity at the end of burning for $i - 1$ th stage or the previous stage.

So, previous stage burns, it leaves the vehicle with certain velocity, and then the i th stage takes over from there, and gives an increment, so that increment is given here by Δu_i , $u_{\text{equivalent } i}$ represents the equivalent velocity for the i th stage. So, that depends on the specific impulse, so I can write it here, as $u_{\text{equivalent } i}$ is $i \text{ spi to } g_e$. Where, $i \text{ spi}$ is the specific impulse for the i th stage and g_e is the acceleration due to gravity at sea level, this is something that is important this is g_e is all sea level.

Only in the gravity term, if we consider then that appears as g , so then with altitude it varies, but here it is only at the sea level. So, the equivalent velocity for i th stage is given like this, and then the mass ratio inverse of mass ratio R , R_i is $M_{\text{dot } i}$ by $M_{\text{dot } f}$, that is the initial mass of the i th stage divided by the final mass of the i th stage. We have defined all these parameters in the last lecture. Now, with this then if I put it back into this equation I get Δu_i equal to $I_{\text{spi}} g_e \ln R_i$, this is my expression for velocity increment for the i th stage of a multi stage rocket.

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The image shows a green chalkboard with handwritten mathematical derivations. On the left, a list of velocity increments $\Delta u_1, \Delta u_2, \dots, \Delta u_n$ is summed to give $\Delta u = \sum_{i=1}^n \Delta u_i$. The main derivation shows $\Delta u = \sum_{i=1}^n \Delta u_i = \sum_{i=1}^n I_{\text{spi}} g_e \ln(R_i)$. It then defines the mass ratio $R_i = \frac{M_{0i}}{M_{fi}}$ and the lambda term $\lambda_i = \frac{M_L}{M_{0i} - M_{fi}}$. The total mass ratio is given as $R = \frac{1 + \lambda}{\lambda + \epsilon}$ and $R_i = \frac{1 + \lambda_i}{\lambda_i + \epsilon_i}$. Finally, the lambda term is expressed as $\lambda_n = \frac{M_L}{M_{0n} - M_L}$.

So, now if I have n stages, then what is happening is this the rocket let us say is starting from 0 velocity. At the end of first stage, it gains a velocity Δu_i Δu_1 , end of

second stage it gains a velocity Δu_2 , like that so to the end the n th stage, after the burning of n th stage it gains the velocity given by Δu_n .

So, therefore the overall increase in velocity is nothing but, the summation of the velocity increment for all the stages, so the overall Δu is nothing but, $\sum \Delta u_i$, i going from 1 to n . So, therefore the overall gain in velocity for n stage rocket is the sum of the gain in velocity in individual stages, so that is given as like this. So, therefore let me write the overall Δu now, in terms of this is equal to $\sum_{i=1}^n \Delta u_i$, and my Δu_i is this term. So, this is equal to $\sum_{i=1}^n I_{sp} g_e \ln R_i$, that is the expression for overall velocity increment for a multi stage rocket.

Now, as we have been seeing so far, the parameters that are known, sometime the structural weight will be known, such time the propellant mass will be known, sometime the payload mass will be known, so there are different things that are known parameters. So therefore, although this is the governing equation, we may need to write it in different forms.

Secondly, when we come to optimization we will see, that we will optimize let us say with respect to the payload fraction of different stages, or let us say with respect to the structural coefficient of different stages. So, therefore for those cases then this equation have to be written, in terms of those variables, let us say payload factors structural coefficient etcetera.

So, what we will do next is this is our basic equation for velocity increment, we will just rewrite it this equation, in terms of the other defined parameter that we have defined. What are the parameters we have defined, we have defined λ , we have defined ϵ , we have defined L etcetera, so we will try to express this, in terms of this parameters.

So now, let us look at this term R_i , as we know that this is the inverse of our mass fraction or mass ratio, so this now R_i , we will represent in terms of this parameters, λ , ϵ and L , because these are our optimization parameters. So first of all, let us look at back at R , we have seen that R is equal to $1 + \lambda$ upon $1 + \lambda + \epsilon$, now this is for a single stage rocket.

So therefore, for every stage of a Multi-stage rocket also this expression is valid, so we can write R_i equal to $1 + \lambda_i + \epsilon_i$, where R_i is this term inverse of the mass fraction for mass ratio for the i th stage. λ_i is the payload factor for the i th stage, and ϵ_i is the structural coefficient for the i th stage.

So, then going back to our definition of payload factor, how did we define the payload factor? Payload factor is the payload mass divided by initial mass minus the payload mass that is, all the mass except the payload. So, we had defined this as, M_L upon M_L minus M_L , M_{naught} minus M_L that is our definition of payload factor.

Now, if we use this definition for the i th stage of a Multi-stage rocket, then we will write it as $\lambda_i M_{L_i}$ upon M_{naught_i} minus M_{L_i} , now comes the interesting part. So, this is the payload factor for the i th stage which is the payload for the i th stage divided by initial mass for the i th stage, minus the payload for the i th stage.

Now, from our discussion in the previous lecture, what is the payload mass for the i th stage as we have discussed in the last lecture, this is the total mass of the $i + 1$ th stage, because this is something the i th stage delivers. So, therefore, this M_{L_i} is the total mass or initial mass, for the $i + 1$ th stage that is the next stage, next upper stage.

Then, λ_i we can write as $M_{dot_i + 1}$ divided by M_{dot_i} minus $M_{naught_i + 1}$. So, the payload factor for the i th stage is the initial mass for the $i + 1$ th stage divided by the initial mass of the i th stage minus the initial mass for the $i + 1$ th stage. So, therefore, this will be defined only up to $n - 1$, because for the $n - 1$ th stage this is M_L , but if i put it as n th stage sorry, it can be defined up to n th stage for the n th stage, this is the overall payload M_L .

So, for the n th stage λ_n is equal to overall payload M_L divided by the initial mass for the n th stage minus the overall payload, so the payload factor for the n th stage is given like this. Next let us look at the structural coefficient, now so far again the structural coefficient we have defined for a single stage. Now, when we come to the multi stage, then we define the structural coefficient for every individual stage.

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Handwritten equations on a green chalkboard:

$$\epsilon = \frac{M_s}{M_s + M_p}$$

$$M_0 = M_s + M_p + M_L$$

$$\Rightarrow M_s + M_p = M_0 - M_L$$

$$\epsilon = \frac{M_s}{M_0 - M_L}$$

$$\epsilon_i = \frac{M_{s_i}}{M_{0_i} - M_{L_i}}$$

$$l = \frac{M_L}{M_0}$$

$$l_i = \frac{M_{L_i}}{M_{0_i}} = \frac{M_{0_{i+1}}}{M_{0_i}}$$

Labels: $R_i, \lambda_i, \epsilon_i, l_i$

Labels: $M_{0_i}, M_{0_{i+1}}, M_{s_i}$

So, next let us define the structural coefficient, structural coefficient for a single stage rocket was defined as the structural mass of the rocket divided by the structural mass and the propellant mass, that was our definition of structural coefficient. Now, we know that the overall mass is the sum of structural mass plus propellant mass plus the payload mass, therefore the sum of structural mass and propellant mass is the initial mass minus the payload mass.

So, if I put it back into this equation, my structural coefficient is equal to M_s upon M_0 minus M_L , this is for a single stage rocket. Now, we use the same definition for a multi stage rocket, so we define the structural coefficient for the i th stage of a multi stage rocket. So, that will be given by the subscript i , which is equal to M_{s_i} divided by now M_0 becomes M_{0_i} minus M_{L_i} , where M_{s_i} is the structural mass of the i th stage, M_{0_i} is the overall mass or initial mass of the i th stage, M_{L_i} is the propellant mass, the payload mass for the i th stage.

Once again going back to the discussion here, the payload mass for the i th stage is the initial mass for the $i+1$ th stage, so therefore, this is equal to $M_{0_{i+1}}$, M_{0_i} minus $M_{0_{i+1}}$, so this is the definition of then structural coefficient for the i th stage. Next let us define l , l is our propellant payload mass fraction, so payload mass fraction, we had define this as M_L upon M_0 for the single stage rocket. This is payload

mass fraction, this is the fraction of payload mass with respect to the overall mass, this is payload factor, λ is payload factor these two are different.

So, as you can see here, λ is defined as the payload mass divided by all the mass except the payload, payload mass fraction is the fraction of payload in total mass. So, λ and L are two different parameters, so λ is called payload mass factor, this is called payload factor, this is payload mass fraction. Now, so coming back to this L is M_L upon M_{naught} , so the payload mass divided by the total mass, this is for a single stage rocket.

So, once again if I use this definition for a multi stage rocket, then i represent this as L_i , so L_i equal to M_{L_i} upon M_{naught_i} , and once again L_i M_{L_i} is equal to M_{naught_i} plus 1, that is the payload mass for the i th stage is the initial mass for the i plus 1 th stage. So, this can be written as M_{naught} .

So now, if I re recap what we have done, so far is we have defined R_i for a multi stage rocket, we have defined λ_i for a multi stage rocket, we have defined ϵ_i for a multi stage rocket and L_i these are the four parameters we have defined so far in this lecture. And, we have defined most of them as functions of M_{naught_i} , M_{naught_i} plus 1 and M_{s_i} see these are the three masses that has been used.

So, we have defined the this four parameters for multi stage i th stage for single stage for a multi stage rocket, in terms of these three masses. The structural mass of the i th stage, the initial mass of the i th stage and the initial mass of the i plus 1 th stage based on this we have defined now, all these parameters.

Let us, now take a further step and write one more relationship here we have one relationship relating R λ i and ϵ i , in the last class we also derived one relationship relating R L and ϵ . So, let me first write that expression for a single stage rocket, then I will write that for a multi stage rocket.

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The chalkboard shows the following derivations:

$$R_i = \frac{1}{\lambda_i(1-\epsilon_i) + \epsilon_i} = \frac{1 + \lambda_i \epsilon_i}{\lambda_i + \epsilon_i}$$

$$\Delta u = \sum_{i=1}^n \Delta u_i = \sum_{i=1}^n u_{eq_i} \ln R_i$$

$$\Delta u = \sum_{i=1}^n I_{sp_i} g_e \ln R_i \quad \text{--- (1)}$$

$$\Delta u = \sum_{i=1}^n I_{sp_i} g_e \ln \left(\frac{1}{\lambda_i(1-\epsilon_i) + \epsilon_i} \right) \quad \text{--- (2)}$$

$$\Delta u = \sum_{i=1}^n I_{sp_i} g_e \ln \left(\frac{1 + \lambda_i \epsilon_i}{\lambda_i + \epsilon_i} \right) \quad \text{--- (3)}$$

For a single stage rocket, in the last class we have derived this expression that R equal to L , 1 minus ϵ plus ϵ , this is one expression we had derived in the last class for a single stage rocket. Now, if I use it for a multi stage rocket, then for the R th, i th stage I can write R_i equal to 1 upon $1 + 1$ minus ϵ_i plus ϵ_i . Now, if I take this expression, and then go back now to our expression for Δu , and this is one another expression was 1 plus λ_i upon λ_i plus ϵ_i , these are the two relationship that we had.

Now, go back to our expression for Δu for the multi stage rocket, we have shown that the overall velocity increment is the algebraic sum of the velocity increment of the n stages. So, this was equal to $\sum_{i=1}^n \Delta u_i$, and Δu_i is equal to $u_{eq_i} \ln R_i$, and then u_{eq_i} is equal to $I_{sp_i} g_e$. So, I can write it as $I_{sp_i} g_e \ln R_i$, so this is one expression let me write it as equation 1.

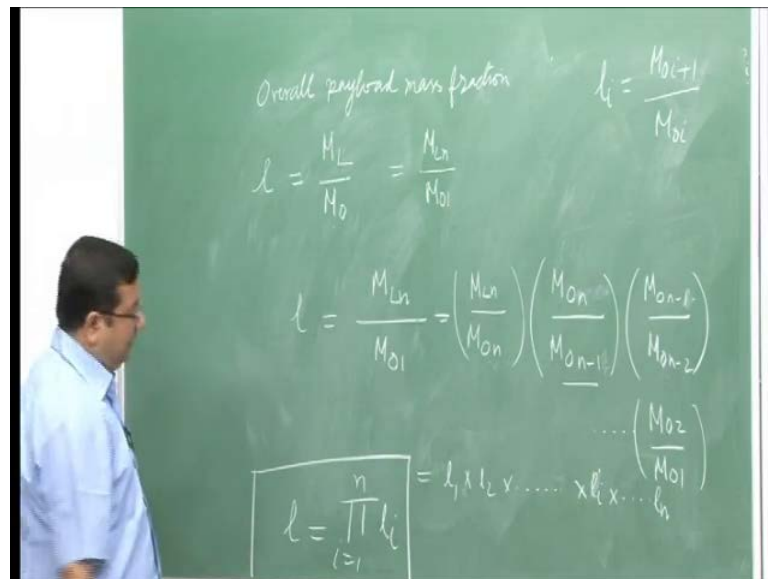
Now, we can replace R_i by this, so in the same equation now, we can replace R_i by either this expression in terms of $1 + 1$ minus ϵ_i plus ϵ_i or we can replace it in terms of λ_i plus ϵ_i upon $1 + \lambda_i \epsilon_i$. So, therefore, I can get another expression for Δu , which will be equal to $\sum_{i=1}^n I_{sp_i} g_e \ln \left(\frac{1}{\lambda_i(1-\epsilon_i) + \epsilon_i} \right)$, if I replace R_i by this then is equal to $1 + 1$ minus ϵ_i plus ϵ_i , let me call this equation 2.

So, here in this what we have done is, we have replaced R_i by this expression for $1 + 1$ minus ϵ_i plus ϵ_i or we can also replace R_i , by this expression in terms of λ_i plus ϵ_i upon $1 + \lambda_i \epsilon_i$.

So, this can be written as $l_i = \frac{M_{i+1}}{M_i}$, instead of R_i we can write $1 + \lambda_i$ upon $1 + \epsilon_i$, let me call this equation 3.

So, these three equations that I have written here are actually same, only thing is that different representation of the various parameters, depending on what are given to us, we can either estimate R or l_i or ϵ_i or λ_i , then these are essentially the equivalent expressions. And, this becomes handy when we go for optimization, so these three equations we will be using for optimization purpose any one of them. Before we proceed further now, we will try to look a relationship for l_i , l_i is a very important parameter that is the payload mass fraction is a very important parameter for multi stage rockets. So, let us take a closer look at the payload mass fraction.

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So, next we will look at, first of all the overall payload mass fraction, this is the overall payload mass fraction for the entire rocket, entire multi stage rocket, so it is given by l . So, then this l is equal to nothing but M_L upon M_0 , where M_L is the actual payload, and M_0 is the full initial mass, which includes all the stages, and this is the actual payload M_L is the actual payload.

Now, in the nomenclature what we have seen is the actual payload actually is the payload for the n th stage also, so therefore, this M_L can also be written as M_{L_n} , so it can be written as M_{L_n} , and the total mass is the initial mass for the first stage. So, I can

write it is M_{n-1} , so then from this discussion, M_L is the payload mass for the n th stage divided by the initial mass for the first stage.

Now, I can write this as the payload mass for the n th stage divided by the initial mass for the n th stage, then the initial mass for the n th stage is my payload mass for the $n-1$ th stage. So, I can write it as M_{n-1} divided by the initial mass for the $n-2$ th stage, just a second initial mass, this is the initial mass for the n th stage which is the payload mass for the $n-1$ th stage.

So, let me just redo it, this is the payload mass for the n th stage divided by the initial mass for the n th stage, and we have said that the initial mass for the n th stage is the payload mass for the previous stage, so this is the payload mass for the previous stage divided by initial mass for the previous stage. And then we continue, so now this becomes the payload for the $n-2$ th stage, and then initial mass for the $n-2$ th stage.

And, we continue like this till we come to the first stage, M_0 is the initial mass for the first initial mass for the second stage, which is also equal to the payload mass for the first stage, so we continue like this till we come to the first stage. So, now, if I look at this equation, and look at the definition of l_i , l_i is the payload mass fraction for the i th stage, which we had defined as M_{i+1} upon M_i , we have defined it like this.

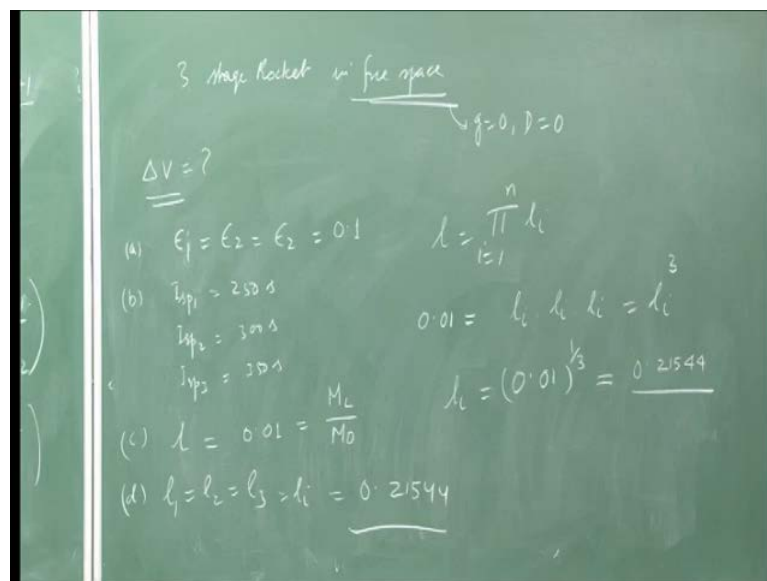
So now let us look at this term, what is this M_0 initial mass of the second stage, which is the payload mass for the first stage divided by M_0 which is the initial mass for the first stage, so therefore, this is nothing but l_1 . So, this is equal to l_1 then multiplied by l_2 continues till if I come to any stage in between it will be l_i into what is this the payload mass for the n th stage divided by the initial mass for the n th stage. So, that is L_n , so that is payload mass fraction for the n th stage.

So now what we see here, is the overall payload mass fraction is essentially the product of individual payload mass fraction, this is a very important observation this gives us as a constraint, and it is true no matter what, this is the constraint with which we will be working. So, I can write as l is equal to product of l_i from $i=1$ to n , l_i this is a very important result.

So, let me call this equation 4, when we are using these equations, when we are using these equations l_i is varying here, typically the overall mass fraction will be a known quantity from there we can estimate l_i , I will come to that later or when we go to optimization there will be a specific relationship, which can be shown. So, therefore, no matter what by the way for a multi stage rocket, this expression is always valid. Because of the fact, that the payload for the one stage is the initial mass for the next stage, therefore this equation is always valid.

Now, with this then let us now solve a problem for estimation of essentially velocity increment for a particular rocket with particular given conditions. We will take a very simple example, later on when we do optimization, and then we will go for little more complex problem. But, very simple problem, essentially what we are trying to do is use these equations use these equations to get some information.

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Let us consider, three stages rocket in free space, so essentially first of all what does this term free space means that g and D are 0, gravity and drag are 0. For this three stage rocket we are supposed to find out the velocity increment, delta v , the conditions given are a, that the structural coefficient for all the stages are same, that is epsilon 1 is equal to epsilon 2 is equal to epsilon 3, that is equal to 0.1, this is a given condition.

Secondly, what is given is that, the I_{sp} values is given that the I_{sp} value for the first stage is 250 second, I_{sp} value for the second stage is 300 seconds, and that for the third

stage is 350 seconds, these are the three values, that are given, it is also given that the overall payload mass fraction λ is equal to 0.01.

And, another condition that is given is that the payload mass fraction for every stage is same, these are the conditions that are given we have to get the velocity increment for this rocket. First let us come to this λ is equal to 0.01, which is the total final payload divided by the initial mass, and we are given λ_1 equal to λ_2 equal to λ_3 .

First, what we do is let us get these values what are the values of λ_1 λ_2 λ_3 for that we use this equation, what we see here is that first lets write λ_1 equal to λ_2 equal to λ_3 is equal to λ_i , then from that equation λ equal to λ_i , λ_i equal to λ_1 to λ_n λ_i , and therefore, this value is given 0.01 equal to λ_i into λ_i into λ_i , so this is equal to λ_i cubed, therefore λ_i is equal to cube root of 0.01.

Now if I solve this is equal to 0.21544, so what we are said doing here is that, the problem gives us the overall payload mass fraction, and it also states that every stage all three stages have the same payload mass fraction. Now, if the payload mass fraction is same for all the stages then from this equation, we have just proved that this equation is valid for any multi stage rocket which says that the product of individual stage payload mass fraction is equal to the overall payload mass fraction.

So, we have used this equation here λ is equal to λ_i equal to λ_1 to λ_n λ_i , this value is given we have from there we can calculate what is the payload mass fraction for individual stages. So, now, this is equal to 0.21544, so this is the first stage of the problem done. Now let us come to the second part of the problem, with this now we have to estimate Δv Δv is our velocity increment for that we go back to our expression for multi stage velocity increment.

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$$\begin{aligned} \underline{\Delta u} &= \sum_{i=1}^n \Delta u_i = \sum_{i=1}^n u_{eq,i} \ln R_i \\ &= \sum_{i=1}^n I_{sp,i} g_e \ln R_i = \sum_{i=1}^n I_{sp,i} g_e \ln \left(\frac{1}{L_i(1-G) + G} \right) \\ &= \left[(9.8) \ln \frac{1}{(0.21544)(1-0.1) + 0.1} \right] (250 + 300 + 350) \\ \Delta V &= 10811.37 \text{ m/s} \end{aligned}$$

So, we have seen that Δv is equal to $\sum_{i=1}^n \Delta u_i$, this we have seen and this is equal to $\sum_{i=1}^n u_{eq,i} \ln R_i$, we have also seen this is equivalent we can write it as $I_{sp,i} g_e \ln R_i$. Now in this problem what are the parameters given to us, after we have solved this, what is given to us are ϵ_1 , ϵ_2 , ϵ_3 and this is ϵ_3 and L_1, L_2, L_3 .

So, essentially this R_i is given in terms of L_i and ϵ_i we had derived a relationship relating R_i and ϵ_i . So, now, if I put it back here, this is equal to $\sum_{i=1}^n I_{sp,i} g_e \ln \frac{1}{L_i(1-\epsilon_i) + \epsilon_i}$, this is the relationship that we had derived. Now let us look at this equation, this is what we want to estimate, what is given to us is $I_{sp,1}, I_{sp,2}, I_{sp,3}$, so these are given, g_e is known acceleration due to gravity at sea level is a known parameter, ϵ_i is given so that means, $\epsilon_1, \epsilon_2, \epsilon_3$ is given.

L_i , we need and we have estimated L_1, L_2, L_3 , so therefore, all the parameters in our right hand side are now known. So, if I now just put it back here, this becomes equal to first $\epsilon_1 I_{sp,1}$ is 250 times 9.8, which is our g_e times $\ln \frac{1}{0.21544(1-0.1) + 0.1}$, 1 minus 0.1 plus 0.1. Now, if I look at this the first term for i equal to 1 is this, for i equal to 2, this term remains same because our L_i is same for all three stages, and this terms also remains same because ϵ_i is same for all three stages.

So, only thing that is going to change is I_{sp} , so what I will do is I will rewrite it as this term is same, and here I will add the I_{sp} values 300 plus 350. So, essentially what I am doing is I have this value as a constant, and then to this I am multiplying sum of 3 I_{sp} values 2 of 250, 300 and 350 seconds.

Now, after this then if you solve this Δv value comes out to be equal to 10811.37 meter per second, so this is the value of Δv for this problem. So, now we know how to estimate Δv for given conditions, later on in the next lecture, what we are going to see is how do we optimize this, that is we are given some parameters how do we distribute it, so that we get this value maximum. So, we will be given some constraints under this constraints, we would like to maximize the velocity increment that we can attain for this multi stage rocket.

This example, I have given is a very simple example where all the structural coefficients were equal, and the stage payload mass fractions were equal, but in reality you may not have the same condition, here only thing that was differing was the I_{sp} . In reality you may have different distribution, depending on the mission requirement you may need to have different distribution, so that we can optimize the performance of the rocket.

So, far we have seen how a multi stage rocket works, we have considered this for free space because as I have said that the drag and gravity can be neglected for most practical applications. So, we work with this expression, we have expressed R_i in terms of different parameters, so depending on what are the values given we choose for that is why I have taken this example. In this example what we have seen is that the epsilon values were given, the l values were calculated, so we used this form of the equation.

But, if let us say instead of this something else were given, then we use a different form of the equation, so therefore, there is a depending on the given parameters we choose which is the equation that needs to be used. And then essentially the governing equation is this you put it here, and get the final expression for our velocity increment, that is not going to change. Only thing is change is going to be that what form of R we are using, so let us stop here today, and in the next class we will take up the optimization of multi stage rockets.

Thank you.